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## Selection of optimal CO<sub>2</sub> capture plant capacity for better investment decisions

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### Abstract

Carbon Capture and Storage (CCS) is an important part of a carbon-constrained energy scenario to reduce global emissions. Most of the present works in literature related to CO<sub>2</sub> capture assumes exhaust stream from power plants, as they represent large CO<sub>2</sub> volume sources, and consider steady flow of exhaust stream to the capture units. However, the feed stream to the CO<sub>2</sub> capture unit from these sources will typically vary over time. As these fluctuations in the exhaust gas profile lead to lower utilization rate of the capture unit, building the CO<sub>2</sub> capture plant for a full capture might not be optimal. Therefore this work evaluates the optimum CO<sub>2</sub> capture unit capacity taking into consideration the trade-off between the cost of capturing CO<sub>2</sub> and paying the emissions cost (quota or tax) for given fluctuating exhaust gas profiles. Costs functions of an amine-based post combustion capture unit for a coal power plant exhaust gas are modelled to represent the cost of capturing CO<sub>2</sub>. A Mixed Integer Linear program is formulated and implemented in General Algebraic Modeling System (GAMS) to calculate the economic optimum CO<sub>2</sub> capture plant capacity. The model when applied to a typical fluctuating exhaust gas profile show results indicating significant economic gains in optimizing the installed CO<sub>2</sub> capture capacity. Therefore, in addition to significantly decreasing the cost of CCS on power plants, being able to forecast the fluctuating load on the CO<sub>2</sub> capture unit can also avoid investment delays compared to cases in which only full capacity capture is considered.

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### 1. Introduction

Large-scale decarbonisation of future energy systems is a possible scenario, moving towards more sustainable energy consumption and conversion. Non-renewable fossil fuels account for over 80% of the global total primary energy consumption, and CO<sub>2</sub> emissions from energy use (conversion) amount to

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about 60% of global manmade greenhouse gas (GHG) emissions [1]. Carbon Capture and Storage (CCS) is an important part of a carbon-constrained energy scenario to reduce global emissions [2]. The timing and selection of CO<sub>2</sub> sources will affect the cost of achieving projected CCS based emission reductions. Among factors affecting the attractiveness of a particular CO<sub>2</sub> source for CCS, IPCC Special Report on CCS [3] highlight four; (I) CO<sub>2</sub> volume, (II) CO<sub>2</sub> concentration and partial pressure, (III) integrated system aspects and (IV) proximity to suitable reservoir.

Most of the present work in literature related to CO<sub>2</sub> capture assumes flue gas from power plants, as they represent large CO<sub>2</sub> volume sources, and consider steady flow profile of the flue gas. However, the feed stream to the CO<sub>2</sub> capture unit from these sources will typically vary over time. For a load following power plant with CO<sub>2</sub> capture, this flow rate can significantly vary within a day as a function of utility demand. The load on a power plant and thus the CO<sub>2</sub> capture unit will also exhibit fluctuation over the longer time frame such as seasonal variations. For a CO<sub>2</sub> capture unit in an industrial facility (cement, steel, natural gas processing, etc.), the feed to the capture unit is also expected to fluctuate over time. However, the time scale of fluctuations in an industrial CO<sub>2</sub> capture unit will be on a longer time scale than that for a power plant.

As these fluctuations in the exhaust gas profile lead to lower utilization rate of the capture unit, building the CO<sub>2</sub> capture plant for a full capture might not be optimal. This paper evaluates the optimum CO<sub>2</sub> capture unit capacity taking into consideration the trade-off between the cost of capturing CO<sub>2</sub> and paying the emissions cost (quota or tax) for given fluctuating profiles.

## 2. Techno-economic optimization model

Given a fluctuating flue gas profile, the plant operator has a choice of whether to invest in a CO<sub>2</sub> capture unit or not and if so what should be the capacity of the unit. Further, operationally there are two options:

- capture the CO<sub>2</sub> and incur operating costs (and an initial capital investment cost) or;
- emit the CO<sub>2</sub> and pay for the CO<sub>2</sub> quotas needed to emit it.

The system under consideration incorporating these options is shown in Fig. 1. The flue gas fed from the source can either be sent to the capture unit or emitted to atmosphere (Flue gas Bypass in Fig. 1). The capture unit has a specified capture ratio defined to be the ratio of CO<sub>2</sub> captured to the CO<sub>2</sub> fed to the capture unit. Thus only part of the CO<sub>2</sub> fed to the capture unit is captured and sent to transport and storage. The residual CO<sub>2</sub> is emitted in the Exhaust Gas (see Fig. 1). This is used to set up the CO<sub>2</sub> balance for techno-economic optimization. The total CO<sub>2</sub> emitted is thus the sum of the CO<sub>2</sub> in the Bypass and Exhaust Gas streams.

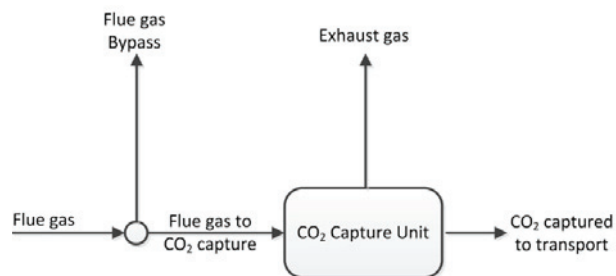


Fig. 1. System boundaries for techno-economic analysis

### 2.1. Economic model for capture costs

An amine post combustion capture process with 90% capture efficiency, based on Monoethanolamine (MEA) solvent is considered in this study. The investment and operating costs for CCS at different capacities were derived from a 2 MtCO<sub>2</sub>/y post-combustion capture plant simulation carried out in Aspen Process Economic Analyzer® [4] and subsequent scaling using the equipment cost power law and installation factors for the 1-7 MtCO<sub>2</sub>/y capacities used in this study. It was assumed the CCS plant received a flue gas with a 13% concentration of CO<sub>2</sub>, which is similar to conventional coal fired power plants.

The operating cost is split into fixed and variable operating costs. The fixed operating cost depends on the total investment cost, and covers maintenance, insurance and labour costs. The variable operating cost is a function of the operation load and CO<sub>2</sub> quantities captured. It covers consumption of utilities, electricity, steam, cooling water and MEA make up. Variable costs are assumed to be linear down to 1 MtCO<sub>2</sub>/y capacity due to parallel construction of main utility consuming units, such as blowers, the stripper and cooler. When a plant doesn't operate at full capacities, some of the parallel units are shut down while the rest operate at full capacity. Therefore it can be assumed that there is no efficiency decreases when a plant doesn't operate at full capacity. However it is assumed that a plant cannot operate under 0.6 Mt/y otherwise the operating condition of the packed columns is overly perturbed.

The annual fixed operating cost is assumed to be 7% of total investment costs, while the annual variable operating cost are estimated using the utilities consumptions given by process simulations and utility costs shown in Table 1. It is worth noting that the steam cost presented in Table 1 is based on extracting steam from the LP steam circuit.

Table 2 shows the functions used to derive Capital, Fixed Operating, and Variable Operating costs.

Table 1: Utilities costs

Utilities	Costs	Units
Electricity [2]	55	€/MWh
Steam prior to LP turbine (5bar 150°C) [1]	3.5	€/GJ
Water [3]	0.02	€/m <sup>3</sup>
Pure MEA [4]	1,300	€/t

Table 2: Cost functions for capture process

Function	Costs	Units (y)
$y = 58.45x^* + 15.24$	Capital	(€) Million
$y = 4.091x^* + 1.067$	Fixed Operating	(€) Million/y
$y = 15.26x^*$	Variable Operating	(€) Million/y

\*x is the plant's CCS capacity, ranging from 1-7 MtCO<sub>2</sub>/y

### 2.2. Model formulation

The objective of the optimization is to maximize the Net Present Value (NPV) of the capture system. The NPV is calculated based on the discounted cash flow method and is given as:

$$NPV = \sum_{t=0}^n \frac{Cash\ Flow_t}{(1+i)^t} \quad (1)$$

where  $Cash\ Flow_t$  is the cash flow in the year  $t$ ,  $i$  is the yearly discount rate not adjusted for inflation and  $t$  is the year number between 0 and  $n$ , the project duration.

The cash flow in year  $t$ ,  $CF_t$ , is calculated as:

$$Cash\ Flow_t = -[Capture\ Cost_t \cdot v_t + (CO_2\ Emitted_t - CO_2\ Captured_t) \cdot Emission\ Cost] \quad \forall t = (1, n) \quad (2)$$

$$Cash\ Flow_0 = -Investment\ Cost \cdot u \quad (3)$$

where  $CO_2\ Emitted_t$  is the total  $CO_2$  emitted in year  $t$  (Mt $CO_2$ ),  $Emission\ Cost$  is the cost of emitting the  $CO_2$  which is given by the  $CO_2$  quota price (€/t $CO_2$ ), and  $Capture\ Cost_t$  (M€) is the operating cost of the plant given as the sum of the fixed and variable operating costs described in Section 2.1.  $Capture\ Cost_t$  is a function of the  $CO_2$  captured in year  $t$  as well as the plant capacity,  $CO_2\ Cap_t$ .  $Investment\ Cost$  is the capital investment cost reported to the year 0, i.e. prior to plant operation.

$u$  is a binary decision variable that is set to 1 when the capture unit is installed and 0 when it isn't and  $v_t$  is a decision variable that indicates whether the capture unit is switched on/off in year  $t$ .  $u$  and  $v_t$  are related in that  $u = 0$  if and only if  $v_t = 0$  for all  $t$ . If any  $v_t = 1$  then  $u = 1$ .

The  $CO_2$  mass balance around the system (Figure 1) is given by the following equations

$$CO_2\ Flue\ Gas_t = CO_2\ Capture_t + CO_2\ Emitted_t \quad \forall t = (1, n) \quad (4)$$

$$CO_2\ Emitted_t = CO_2\ Flue\ Gas\ Bypass_t + CO_2\ Capture\ Unit\ Flow_t \cdot (1 - CO_2\ Capture\ Ratio) \quad \forall t = (1, n) \quad (5)$$

$$CO_2\ Captured_t = CO_2\ Capture\ Unit\ Flow_t \cdot CO_2\ Capture\ Ratio \quad \forall t = (1, n) \quad (6)$$

where  $CO_2\ Flue\ Gas_t$  is the total  $CO_2$  in the flue gas in year  $t$  (Mt $CO_2$ ),  $CO_2\ Flue\ Gas\ Bypass_t$  is the total  $CO_2$  in the Flue Gas Bypass that is not captured in year  $t$  (Mt $CO_2$ ),  $CO_2\ Capture\ Unit\ Flow_t$  is the total  $CO_2$  flow to the capture unit in year  $t$  (Mt $CO_2$ ) and  $CO_2\ Capture\ Ratio$  is the ratio between  $CO_2$  captured and  $CO_2$  capture unit flow defined by Equation 5.

$CO_2\ Captured_t$  is constrained by the size of the capture unit. This capture unit capacity related constraints are defined in the model as

$$Minimum\ CO_2\ Captured \leq CO_2\ Captured_t \leq Capture\ Unit\ Capacity \quad \forall t = (1, n) \quad (7)$$

$$Capture\ Unit\ Capacity \geq Minimum\ Capture\ Unit\ Capacity \quad (8)$$

where  $Capture\ Unit\ Capacity$  is the  $CO_2$  capture unit capacity (Mt $CO_2$ /year),  $Minimum\ CO_2\ Captured$  is the lowest  $CO_2$  capture possible in the capture unit (Mt $CO_2$ ) and  $Minimum\ Capture\ Unit\ Capacity$  is the smallest  $CO_2$  capture unit capacity (Mt $CO_2$ /year). The smallest  $CO_2$  capture unit capacity is defined to

be 1 MtCO<sub>2</sub>/year in this work and subsequently the lowest CO<sub>2</sub> capture possible is 0.6 MtCO<sub>2</sub>/year. The maximum CO<sub>2</sub> capture unit capacity need not be defined, but would the maximum CO<sub>2</sub> flow rate in the flue gas profile.

The objective function will try make  $u$  and  $v_t$  to take values 0. Hence we need to include an equation that links a continuous variable,  $CO_2\text{ Captured}_t$ , to the binary variable,  $v_t$ , to ensure it takes a value 1 when CO<sub>2</sub> is captured by the system. This is given by the "big M" constraint below

$$CO_2\text{ Captured}_t - M \cdot v_t \leq 0 \quad \forall t = (1, n) \quad (9)$$

where  $M$  is set to the maximum CO<sub>2</sub> capture possible for the given variable CO<sub>2</sub> flue gas profile. Equation 9 will ensure that  $v_t = 1$  when  $CO_2\text{ Captured}_t > 0$ .

The techno-economic optimization model to find the optimum capacity is thus formulated as a Mixed Integer Linear Problem (MILP) with Equation 1 as the objective function to be maximized. Equations 2 – 9 are the constraints of the problem. The model is solved in GAMS using CPLEX as the solver.

### 3. Optimal capacity for fluctuating flue gas profiles

The daily flow profile of the flue gas is shown in Fig. 2 (in blue). The flue gas contains 13.3 vol% CO<sub>2</sub>. The CO<sub>2</sub> flow rate is represented by the red bars in Fig 2.

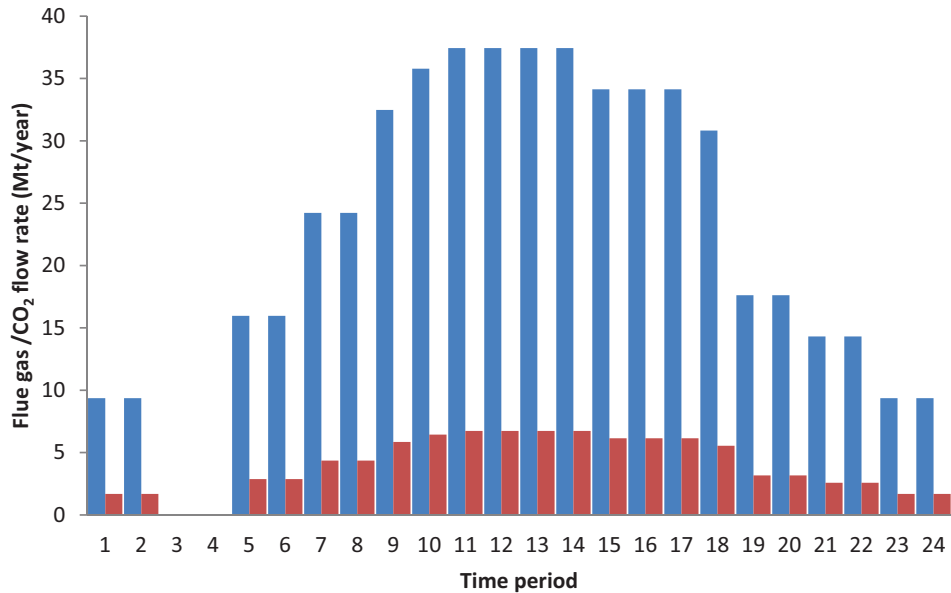


Fig. 2. Daily flow profile of flue gas

The flue gas has a CO<sub>2</sub> concentration of 13.3 vol% and the molar mass of the flue gas is 32.5 kg/kmol. The time period of analysis and lifetime of the capture plant is set to 30 years. The discount rate is assumed to be 8%.

For a given flue gas flow profile, the optimal capacity and CO<sub>2</sub> captured depends on the CO<sub>2</sub> quota price. Figure 3 shows the optimal capacity calculated for a range of CO<sub>2</sub> quota prices from 15 to 80 €/t CO<sub>2</sub>.

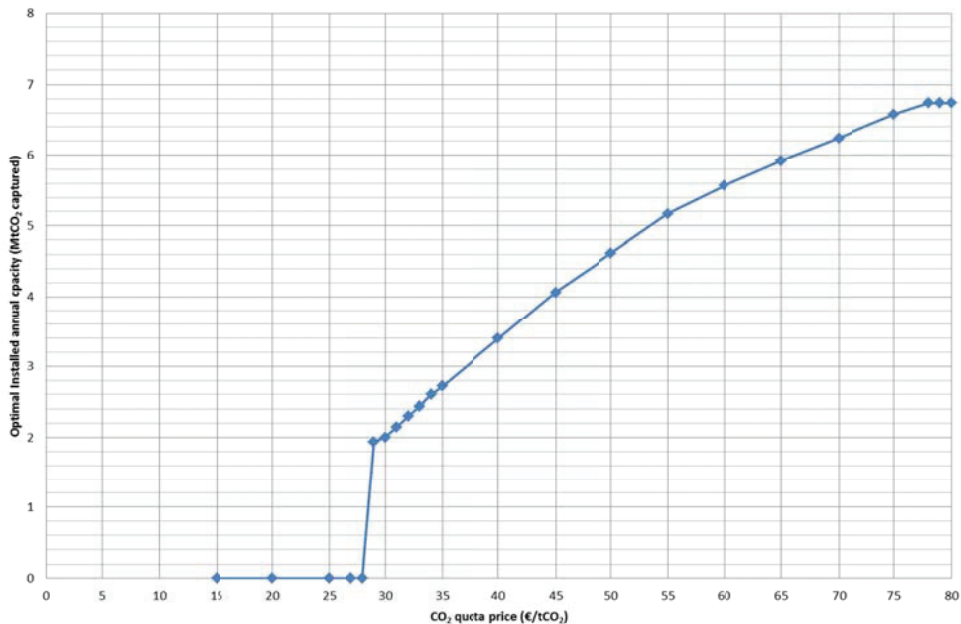


Fig. 3. Optimal capacity as a function of CO<sub>2</sub> quota price

As it can be seen from Fig. 3 and as it can be intuited, at low CO<sub>2</sub> quota price, no CO<sub>2</sub> capture capacity shall be installed. At 29 €/t CO<sub>2</sub> the optimal installed capacity is 1.9 MtCO<sub>2</sub> captured/year. This corresponds to the capture break-even price which is the lowest CO<sub>2</sub> emission cost required to equal the cost of a non-null capacity.

The optimal installed capacity steadily increases with increasing quota price until it reaches its maximum capacity value of 6.7 MtCO<sub>2</sub> captured/year for an emission cost of 78 €/t CO<sub>2</sub>. This correspond to the full capture break-even price which is the lowest CO<sub>2</sub> emission cost for which the cost optimal capacity is maximum CO<sub>2</sub> amount which can be captured from flow in exhaust gas profile.

As it can be seen here, the difference between these two costs is quite significant<sup>†</sup>. Indeed, the full capture break-even price is almost three times the capture break-even price. Therefore one can see the

<sup>†</sup> It is however worth noting that in the case of a constant flow, these two break-even costs and volume are the same.

interest of not capturing at full capacity. A first result of this trend is that industrial actors might make different capture capacity selection depending on their expected CO<sub>2</sub> price and their value for flexibility. Fluctuating production profiles for gas and coal fired power plants could be the case in electricity markets with increased capacity of intermittent renewable production capacity. Another result is that not capturing at full capacity from fluctuating, but at a lower capacity, is less expensive and therefore not capture at full scale may enable a faster development of CCS projects. However this conclusion shall be tempered by the fact that transport and storage, not included here, will also benefit from economies of scale and might decrease the benefit of smaller capture capacities in the case of fluctuating flow.

#### 4. Conclusions

An MILP formulation for the techno-economic optimization for evaluating the optimal CO<sub>2</sub> capture unit capacity for a fluctuating flue gas flow profile has been developed. The model was applied to a typical flue gas profile and the results showed that the profile in accordance with the CO<sub>2</sub> quota price influences whether CO<sub>2</sub> capture unit is installed or not and the optimal installed CO<sub>2</sub> capture unit capacities. Therefore, in addition to significantly decreasing the cost of CCS on power plants, being able to forecast the fluctuating load on the CO<sub>2</sub> capture unit can also avoid investment delays compared to cases in which only full capacity capture is considered.

The results presented here are valid when the CO<sub>2</sub> quota price is kept constant throughout the life time of the unit. Further work should involve, varying the CO<sub>2</sub> quota price over the horizon to include the decision on when to install the CO<sub>2</sub> capture plant in addition to its optimal capacity. Further, coupling this with the electricity prices, the plant operation can be optimized to maximize profit by emitting CO<sub>2</sub> when the electricity price is higher relative to the CO<sub>2</sub> quota price. It is also envisaged that this model could be expanded to study CO<sub>2</sub> chains from multiple sources to multiple sinks.

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