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Embodied greenhouse gas emissions from PV systems in Norwegian residential Zero Emission Pilot Buildings

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Abstract

Greenhouse gas (GHG) emissions from the combustion of fossil energy need to be reduced to combat global climate change. For zero energy and zero emission buildings (ZEB), photovoltaic solar energy systems are often installed. When the goal is to build a life cycle zero emission building, all emissions come under scrutiny. Emissions from photovoltaic (PV) energy systems in zero emission buildings have been shown to have a relative large share of material emissions. In this paper, we compare GHG emissions per kWh of electricity and greenhouse gas emission payback times (GPBT) for three residential PV systems in zero emission pilot buildings in Norway. All the buildings have roof mounted PV systems with different design solutions. The objective is to analyse the emission loads and GPBT of these three systems to facilitate for more informed choices of energy systems for zero emission buildings. The results show that the total embodied emissions allocated per square meter of module area are around 150 kg CO₂eq/m² to 350 kg CO₂eq/m² for the three different systems. Emissions from the mounting systems vary from 10-25 kg CO₂eq/m² depending on the material types and quantities used. When modules replace other roofing materials, such as roof tiles, mounting emissions were reduced by approximately 60%. GHG emissions per kWh electricity produced were in the range of 30-120 grams CO₂eq/kWh for the different systems. The system with the lowest emissions was the largest system, which had a simple mounting structure and modules with reused cells. It was found that the GPBT was strongly dependent on the scenario used for electricity grid emissions. By applying a dynamic emission payback scenario with an optimistic reduction of emissions from the European electricity grid, the GPBT was 3-8 years for the different systems. When comparing the emissions with current Norwegian hydropower emissions, of around 20 grams CO₂eq/kWh, it was found that all of the PV system's emissions were higher. When compared to a mainly fossil fuel based grid, all the PV system's emissions are low. This study highlights the importance of reliable emission documentation for PV modules and their mounting structures on the market.

Keywords: zero emission buildings, building integrated photovoltaics, embodied emissions, GPBT, PV system design

1. Introduction

The building industry accounts for approximately one third of global energy use (IEA, 2013) and one fifth of global greenhouse gas emissions (IPCC, 2007). In order to reduce these emissions the concepts of zero energy and zero emission buildings have emerged. The revised directive on energy performance of buildings requires that all new buildings should be 'nearly zero energy buildings' by 2020 (European Parliament, 2010). According to Peterson et al. (2015) zero energy building is defined as "An energy-efficient building where, on a source energy basis, the actual annual delivered energy is less than or equal to the on-site renewable exported energy". Photovoltaic solar energy systems are the most common energy source installed in zero energy buildings (Voss and Musall, 2011). Dokka et al. (2013) presents a definition for Norwegian zero emission greenhouse gas buildings. The concept of a Zero Emission Building is similar to Zero Energy Buildings, except it uses emissions

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42 of CO₂ equivalents as the balancing indicator instead of primary energy (Sartori et al., 2012). A zero greenhouse
43 gas building (Zero Emission Building – ZEB) can also be referred to as a zero carbon building, ZCB (Hui, 2010).
44 The definition of zero emission buildings (ZEB) presented by Dokka et al. (2013) includes different ambition
45 levels depending on which emissions are included and compensated for. Two fundamental levels are the “ZEB-
46 O” level, which aims to balance out all operational emissions (O) from energy use, and the “ZEB-OM” level,
47 which aims to compensate for both operational emissions (O) and material (M) emissions. Material emissions
48 can also be referred to as embodied emissions. A life cycle zero energy concept has also been introduced by
49 Ramesh et al. (2010) and Cellura et al. (2014). The relative share of embodied energy compared to operational
50 energy is higher in zero energy buildings compared to conventional buildings (Cabeza et al., 2014) (Chau et al.,
51 2015). Life cycle GHG analysis of two Norwegian ZEB concept buildings aiming for the ZEB-OM level is
52 presented in Georges et al. (2015). In order to take the first steps from theoretical concept buildings to real-life
53 pilot buildings, three residential zero emission pilot buildings have been built in Norway. These are the Skarpnes
54 case study with a ZEB-O ambition level, and the Multikomfort and Living Lab buildings both with ZEB-OM
55 ambition levels. Previously, material emission accounting for both of the ZEB-OM pilot buildings have been
56 performed (Kristjansdottir et al., 2016, Inman and Houlihan Wiberg, 2015). The studies showed that the PV
57 systems were a large contributor to embodied emissions for both cases, confirming the results from the concept
58 studies (Good et al., 2016, Wiberg et al., 2014, Georges et al., 2015). In these analyses the PV system emission
59 accounting were simplified. Since the PV systems contribute largely to the material emissions in Norwegian
60 ZEBs, it is important to know more about these systems and different emission loads. Can these emissions be
61 reduced? What are the emissions per kWh produced? What are the building integration benefits? And what is
62 their greenhouse gas payback time (GPBT) in years?

63 The objective of this study is to analyse greenhouse gas emissions from these three PV systems installed in
64 Norwegian ZEB pilot buildings. Further, the goal is to look into their GPBT with different electricity grid
65 emission scenarios. Increased knowledge on emission profiles for different PV systems suitable for Norwegian
66 dwellings will facilitate more informed choices on energy systems for zero emission buildings. The PV systems
67 installed differ in terms of type of modules used, the roof mounting system, geographical location and design. In
68 Norway, there is limited experience with photovoltaics, and there are no standardised solutions for integrating
69 PV modules into roofs. In general, learning from PV pilot systems with regards to mounting solutions, module
70 choices and emissions pay back times, can improve future installations. To follow, we provide an overview of
71 the status of life cycle assessments of PV systems, and provide an introduction to roof integrated PV systems.
72 We then provide a description of the applied method and present the three case studies. Subsequently, we present
73 the results, and discuss and interpret our approach. Finally, we present some concluding remarks.

74 1.1. Life Cycle Assessment

75 Life cycle assessment is divided into four main steps: goal and scope definition, inventory analysis, impact
76 assessment, and interpretation. Life cycle assessments often include a sensitivity analysis of important parameters
77 (ISO, 2006). The basic steps of a life cycle assessment for a photovoltaic system are presented in Fthenakis and
78 Kim (2011b). The raw material inputs and manufacturing of PV modules have been well documented through
79 various life cycle assessments (Alsema and de Wild-Scholten, 2006) (Jungbluth, 2005, Jungbluth et al., 2009,
80 Jungbluth et al., 2012, Fthenakis et al., 2011, NREL, 2012). However, according to Peng et al. (2013), life cycle
81 assessments of installed/operating PV systems are limited. In order to increase the comparability, transparency
82 and credibility of the life cycle assessment of photovoltaic electricity, methodological guidelines have been
83 developed by Fthenakis et al. (2011). Fthenakis and Kim (2011b) conclude that the emissions and energy payback
84 times of PV modules are heavily dependent on the type of electricity used to produce the modules. The global
85 PV market share is dominated by China and Taiwan (ISE, 2014). A comparative study of the carbon footprint of
86 PV module production in China and Europe was carried out by Yue et al. (2014). The study revealed that modules
87 produced in China have almost double the emissions compared to modules produced in Europe, with emissions
88 of around 72 grams CO₂eq/kWh and 37 grams CO₂eq/kWh respectively (for mono-Si modules). This difference
89 is mostly due to the fact that the emission intensity of electricity production in China is significantly higher than
90 in Europe. Yue et al. (2014) apply irradiation levels of 1700 kWh/m²yr and a performance ratio of 0.75. In
91 contrast, documentation of Norwegian produced PV modules has shown that there is a significant benefit from
92 using renewable hydropower in the production of silicon solar modules (Wild-Scholten, 2012). Prospective
93 studies of the life cycle primary energy use of PV modules have been presented in Frischknecht et al. (2015b),
94 Bergesen et al. (2014) and Mann et al. (2014). These studies highlight the expected reduction of material use, as
95 well as expected increases in the efficiencies of PV modules.

96 *1.2. Integrated Roof Mounting Solutions for PV Modules*
 97 PV systems may be integrated into building facades or roofs, or may be roof mounted. The three cases studied
 98 herein, all have roof mounted PV modules. In building integrated photovoltaic (BIPV) systems, the PV modules
 99 are used as part of the building envelope or any other architectural element that is necessary for the proper
 100 functioning of the building (SUPSI, 2015). Hence, the PV modules are replacing traditional parts of the building
 101 envelope, e.g. the roofing. A BIPV module can therefore not be removed without damaging the physical functions
 102 of the building envelope. Integrated systems present possible cost and material savings, as the modules are serving
 103 dual purposes (Jelle et al., 2012). Other roof mounting solutions on the market includes semi-integrated PV
 104 systems, sometimes referred to as in-roof systems. These solutions are designed to mount PV modules in line
 105 with the roof surface, in order to be visibly integrated in the existing roof.

106 **2. Materials and Methods**

107 The life cycle approach used is an attributional approach, focuses on the documentation of greenhouse gas
 108 emission burdens from the different life cycles of the PV system. The environmental impact category assessed is
 109 global warming potential (GWP) and is based on the IPCC GWP 2007 and IPCC 2013 100-year method,
 110 measured in kg CO₂ equivalents (IPCC, 2007) (IPCC, 2013). This assessment follows the methodological
 111 guidelines developed by Fthenakis et al. (2011) for the selection of functional unit and service lifetimes. The
 112 module degradation is calculated using values given by the producers.

113 *2.1. Goal, Scope and Functional Unit*

114 The goal of the assessment is to analyse and compare the different systems with respect to the GHG emission
 115 burden per kWh of produced electricity and the greenhouse gas payback time (GPBT) in years. The functional
 116 unit is "an averaged kWh of electricity produced per square meter of module area from the systems over a period
 117 of 30 years." Life cycle stages include: production of raw materials, manufacture of components, transport to the
 118 building site, manufacture of replaced components and simulated energy production with degradation over the
 119 service lifetime. Emissions associated with energy used during the installation of the systems are not included,
 120 as these emissions are considered to be similar across the different systems. The embodied emissions are
 121 calculated according to Equation 1:

122 **Equation 1**

$$123 \quad CO2eq_{embodied} = CO2eq_{modules} + CO2eq_{mounting} + CO2eq_{electric} + CO2eq_{transport}$$

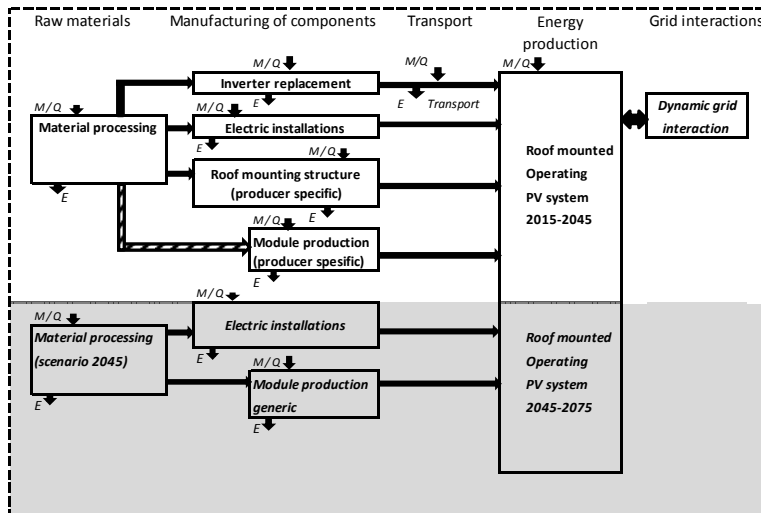
124 Here, the parameter $CO2eq_{embodied}$ includes the embodied emissions that have gone into the production of the
 125 PV modules, the mounting structure, the electric installations (e.g. inverter and cabling) and transport. The
 126 transport scenario includes transport to the building site. Figure 1 presents the scope of the analysis. The scope is
 127 divided into two main phases based on an estimates service lifetime of 30 years for the PV modules. The first
 128 phase, the initial 30-year scenario analysis is based on specific information from the case studies, and then a
 129 simplified generic future scenario is used for the replaced system in 30 years time. The end of life stage is not
 130 included, as it does not affect the emissions occurring in the next 30 years. In addition, waste treatment of PV
 131 modules in the future is highly uncertain.

132 *2.2. GHG Payback Time*

133 The term GHG payback time (GPBT) is defined as the number of years it takes for an energy generation system
 134 to "pay back" its embodied emissions through renewable energy generation (C. Reich-Weiser et al., 2008). It is
 135 calculated according to Equation 2, whereby ($CO2eq_{avoided(year)}$) (kg CO₂ eq) are the emissions avoided per year
 136 due to the production of electricity from the installation. $CO2eq_{avoided(year)}$ is calculated by multiplying the
 137 annual production with the average emissions per kWh per year from the local grid.

138 **Equation 2**

$$GPBT = \frac{CO2eq_{embodied}}{CO2eq_{avoided(year)}}$$



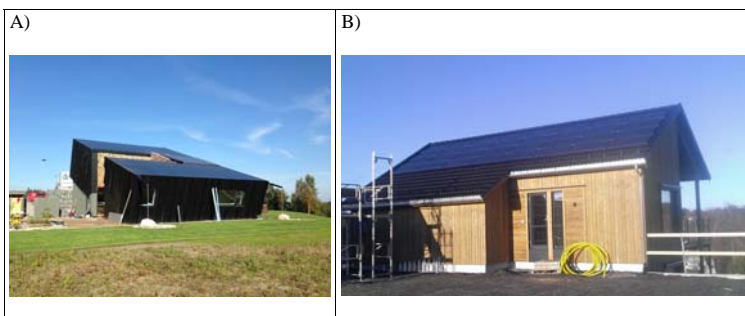
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141 Figure 1 Scope of the analysis, the boxes illustrate what is included in the analysis, M refers to materials, Q refers to energy, and
 142 E refers to emissions. The white area refers to the initial specific comparison applied for the first 30 years of the life time, while
 143 the grey area refers to a simplified generic scenario applied for the last 30 years of the life time.

144 2.3. Case Descriptions

145 The three analysed PV installations in Norway are shown in Figure 2. The three buildings are pilot studies
 146 within the Norwegian Research Centre on Zero Emission Buildings. All the buildings have low consumption of
 147 energy for space heating due to highly insulated envelopes, and a high heat recovery rate in the ventilation
 148 systems. The energy target set for the PV systems studied states that they should provide enough electricity on
 149 an average annual basis to cover all electricity consumption of the buildings. Details on the energy concepts for
 150 the three case studies can be found in Dokka et al. (2015), Goia et al. (2015) and Nord et al. (2016). For the
 151 Multikomfort building and the Living Laboratory, the ambition was set to a ZEB-OM level, whereby the PV
 152 systems were dimensioned to provide electricity to compensate for the electricity use from operation, and the
 153 embodied emissions from materials over the 60 year service lifetime of the building. We do not include the entire
 154 ZEB-OM balance calculations here, but focus only on the PV systems performances. Selected information for
 155 the PV systems for each of the buildings is provided in Table 1. Table 2 shows details of the installed PV
 156 systems. The three case studies represent three different roof mounting systems for the fixing of PV modules.

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157 Figure 2 The roof mounted PV system design of the pilot buildings: A) Multikomfort (Kristian Edwards, Snøhetta) B) Skarpnes
 158 (Skanska) C) Living Laboratory (Katrine Peck Size Lim)

159

160

Table 1. Building specifications

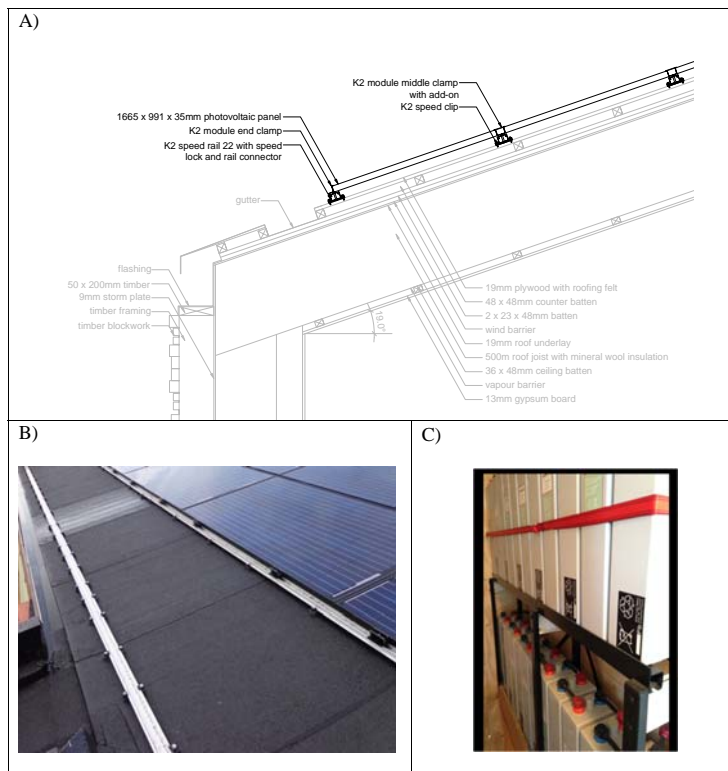
Description	Unit	A – Multikomfort	B – Skarpnes	C – Living Laboratory
Location	-	Larvik (59°12'N, 10°15'E)	Arendal (58°25'N, 08°43'E)	Trondheim (63°25'N 10°24'E)
Annual average ambient temperature	°C	8	8	5.7
Annual irradiation with optimal tilt angle	kWh/m ²	1182	1182	1120
Annual irradiation on the tilted plane	kWh/m ²	1057	1060	1091
Loss at current angle compared to optimal	kWh/m ²	11 %	10 %	3 %
Year of construction	year	2014	2015	2015
Heated floor area	m ²	202	154	102
Available roof area	m ²	155	106	108
Roof orientation		-45 (south-east)	51 (south-west)	0 (south)
Roof tilt	°	19	32	30
Ratio roof /floor area	m ² /m ²	0.77	0.69	1.06

161 *Irradiation data from PVGIS (Institute for Energy - Renewable Energy Unit)

162 2.3.1. Case A: Multikomfort

163 The Multikomfort case study is shown in Figure 2 A. It is a two-story residential building completed in 2014. It
 164 was built as a demonstration building for energy solutions for plus energy buildings. The design of the house is
 165 based on Saint-Gobain's Multi-Comfort concept (Saint-Gobain, 2015). The focus of the concept is both on
 166 comfort issues such as indoor air quality and daylight, as well as environmental performance. The photovoltaic
 167 modules are from Innotech Solar (ITS) (EcoPlus) and were chosen due to their low carbon profile (Innotech
 168 Solar, 2015, ITS, 2012, De Wild-Scholten, 2013). The PV system consists of 91 installed ITS modules. The PV
 169 system is grid connected and mounted in a landscape orientation. There are no shading objects in the immediate

170 surroundings of the building. Energy storage is included in the form of a battery bank, with the aim to increase
171 the economic output of the PV system. Previous LCA studies have documented that batteries used in photovoltaic
172 systems may contribute significantly to GHG emissions. This is mainly due to the manufacturing processes used,
173 and the short lifetime of batteries (Beccali et al., 2012, Beccali et al., 2014). In order to compare the three case
174 studies upon the same technological basis it was decided to exclude the batteries used in the Multikomfort house
175 from the system boundary. A section of the roof construction for the Multikomfort building is shown in **Figure**
176 **Figure-3A** and site pictures of the installation and battery bank are shown in Figures 3B and 3C. The PV modules
177 are not integrated in the roof, but are instead mounted on top of bitumen felt. Both the PV modules and the
178 mounting structure can be removed without any impact on the physical functions of the roof. The roof mounting
179 system is named K2 systems (Systems, 2015).



180 **Figure 3. A) Section of the roof construction (adapted from Snøhetta architects), B) Picture of the roof installation, C) Battery**
181 **bank**

182 2.3.2. Case B: Skarpnes

183 The Skarpnes case study is shown in Figure 2B. It is a two storey single residential building available on the
184 normal housing market. Skanska is responsible for the energy concept of the building. The building is located in
185 the first zero energy neighbourhood in Norway. The PV system consists of 32 high efficiency modules from
186 SunPower. The modules are mounted in a landscape orientation in four rows on the south-facing part of the
187 pitched roof. The PV array is connected in two strings to one inverter from SMA which is communicating with
188 the grid. There are no shading objects in the immediate surroundings of the building. The installation is a fully
189 building integrated PV system (BIPV). The mounting solution used is Solrif®XL from Schweizer (Schweizer,
190 2015). The BIPV installation on the Skarpnes building does not cover the full area of the roof, but is integrated
191 in the upper part of the south facing side. The rest of the roof is covered with traditional roof tiles. Hence, the
192 modules are substituting roof tiles in the areas they cover. A section of the roof solution is shown in Figure 4A,
193 and site photographs are given in Figures 4B and 4C.

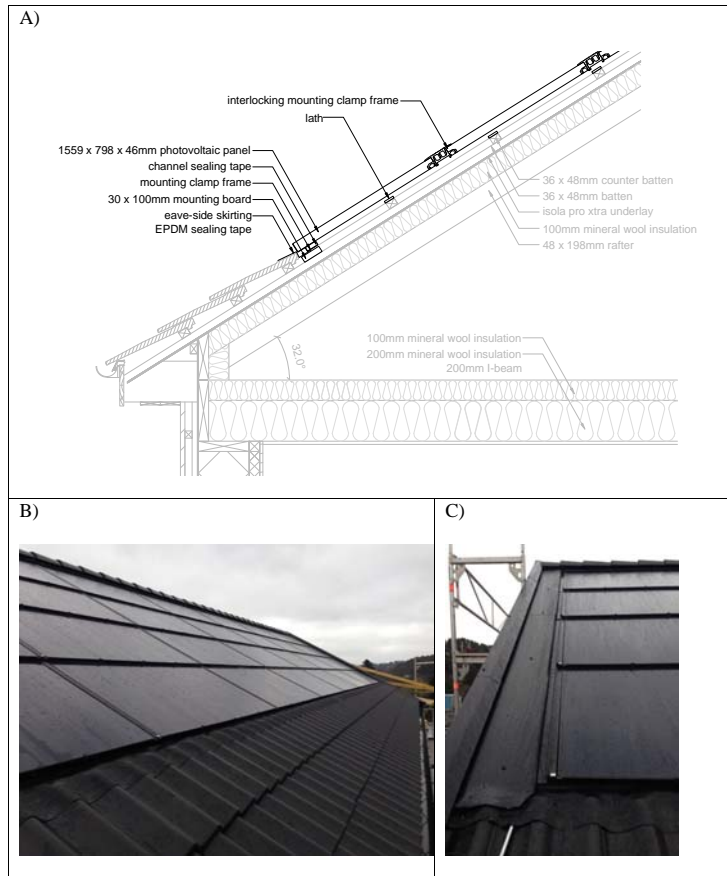
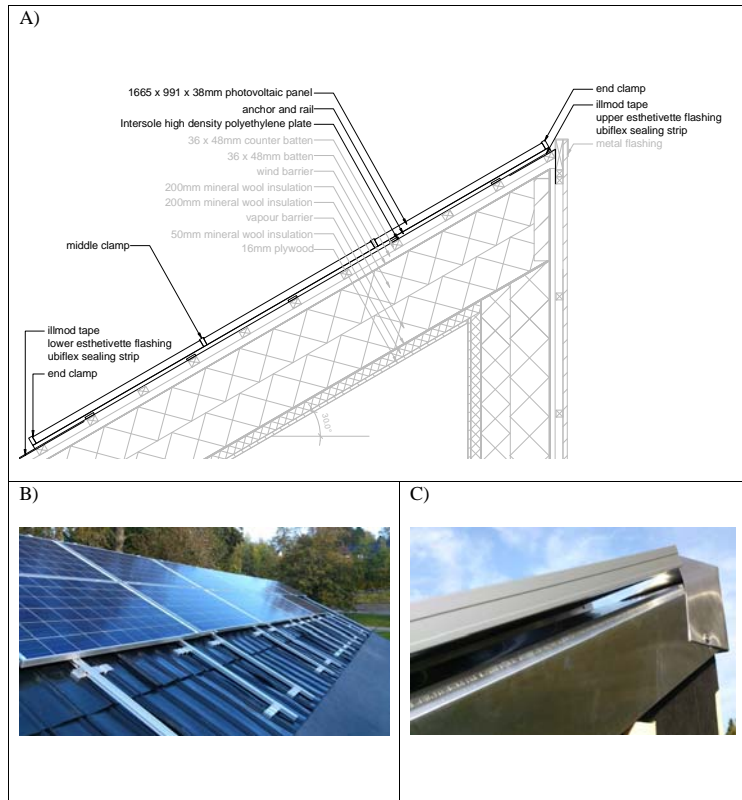


Figure 4 A) Section of the roof construction (adapted from Roald Rasmussen at Skanska), B) Picture of the roof installation, C) End profile

194
195

196 2.3.3. Case C: Living Lab

197 The Living Lab building is shown in Figure 2C. The building is located on campus at the Norwegian University
 198 of Science and Technology (NTNU) in Trondheim. The purpose of the building is to be a “living laboratory”
 199 whereby the performance of the building and its technology is observed and measured, whilst the building is in
 200 operation (i.e. when inhabited). The roof of the Living Lab has a saw-tooth shape, and the PV installation is
 201 divided between the two tilted roof areas (see 2C), each with 24 PV modules from REC Corp (REC, 2013). The
 202 PV installation is south facing with a 30° inclination. The southern-most roof shades the lower part of the
 203 northern-most roof during a relatively large part of the year. To minimize the impact of shading as much as
 204 possible, the modules are divided into two module strings (one upper and one lower). The module strings are
 205 connected to two inverters from SMA which feed into the grid. The roof construction of the Living Lab is shown
 206 in Figure 5A, and site pictures are shown in Figures 5B and 5C. The mounting structure replaces the roofing, but
 207 the modules, which are mounted on top of a solid board, can be removed without any impact to the building
 208 physics. The system applied is from Renusol Solar Mounting Systems (Renusole, 2015). The mounting structure
 209 has a 10-year product warranty and an expected reference service lifetime of more than 30 years (Solbes, 2013,
 210 Renusol, 2010a, Renusol, 2010b).



211 Figure 5. A) Section of the roof construction (adapted from Luca Finocchiaro), B) Photograph of the roof installation, C) End
 212 profile

213 Table 2. Details of the three PV Installations

Description	Unit	A – Multikomfort	B – Skarpnes	C – Living Lab
Manufacturer	-	Innotech Solar (ITS)	Sunpower	REC
Type of module	-	Design Black 250	SPR-230NE-BLK-D	REC260PE
Country of PV module production		Sweden (modules) and Germany (cells)	The Philippines	Singapore
Cell technology	-	Poly-Si	Mono-Si (back-contacted)	Poly-Si
Rated power per module	Wp	250	230	260
Efficiency at STC*	%	15.5	18.5	15.8
Module size	m ²	1.65 (1.665 x 0.991)	1.24 (1.559 x 0.798)	1.65 (1.665 x 0.991)
Weight	kg	19	15	18

Number of modules	-	91	32	48
Total module area	m ²	150	40	79
Total rated power	kWp	22.75	7.36	12.48
Total weight of modules	kg	1729	480	864
Inverter		Schneider Electric	1 x SMA Sunny Tripower 7000TL	2 x SMA Sunny Boy 5000TL 21-MS Basic
Number of strings		4	2	4
PV/inverter power ratio		1.15	1.05	1.36
Type of mounting system		BAPV	BIPV	In roof (semi integrated)
Mounting system manufacturer		K2 Systems	Schweizer/ Schweizer	Renusol/ InterSole SE
Place of mounting frame production		Leonberg, Germany	Chemnitz, Germany	Cologne, Germany
Battery storage		24, 42.3 kg Norbat, CFPV 2V 600Ah, OpzV GEL, (China)	No storage	No storage

214 *STC – standard test conditions: 1000 W/m², cell temperature 25°C and AM 1.5 spectrum

215 2.4. Inventory Assessment

216 The inventory is based on specific data gathered on the installed PV systems. The inventory includes simulations
 217 of operational energy performance, module emissions (with frames), the mounting structures, transport, the
 218 inverter and other electrical installations (cabling etc.). The background data is obtained from Ecoinvent v.2.2
 219 and v.3.1 (Frischknecht et al., 2007, Weidema et al., 2013). The life cycle analysis tool SimaPro v.8.0.5 (Pre
 220 Consultants, 2012) has been applied to access and analyse the Ecoinvent data. Benefits from the reuse or
 221 recycling of components are not included. The inventory for the electrical installations is based on specific details
 222 relating to the size of the system and weight of the inverters with background data from Ecoinvent.

223 2.4.1. Energy Performance of PV Systems

224 The energy performance of the three PV systems is evaluated through simulations, using the tool PVsyst
 225 (PVSYST SA, 2011.). Site-specific Meteororm data (Meteotest, 2009) has been used. Annual total solar
 226 irradiation for the given locations is given in Table 1. The performance ratio (PR) is defined as the ratio between
 227 the final system yield (Y_f) divided by the reference yield (Y_r) given by Equation 3:

228 **Equation 3**

$$229 \quad PR = \frac{Y_f}{Y_r}$$

230 Whereby, Y_f is the ratio of the net energy output and the nominal power of the installed array and Y_r is the ratio
 231 between the total in-plane irradiance and the PV reference irradiance (1000W/m²).

232 The performance ratio takes into account array and system losses, such as losses due to shadows, the inverter and
 233 wiring (Marion et al., 2005) (PVSYST SA, 2011.). The performance ratio of these three systems was around 0.8,
 234 depending on the actual system design in each case. Losses due to snow coverage of the PV modules represent
 235 an area of high uncertainty. Snow coverage and the possibility of snow clearing depend not only on the location,
 236 but also the orientation, maintenance, type of modules, glazing and frame (Andrews et al., 2013). It is assumed
 237 that the modules are covered by 20% snow, between November and February, for all three cases. This assumption
 238 is based on discussions with PV consultants and installers in Norway.

239 Internal energy consumption of the inverters is considered negligible. None of the systems are optimally oriented
 240 for their location, which would be around 40–45° and south facing (annual optimisation). The losses in available
 241 irradiation, due to non-optimal orientation (not including shading losses), are largest for Multikomfort with
 242 around 12%, followed by 9% for Skarpnes and 3% for the Living Lab. Module degradation has been included in
 243 accordance with the warranty specified by the producers, as shown in Table 4. However, we apply a service
 244 lifetime of 30 years to all of the modules according to Fthenakis et al. (2011). The linear degradation is assumed
 245 to extend beyond the 25-year warranty period.

246 **Table 4. Product and power warranties of the three types of PV modules (Innotech Solar, 2013, SunPower Corp., 2012, REC**
 247 **Group, 2013)**

Module	ITS	SunPower	REC
Product warranty	12 years	25 years	10 years
Performance, warranty, initial degradation	At least 97% of initial power after the first year	At least 95% of initial power for the first 5 years	At least 97% of initial power after the first year
Performance, warranty, annual degradation	No more than 0.7% (at least 80.2% after 25 years)	No more than 0.4% per year (at least 87% after 25 years).	No more than 0.7% (at least 80.2% after 25 years)

248

249 The energy output with degradation accounted for, E' (kWh/m², year), is calculated according to equation (4)
 250 where E (kWh) is the first year energy yield, d_{int} (-) is the initial degradation, d_{lin} (-) is the linear degradation,
 251 A_{PV} (m²) is the module area, t_{int} (years) is the time of initial degradation, and t (years) is the module lifetime.

252 **Equation 4**

$$E' = \frac{E \cdot d_{int}}{A_{PV} \cdot t} \cdot \frac{1 - d_{lin}^{t-t_{int}}}{1 - d_{lin}}$$

253 PV module efficiency is dependent on the operating temperatures, decreasing with increased temperatures (M.A.
 254 Green, 1992). In a building integrated PV system, it is more difficult to assure good ventilation of the modules,
 255 resulting in higher temperatures than in free standing systems. This factor is taken into account in the simulations,
 256 whereby the Skarpnes system is considered fully integrated, the Multi- comfort and Living Lab systems are
 257 building adapted and semi-integrated respectively, and therefore have some degree of ventilation. The rear
 258 ventilation of the modules is taken into account by changing the thermal loss factor in the simulation program.
 259 The fully integrated system was simulated with a thermal loss factor of 15 W/m²K, and the semi-integrated and
 260 building adapted systems were simulated with a thermal loss factor of 20 W/m²K, as per the recommendations in
 261 the program (PVSYST SA, 2011.) When calculating the CO₂ avoided in the GPBT, we apply the dynamic
 262 production profiles per year, including the degradation of the modules. The PV energy performance, in the
 263 replacement scenario, is assessed in a simplified way, due to the large uncertainties in future module performance.

264 2.4.2. Module emissions

265 PV module emissions are sensitive to the local energy source at the production site of the main material inputs
 266 (Fthenakis and Kim, 2011a, Yue et al., 2014). It is assumed likely that single- Si module production emissions
 267 are within the range of 100–300 kg CO₂ eq/m² based on previous analyses (Jungbluth et al., 2012, Frischknecht
 268 et al., 2015a, Fthenakis et al., 2011, Fthenakis and Kim, 2011a). Life cycle emissions from the SunPower
 269 modules have been thoroughly documented in Fthenakis et al. (2012). According to that previous study, the
 270 SunPower life cycle emissions are 281 kg CO₂ eq/m² based on Philippine production, which is to the authors'
 271 knowledge the case for the modules used in Skarpnes. According to ITS, the emissions from the ITS modules
 272 are 80% lower than that from conventional crystalline modules, due to the optimization process of unused cells
 273 from other manufacturers (ITS, 2012). Emissions from the ITS modules have been documented with a simplified
 274 carbon footprint analysis by Wild-Scholten (2013), a study that is not comparable to a complete LCA study.
 275 Thus, we use module emissions data from the Ecoinvent database to resemble the ITS modules: "Photovoltaic
 276 panel, multi-Si, at plant/RER/I." We make the following adjustment in the Ecoinvent process to resemble the
 277 use of secondary cells in the ITS modules: "50% reduction in the use of primary cells for the baseline scenario,
 278 based on ITS (2012), Wild-Scholten (2013) and (Ecoinvent, 2013)." We apply emission data based on the

279 Ecoinvent database directly for the REC module (Photovoltaic panel, multi-Si, at plant/RER/I) with 210 kg CO₂
 280 eq/m² (Ecoinvent, 2013). REC was unable to provide specific emission data for their modules. Since the modules
 281 are the largest fraction of the PV system inventory, we have carried out a sensitivity analysis based on
 282 assumptions for “best case” and “worst case” scenarios for module emissions. The sensitivity analysis for the
 283 SunPower modules is based on differences in production locations as presented in the paper by Fthenakis et al.
 284 (2012). The “best case” is based on Norwegian production and the “worst case” is based on Malaysian
 285 production, whilst the baseline is Philippine production. The sensitivity for the REC modules is based on a Monte
 286 Carlo analysis performed in SimaPro v.8.0.5 of the Ecoinvent data, resulting in a normal distribution with a
 287 standard deviation (SD) of 16.8 kg CO₂ eq/m² (Ecoinvent, 2013) (Pre Consultants, 2012). The “best case” is -2 x
 288 SD, the “worst case” +2x SD, whilst the mean value is the baseline scenario. Finally, the sensitivity for the ITS
 289 modules is based on different assumptions of the amount of primary cells used. The “best case” is based on a
 290 scenario where 75% of the cells are reused, whilst the baseline assumes 50% reused cells, and the “worst case”
 291 assumes that no cells are reused. The ITS scenarios are inspired by the production methods of the ITS modules
 292 (ITS, 2012) (De Wild-Scholten, 2013). The sensitivities are given in Table 3.

293

Table 3 Module emission scenarios

Module	Best case kg CO ₂ eq/m ²	Baseline kg CO ₂ eq/m ²	Worst case kg CO ₂ eq/m ²
SunPower	200	281	307
ITS	89	130	210
REC	176	210	244

294

295

Table 4 Material inventory for the roof mounting structures, given per m² of PV

Material	Unit	A – Multikomfort	B – Skarpnes	C – Living Lab
Aluminium	kg	1.02	2.1	2.12
Glass fibre reinforced polyamide	kg	0.06	n/a	n/a
Polyethylene	kg	n/a	1.08	2.84
Polyurethane Foam	kg	n/a	0.68	0.28
Rubber	kg	n/a	1.2	n/a
Sealing Tape (alu PE)	kg	n/a	n/a	1.34
Steel	kg	0.07	0.19	n/a
Zinc plated steel	kg	0.05	n/a	n/a
Wood	m ³	n/a	0.004	0.002

296

297 2.4.3. Mounting structures

298 All materials used for the sake of mounting the PV modules have been included. The mounting material inventory
 299 is given in Table 4. The PV roof mounting structures consist of rails, clamps, sealing materials and other
 300 components. In some cases, for their installation in or onto the roof, additional timber battens were necessary,
 301 and flashings were required for the edges of the roof, for reasons of building physics and/or aesthetics. Material
 302 quantities for the Schweizer system were obtained directly from (Jungbluth et al., 2007). For the Living
 303 Laboratory and Multikomfort case studies, the inventory was gathered from technical datasheets for the system
 304 and system descriptions. Aluminium is used in all three of the mounting structures, because of the lack of specific
 305 information concerning the type and location of aluminium used, we have included a sensitivity analysis for
 306 aluminium emissions based on the Ecoinvent database: “best case” 1.4 kg CO₂ eq/kg (secondary), “baseline” 8.4
 307 kg CO₂ eq/kg (production mix) and “worst case” 22.8 kg CO₂ eq/kg (alloy based on Chinese electricity). For the

308 “best case” emission scenario, we include a possible building integration benefit by subtracting emissions of the
309 roofing material avoided, for the “baseline” and “worst case” scenarios the building integration benefits are not
310 included.

311 2.4.4. Transport

312 To calculate transport emissions of the components used, the production factory has been located using product
313 information from the manufacturer and factory inspection certificates. The online route explorer tool SeaRates
314 (SeaRates, 2015) has been used to calculate distances. Three transport scenarios have been modelled: “best case”
315 by ship, “baseline” by ship and truck and “worst case” only by trucks. Transport emission data is based on
316 Ecoinvent EURO 5 truck (Ecoinvent, 2013) and Ecoinvent Transoceanic Ship.

317 2.4.5. Electricity Grid Factor Scenario

318 To calculate the greenhouse gas payback time (GPBT) in years,
319 a reference value for the local grid is necessary to calculate the
320 avoided emissions. Future dynamic grid emission scenarios are
321 complex and we apply annual averages in our analysis.
322 Currently around 97% of the electricity production in Norway
323 stems from hydropower (NVE, 2013). The emissions of CO₂
324 eq/kWh from Norwegian Hydropower have been calculated to
325 be around 20 grams CO₂ eq/kWh (low voltage) by Ecoinvent
326 (2010). Figure 6 shows the average monthly power balance for
327 Norway, (production/consumption) based on hourly
328 production and consumption statistics from 2006-2014
329 (Statnett, 2015). From these statistics we see that Norway is
330 normally exporting electricity. However, Norway has been, on
331 average, sensitive to the import of electricity during the spring
332 months. Norway is connected to the European electricity grid
333 and the transfer capacity between Norway and Europe will
334 increase in the near future (Statnett, 2013). Graabak and
335 Feilberg (2011) and Graabak et al. (2014) previously
336 developed scenarios for emission profiles in 2010, 2020, 2030,
337 2040 and 2050, for the emissions of electricity
338 production in Europe. One of the scenarios developed is the “ultra-green” scenario, which assumes the European
339 electricity grid in 2050 will be nearly emission free. In this scenario, it is assumed that Norway is fully integrated
340 with the European electricity grid. Initial emissions for this scenario are documented as 361 grams CO₂
341 eq/kWh. We have interpolated the hourly profiles of the ultra-green scenario for each year towards 2050; the
342 results are shown in Figure 7. From this figure we see seasonal variations due to the dynamics of electricity
343 production and consumptions patterns modelled in the scenario by Graabak and Feilberg (2011). We also
344 see the decreasing trend towards 2050. We apply this future scenario for our baseline GPBT calculations, starting
345 from year 2015. Graabak and Feilberg (2011) also developed a simplified “worst case” scenario, the “red”
346 scenario, with low emission reductions due to a higher demand and lower increase in renewable energy
347 production. The “red” scenario estimates emissions from the grid to be 224 grams CO₂ eq/kWh in 2050, in
contrast to the ultra-green scenario which predicts an optimistic 30 gram average.

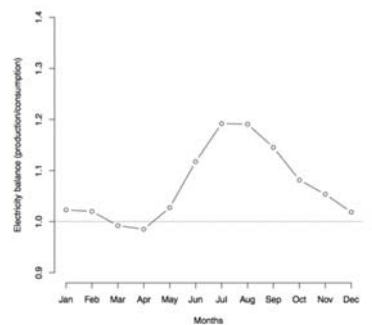
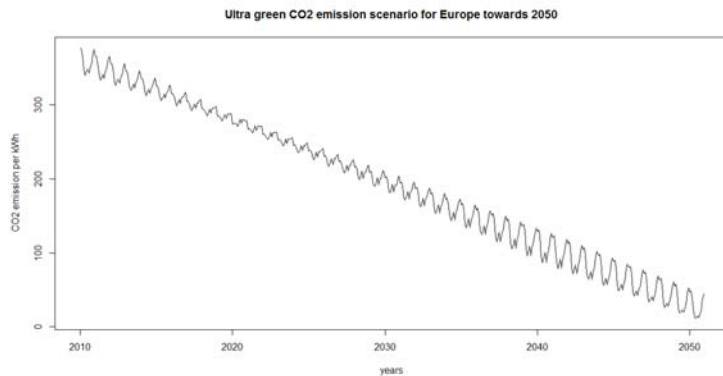


Figure 6 Average monthly power balance for Norway, 2006-2015 (import lower than 1, export higher than 1)



348

349 **Figure 7** Ultra-green scenario for emissions per kWh electricity in Europe towards 2050 (Graabak and Feilberg, 2011)

350 Dokka et al. (2013) present a Norwegian “ZEB emission factor” that is based on averaged emissions from the
 351 “ultra-green” scenario towards 2050, resulting in emissions of 132 grams CO₂ eq/kWh. For the sensitivity
 352 assessment, we include the ZEB emission factor and the “red” scenario.

353 2.5. System Replacement Scenario 2045

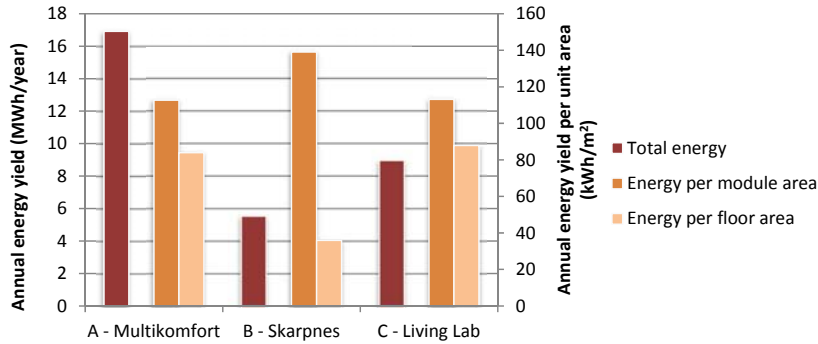
354 Within the PV industry there is a continuous development for new technologies and material use, as well as
 355 efficiencies for PV modules (NREL, 2016). For our case studies the building service lifetime is estimated to be
 356 60 years, thus the PV system needs to be replaced once. To increase our long term perspective we include a
 357 replacement scenario for the Skarpnes system. We assume that the replaced technology for the PV modules is
 358 the same, mono-Si. Frischknecht et al. (2015b) developed scenarios for life cycle emissions from future mono-
 359 Si and CdTe modules. They developed three different scenarios: “business as usual”, “realistic improvement”
 360 and “optimistic improvement”. The efficiency of the replaced single-Si modules is expected to be 22.9, 25.2 and
 361 27.6% in the different scenarios, respectively. We have chosen the realistic improvement scenario and set the
 362 module efficiency to 25.2%. The embodied emissions per m² of module are expected to decrease by 65%, based
 363 on (Frischknecht et al., 2015b). It is assumed that future modules will be produced in Asia, with initial emissions
 364 resembling the Malaysian production of SunPower modules (300 kg CO₂ eq/m²), as documented by (Fthenakis
 365 et al., 2012). This estimates replacement module emissions at 100 kg CO₂ eq/m². It is assumed that there are no
 366 emissions from mounting structures; the PV modules are fully integrated. Transport distances are assumed to be
 367 the same. It is assumed that the inverter, electrical installations and transport emissions are also reduced by 65%,
 368 (Frischknecht et al., 2015b). The degradation profile is based on data from SunPower (SunPower Corp., 2012).
 369 The production yield calculations are further based on irradiation and efficiency. For the future scenario we
 370 calculate greenhouse gas emissions per kWh produced, and the GPBT with the ZEB-factor and “red” scenario.

371

3. Results

372 3.1. Production yield

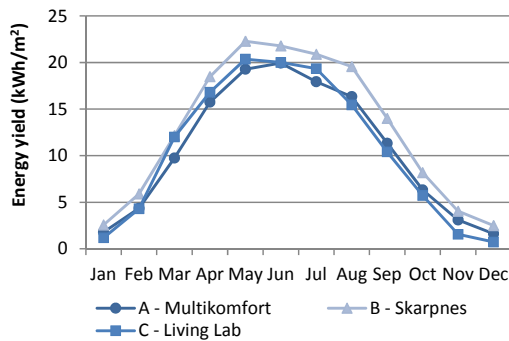
373 In Figure 8, the simulated production yield from the different systems is shown, in terms of both the annual energy
 374 production per module area, and per floor area of the buildings. The figure also shows the total annual power
 375 yield from the systems. The yield from the Multikomfort system is the highest, since this is the largest system.



376

377 **Figure 8. Simulation results for the total annual the energy yield per year (left axis) is shown together with the annual yield**
 378 **normalized per square meter module area and per square meter heated floor area (right axis).**

379 The normalised values for Multikomfort and the Living Laboratory are approximately equal, both with respect
 380 to energy yield per square meter module area and heated floor area. The irradiation (see Table 1) is slightly higher
 381 for the Living Lab than Multikomfort, but the Living Lab's system is also significantly influenced by self-shading,
 382 resulting in a similar energy output between the two buildings. Skarpnes has a smaller production in relation to
 383 heated floor area, but a higher energy production performance per square meter due to the higher efficiency of
 384 the mono-Si modules. The monthly energy yield for the first year of the three systems is shown in Figure 9. The
 385 Skarpnes system has the highest specific output during the whole year. The energy yield from Multikomfort is
 386 slightly higher during the autumn months compared to the Living Lab, due to the difference in tilt angles.



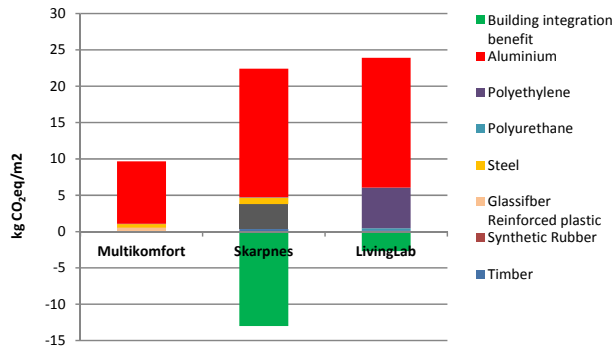
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388 **Figure 9. Simulations results for the monthly yield for the first year energy per square meter module area**

389 3.2. Emissions from Mounting structures

390 The emission loads for the different mounting structures are shown in Figure 10 for the baseline aluminium
 391 scenario. The K2 System applied in the Multikomfort building, has less than half of the emissions compared to
 392 the Schweizer and the Renusol systems. Between Schweizer and Renusol, the difference is less significant. The
 393 Living Lab and Skarpnes mounting systems have a larger material demand, which drives up emissions compared
 394 to the simpler K2 BAPV system. BIPV systems reduce the demand for traditional roofing material, because the
 395 system replaces the roofing materials in the areas where the PV is installed. The avoided emissions associated
 396 with this will depend on the type of roofing avoided. In the Skarpnes case, cement roof tiles are used. By applying
 397 the emission factor for roof tiles from Ecoinvent, 13 kg CO₂ eq/m², (Ecoinvent, 2010) the Skarpnes mounting
 398 structure emissions are reduced by around 60%. The emissions for the Living Lab are reduced by approximately

399 3 kg CO₂ eq/m² due to the avoidance of bitumen felt (Ecoinvent, 2010), but still has the largest amount of GHG
 400 emissions compared to the two other cases.



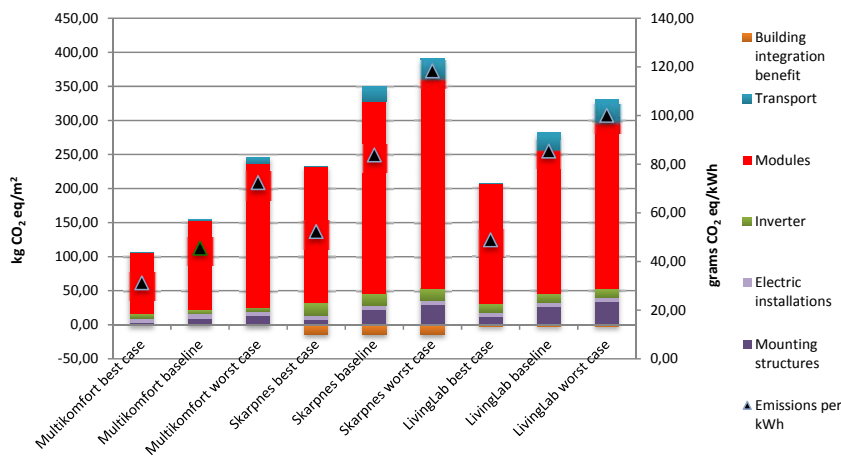
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 403

Figure 10. Emissions in kg CO₂eq/m² for the different materials for the roof mounting structures and building integration benefits

404 3.3. Emissions per square meter module area and kWh

405 In Figure 11, we present the results for the total embodied emissions allocated per square meter module area,
 406 including the sensitivity scenarios for module, transport and mounting aluminium emissions. The module
 407 emissions are the largest contributor, followed by the mounting structures and inverters. Total embodied
 408 emissions for the baseline scenario are around 150 kg CO₂eq/m² for Multikomfort, 350 kg CO₂eq/m² for Skarpnes
 409 and around 280 kg CO₂eq/m² for the Living Lab.



410

411
 412

Figure 11 Emissions loads from the systems in kg CO₂eq/m² and GHG emissions per kWh produced over the service lifetime of 30 years, including best, baseline and worst case scenarios

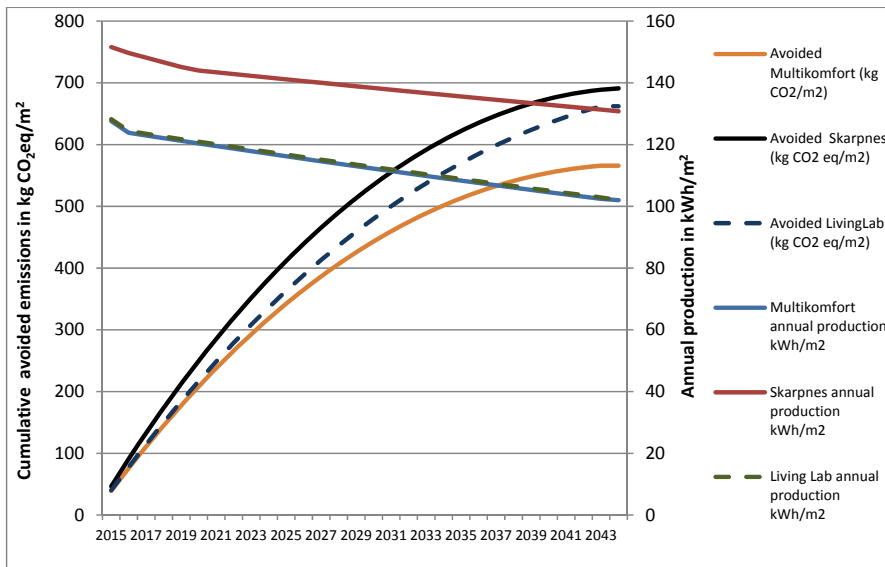
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414 From this figure, we see that the GHG emissions per kWh for the different systems range from around 30 to 120
 415 gCO₂eq/kWh. Emissions per kWh produced are lowest for Multikomfort. Emissions per kWh for Skarpnes and
 416 the Living Lab cases are similar. The sensitivity assessment shows that there can be a significant difference
 417 between system emissions per kWh. With emissions ranging from around 50 grams to 120 grams for the Skarpnes
 418 system, 30-70 grams for the Multikomfort system and 50-100 grams for the Living Lab.

419 **3.4. Greenhouse gas payback time (GPBT)**

420 In Figure 12, we show the dynamics of the emission payback scenario per square meter of module area for the
 421 different systems. The production profiles and cumulated avoided emissions are very similar for the Living Lab
 422 and Multikomfort systems, giving similar efficiencies. For the baseline scenario, embodied emissions and the
 423 "ultra-green" electricity emission scenario have payback times of around 3, 7 and 8 years for the Multikomfort,
 424 Living Lab and Skarpnes respectively. We also see from Figure 12 that Skarpnes gives larger emissions avoided
 425 per year due to higher module efficiency. When applying the "red" scenario; the GPBT is reduced to around 6
 426 years for both the Living Lab and Skarpnes. With the current averaged Norwegian ZEB factor of 132 grams CO₂
 427 eq/kWh, the GPBT increases to 8, 15 and 18 years respectively.

428



429

430 **Figure 12 Annual average productions with degradation and corresponding cumulative avoided emissions based on the "ultra-**
 431 **green" scenario**

432 For the replacement scenario from 2045-2075, the emissions per kWh are around 20 gram CO₂ eq/kWh for the
 433 Skarpnes system, with annual production yields of around 220 kWh/m². In the "ultra-green" emission scenario,
 434 the emissions are not payed back, but for the "red" scenario emissions are payed back within two years. When
 435 using the ZEB emission factor emissions are payed back within three years.

436 **4. Discussion**

437 From our analysis, we see that the life cycle emissions from the PV systems analysed have lower emissions
 438 compared to fossil fuels, thus confirming previous studies (NREL, 2013). We also see that there are significant
 439 differences between the systems, with respect to emissions from the modules and mounting structures. However,
 440 we also saw a wide range of emission loads within the best and worst case scenarios, thus it is challenging to
 441 make any decisive comparative conclusions. The GPBT varies significantly according to which scenario is
 442 applied, according to the avoided emissions in the grid. In the "ultra-green" scenario we saw that it takes 8 years
 443 to payback emissions from the Skarpnes system, but in the "red" scenario we saw a GPBT of 6 years for the same
 444 system. The simplified, static ZEB emission factor scenario gave us a GPBT of up to 15 years. Emissions can be
 445 paid back if PV system emissions are lower than the grid emissions. If we consider only an isolated Norwegian
 446 hydropower grid, which would have emissions of approximately 20 grams CO₂eq/kWh, (Ecoinvent, 2010) then
 447 the PV systems emissions are not payed back. This uncertainty emphasizes the need for careful consideration,

448 between the grid interaction and related system boundaries, when choosing energy systems for buildings. Even
449 though module emissions represent the largest fraction of emissions from PV systems, the mounting structures
450 also contribute significantly. From our analysis we saw that with proper integration of PV systems, we can reduce
451 the use of roofing materials, and thus reduce building material emissions. With large-scale implementation of
452 solar home systems, mounting emissions become more significant, even though they seem small when viewed
453 on an individual building basis. Therefore, minimizing mounting structure emissions with proper integration is
454 beneficial. Based on our simplified future emission scenario, emissions from electricity, from PV systems are
455 likely to be significantly reduced. At the same time, a payback calculation becomes more irrelevant in a scenario
456 where the grid becomes nearly emission free.

457 Emissions from the SunPower modules have been thoroughly documented, while for the REC modules, emission
458 data was not available. For the Multikomfort case, emissions from the module scenarios were low, due to the
459 use of reused cells in the ITS modules. The allocation procedures for emission burdens, when using secondary
460 or waste material, can be challenging. We therefore made a simplification, in that there were no emission loads
461 from the reused cells, which is debatable. Comparing different life cycle studies is challenging, as different
462 methods and reporting formats are used by different authors, thus reducing comparability. When installing a PV
463 system, it is preferable to have proper knowledge of the emission burdens of the installed modules. In some cases,
464 we encountered difficulties in gaining specific data from producers, a challenge that may be resolved in the future.
465 According to (Fraunhofer, 2012) [Fraunhofer \(2012\)](#) the end of life benefits of recycling, especially glass and
466 aluminium can have significant influence on the overall life cycle impact of PV modules. These potential benefits
467 have not been included.

468 With regards to the battery storage, the Multikomfort system is more self-sufficient and possibly gains a better
469 economic output. We have not included the impact from the batteries. This is an aspect that requires further
470 investigation. We have limited our analysis to GHG emissions, mainly due to the fact that the pilot case studies
471 have focused on a zero emission GHG balance. Looking also into the primary energy balance of the different
472 systems would be of interest. Nevertheless, previous studies have shown that cumulative energy demand and
473 greenhouse gas emissions often correlate (Huijbregts et al., 2006).

474 Service lifetime is an important parameter for emission burden accounting; in a scenario with a shorter service
475 lifetime, emissions per kWh are increased. The replacement of possible defect modules has not been taken into
476 account, which is also an aspect that could increase service lifetime emissions.

477 Currently, there is a lack of guidelines for good BIPV practice in Norway. In cold climates, shading caused by
478 snow, needs to be considered. How much this influences a system is difficult to know, without site-specific
479 measurement. None of the systems are optimally oriented for their location, which would be around 40-45° and
480 south facing (annual optimisation). Optimal orientation would have resulted in lower emissions per kWh.

481 From historical statistics of the Norwegian export profile for electricity, it can be argued that producing electricity
482 in the spring months gives an extra benefit for the Norwegian electricity grid. Production in the summer months
483 is considered to have a lesser value, as it could lead to lower prices. With the high availability of hydropower in
484 Norway, one could argue that PV system installations are not necessary. As a result, PV systems should be
485 prioritised in areas with higher solar irradiation and electricity grids based on fossil energy. In contrast, a large
486 fraction of Europe's electricity is produced from fossil fuels, emphasising a general need for the increased
487 electricity production from renewable energy sources, and therein PV systems (Eurostat, 2015).

488 From the "ultra-green" emission scenario in Figure 7, and the Norwegian export-import sensitivity analysis in
489 Figure 6, we get a picture of the seasonal grid production and emission sensitivities. Essentially, the emissions
490 are higher in the winter and lower in the summer. As an area for further study, it would be interesting to include
491 a month-by-month emission payback profile of the systems, combining energy demand and generation on an
492 hourly basis. There are plans to measure the energy outputs of the systems, which will bring insight into the real
493 operational performance of the PV systems in a Norwegian context.

494 5. Conclusions

495 We have looked at the emissions of GHG and GPBT for three different PV systems installed in Norwegian Zero
496 Emission Buildings for an estimated service lifetime of 30 years. These systems are referred to as the

497 Multikomfort, Skarpnes and Living Lab. We have included a simplified future scenario, whereby one of the PV
498 systems is replaced after 30 years. Total embodied emissions, allocated per square meter of module area, for the
499 baseline scenario are around 150 kg CO₂ eq/m² for Multikomfort, 350 kg CO₂ eq/m² for Skarpnes and around 280
500 kg CO₂ eq/m² for the Living Lab. The simplest mounting system showed emission of around 10 kg CO₂/m²,
501 whilst the other, more complex systems showed emissions from around 20-25 kg CO₂ eq/m². A building
502 integration benefit, where roof tiles were replaced with PV modules, reduced mounting system emissions by
503 around 60%. We also see that module emissions have the largest proportion of emissions from the three different
504 systems, stressing the need for reliable data on PV module production. Emissions per kWh produced, showed
505 that the lowest emissions originated from the Multikomfort system which had approximately 45 grams CO₂
506 eq/kWh, and around 80-85 grams for the other two systems. Emissions from the Multikomfort system are lowest,
507 due to the use of reused cells in the modules, combined with the large dimension of the system, and the simple
508 roof mounting structure. The sensitivity analysis showed that there are large variations in emissions, with the
509 total span from around 30 to 120 grams CO₂ eq/kWh. The GPBT is very sensitive to the grid scenario for
510 emissions. The baseline scenario “ultra-green”, showed emission payback times of 3, 7 and 8 years respectively.
511 The GBPT is decreased to around 6 years, if the “red” scenario for emissions from the grid is used for the Living
512 Lab and Skarpnes cases. A constant emission factor, namely the Norwegian “ZEB factor” of 132 grams CO₂
513 eq/kWh showed payback times of 8, 15 and 18 years for the three systems. If we assume Norwegian hydropower
514 emissions of 20 grams CO₂eq/kWh, as an average for local grid emissions, then the modules do not payback
515 emissions within their 30 year service lifetime. Furthermore, when looking 30 years into the future, the emissions
516 from the Skarpnes system are likely to be reduced from around 80 to 20 grams CO₂ eq/kWh.

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