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# TECHNICAL REPORT

SUBJECT/TASK (title)

**USE OF ELECTRIC HIGH POWER EQUIPMENT  
DURING WELL INTERVENTION WITH DC CURRENT**

CONTRIBUTOR(S)

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CLIENT(S)

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RESULT (summary)

## USE OF ELECTRIC HIGH POWER EQUIPMENT DURING WELL INTERVENTION WITH DC CURRENT

Investigation to confirm that there not will occur dangerous voltage drops in the platform construction during wire line operations with a voltage up to 1500 V and 25 A DC.

Wire line cables used to well intervention consist of a steel wire with inlaid conductors. The return path of the current is mainly the construction and earth system of the platform. This is not according to the prevailing regulations.

The results of the voltage measurements confirm that it is safe to do well operations with currents up to 25 A DC, if the recommendations for the electrical equipment and the earth connections to the grease injection head are fulfilled. According to the regulations (FEA-M 1990 and others) the limit for low voltage is 1500 V DC.

At a current of 15 A the voltage drop in the platform construction was 60 mV and it will be about 100 mV at 25 A.

The present report is a supplement to EFI report TR A4596 "Bruk av enlederkabel under brønnintervenering", november 1997. EFI TR A4596 approaches in principle the same problem but using an AC power supply.

Similar conditions as to wire line operation exist when coil tubing is used with electrical tools. In this case the same safety requirements has to be fulfilled. Instead to the grease injection head the earth connection is to the upper bushings where the coil is entering the slipper.

\* Rapporten er omklasifisert til åpen 27/1-04 etter oppdragsgivers ønske.

## KEYWORDS

SELECTED BY AUTHOR(S)	Offshore	Well intervention
	Wire line	Safety

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## **USE OF ELECTRIC HIGH POWER EQUIPMENT DURING WELL INTERVENTION WITH DC CURRENT**

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Similar conditions as to wire line operation exist when coil tubing is used with electrical tools. In this case the same safety requirements has to be fulfilled. Instead to the grease injection head the earth connection is to the upper bushings where the coil is entering the slipper.

## **1 BACKGROUND AND APPROACH TO THE PROBLEM**

For efficient well operation it is necessary with well intervention such as measurements and performing perforations, plugging, etc. The transmission of measured signals and power requires cables with as little cross section as possible to overcome the pressure of the well.

Wire line cables consist of one conductor or several conductors, usually connected in parallel during high power operations, inlaid in a steel wire. The operating current uses the casing of the well and the earth system of the platform as return path. Due to practical and technical problems it is not possible to fulfil the requirements of the regulations. The wire line cables would get a large diameter due to the necessary copper cross section which would lead to problems to overcome the pressure in the well. To avoid potential differences in the ground system of the platform an earth connection was implemented between the power supply and the grease injection head as a compensating effort.

According to the regulations for electrical equipment a cable shall consist of:

- conductors with insulation
- common metallic screen, which has to be grounded, operating current is not allowed in the screen
- an insulating layer on the outside of the screen

In addition the earth system shall not carry operating currents.

The intentions of this investigation is to prove that there is no danger with respect to contact voltage for the personnel and ignition of explosive gas mixtures, although the regulations are not fulfilled.

## 2 REGULATIONS

References to regulations:

“Regulations relating to electrical installations in the petroleum activities”, issued by the Norwegian Petroleum Directorate 08. January 1991, last amended 25 February 1998 with references to:

“Regulation for electrical installations - Maritime installations- FEA-M” 1990 and “Regulation for electrical installations of buildings etc.” 1991, both issued by The Norwegian Directorate for Product and Electrical Safety.

IEC Publication 60079-11 “Electrical apparatus for explosive gas atmospheres, Part 11: Intrinsic safety “i”, 1991-11.

IEC Publication 61892-7 “Mobile and fixed offshore units- Electrical installations, Part 7: Hazardous areas, 1997-05.

## 3 MEASUREMENTS AND RESULTS

The measurements were performed on Snorre TLP during a patchflex operation using a DC power supply. The maximum voltage and current are specified by the manufacturer:

Max. no load output voltage: 1410 V  
Max. output current: 21 A

During the patchflex operation the maximum voltage and current were 923 V and 14,8 A.

The maximum voltage drop at accessible current-carrying parts of the power supply is between the earth point of the voltage source (Drillflex container) and the cable at the well head where the wire line cable enters the grease injection head.

The maximum voltage difference between the wire line cable at the grease injection head and the earth point of the power supply at the Drillflex container was < 60 mV at 14,8A. There was only a very low current (<0.05A) in the steel armour of the accessible part of the cable. Figure no.1 in Appendix 1 shows a schematic diagram of the earth connections.

The voltage drop in the earth system was continuously logged during the whole Patchflex operation. The figures nos. 2-4 in Appendix 1 show the results of the voltage measurements.

Channel 2 in these records shows the voltage drop between the cable and the flow tubes in the grease injection head. Low voltage (<100 mV) is required to make sure that heat spots will not occur between the armour and the grease tubes which could reduce the mechanical strength of the cable.

Channel 3 in the records shows the maximum voltage drop in the earth system.

Peaks on the voltage measurements occurring each 15 min. are due to electromagnetic noise. Each 15 minutes the power supply was switched off to do temperature measurements and the switched on again. If necessary the value of the current was adjusted.

The polymerisation record data sheets of the operation shown in Tables 1 and 2 in Appendix 1 allow a correlation between operating current and voltage drop.

The maximum voltage drop between the earth point at the Drillflex container and the cable at the grease injection head did never exceed 60 mV.

## **4 EVALUATION OF SAFETY ASPECTS**

The following requirements to electrical installations are not fulfilled when using wire line cables during well intervention:

- The cable screen (the steel armour) can carry some operating current
- The cable has no insulating sheath

Under such conditions it is possible that:

- personnel may come in contact with live parts of the power supply
- unintended connections may occur between the cable and the deck, for example due to tools or other metallic objects. This may lead to electric sparks if the voltage and current are high enough

The maximum values for currents in the steel armour of the cable and for voltage differences are < 100mA respectively 100mV at the limits given introductorily (1500V, 25A, DC).

Under such condition no danger with regard to contact voltage exists.

To evaluate danger of ignition of explosive gas mixtures Table no. 1 compares the measured values of current and voltage with the limits for intrinsic circuits given in FEB,1991,§808.7.4.3 and IEC Publication 60079-11, 1991.

Table no. 1 compares measured values of voltage and current with the limits given in different regulations. Appendix 2 contains detailed references to regulations and standards.

Table no. 1: Comparison of measured values and the limits in different regulations and standards.

	Requirement in FEB 1991	Requirement in IEC 60079-11 <sup>(*1)</sup>	Measured values <sup>(*2)</sup>
Voltage	<1.2 V	< 24 V	< 100mV
Current	< 100 mA	< 950 mA	< 100mA
Power	<25 mW		< 10 mW

- (\*1) Assumption
- The inductance of the circuit given by the wire line cable and the platform does not exceed 100  $\mu\text{H}$ . It is realistic to assume an inductance of 1  $\mu\text{H}$  per  $\text{m}^2$  of the loop between the cable and the deck.
  - The gas mixture is corresponding to group II A.
- (\*2)
- The values in the table are extrapolated from measured values at 14.8 A operating current to expected values at the maximum current of 25 A.

## 5 ROUTINES ON USING WIRE LINE CABLES

To secure correct electrical installation and safe performance of well intervention these recommendations has to be fulfilled:

- Earth points performed according to the regulations have to be installed at the collector ring box at the winch and at the power supply.
- The terminal of the power supply which is connected to ground may not have an independent fuse.
- An earth cable with a min. cross section of at least 70  $\text{mm}^2$  (Cu) has to be installed from the nearest earth point of the power supply to the grease injection head. (At coil tubing to or nearby the upper bushings) If the length of the cable does exceed 50 m, the cross section of the earth cable has to be increased corresponding to the resistance of the cable.
- The power supply has to fulfil relevant recommendations for short circuit currents and breaking time.

All installations have to be in accordance with relevant regulations for electrical installations off shore.

## 6 CONCLUSIONS

Due to practical problems it is difficult to meet the requirements of the regulations for electrical equipment during wire line operations. The measurements prove that no danger for personnel touching the wire line cable or for ignition of explosive gas – air mixtures exists, provided that the procedures mentioned in clause 5 are met. The measurements show that the values for voltage and current in accessible parts of the construction do not exceed the limits for intrinsic circuits in classified areas.

## **Appendix 1: The earth system and results of the measurements**

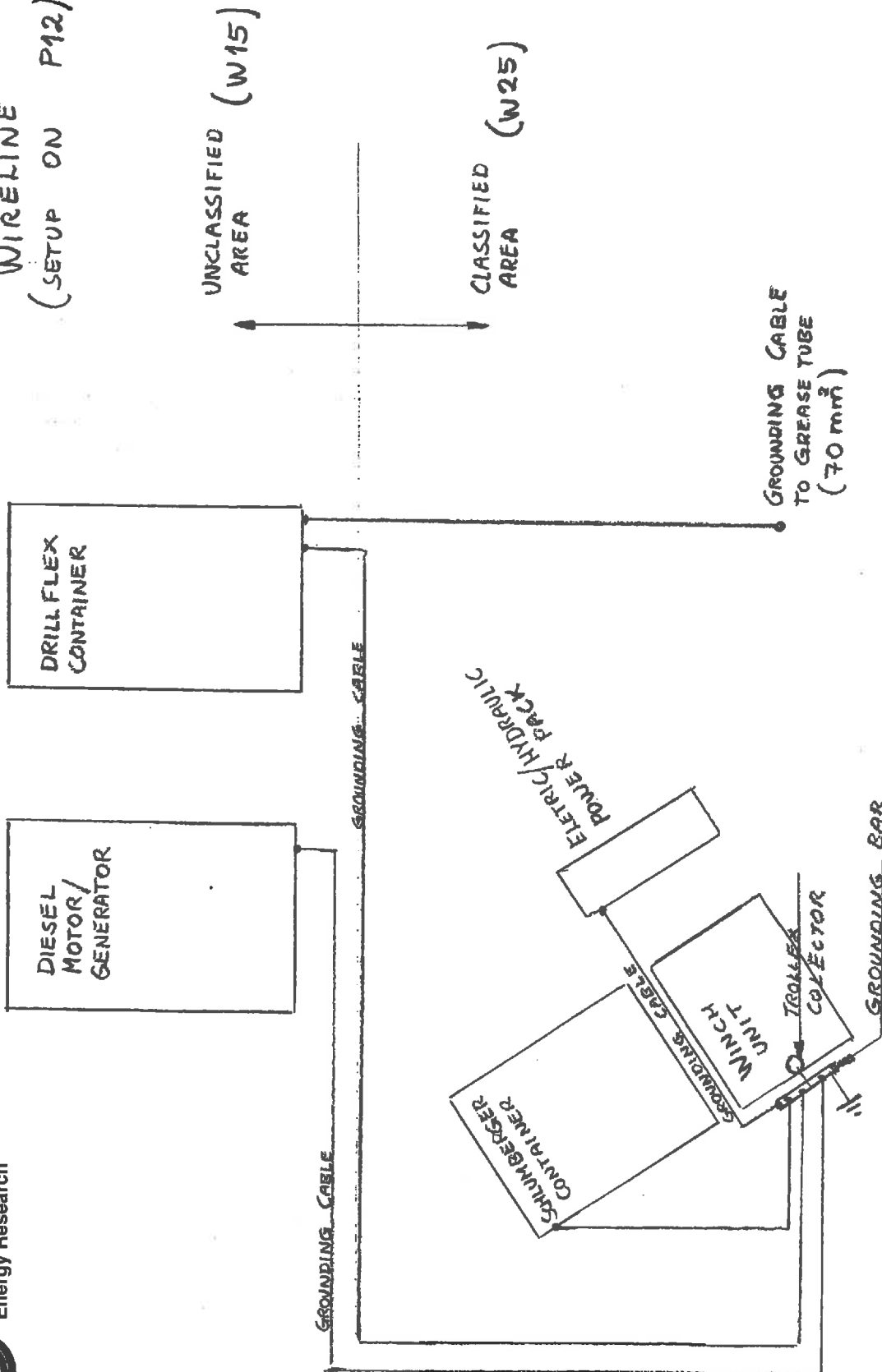
- Figure A1: Grounding system for wire line set up at Snorre TLP, Patchflex operation at P12 from Schlumberger
- Figure A2: Record of the voltage measurements, the first 210 minutes
- Figure A3: Record of the voltage measurements, from 210 to 440 minutes
- Figure A4: Record of the voltage measurements, from 440 to 700 minutes
- Table A1: Polymerisation record data sheet from Drillflex containing information of values of the operating current, the first 9 hours
- Table A2: Polymerisation record data sheet from Drillflex containing information of values of the operating current, from 09.00 to 12.45 hours



4.

SCHLUMBERGER  
WIRELINE

(SETUP ON P12)



**GROUNDING SYSTEM**  
22/1-99  
SINTEF

Figure A1: Grounding system for wire line set up at Snorre TLP, Patchflex operation at P12 from Schlumberger

09.02.1999 Skov TLP

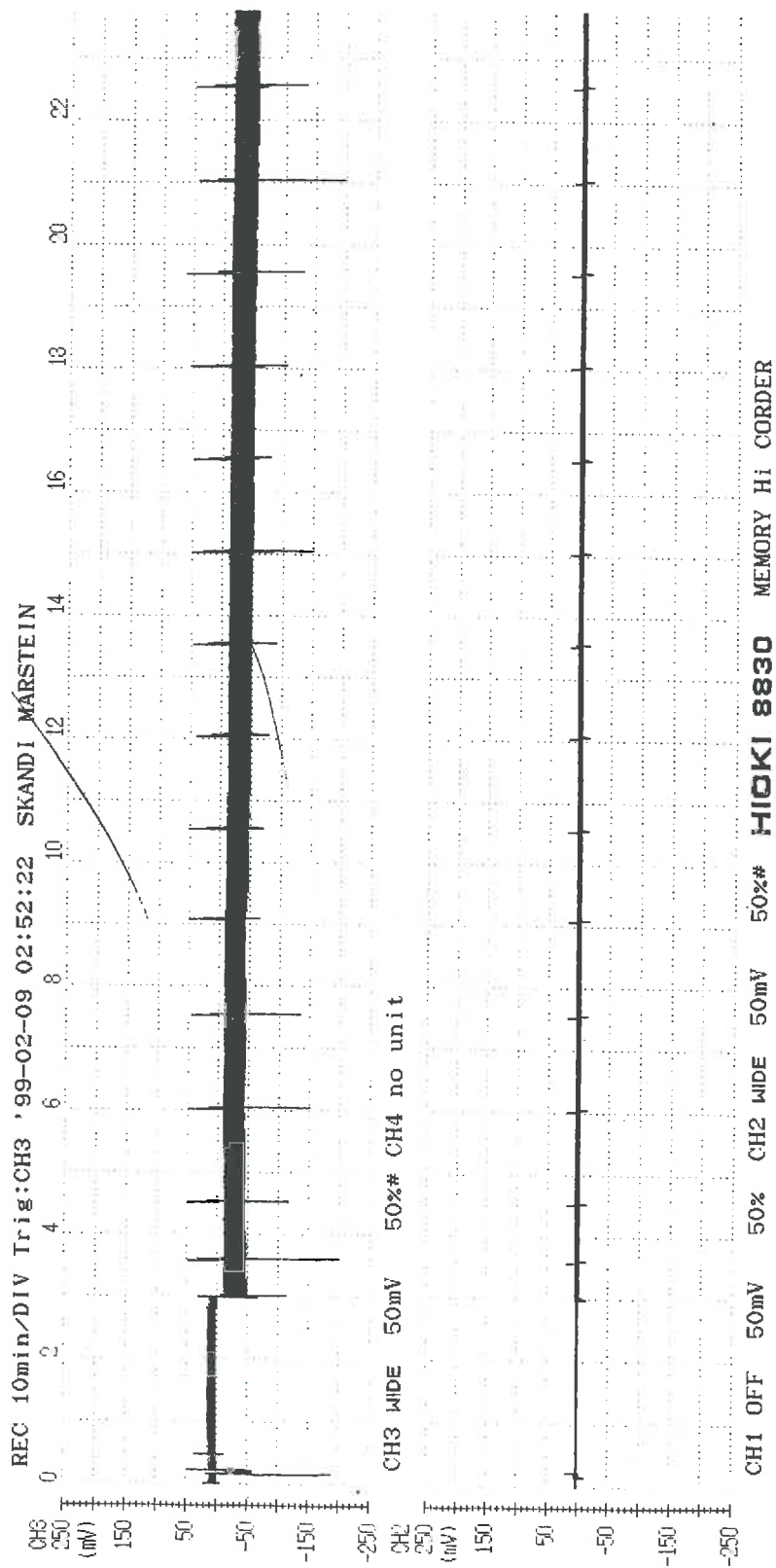


Figure A2: Record of the voltage measurements, the first 210 minutes

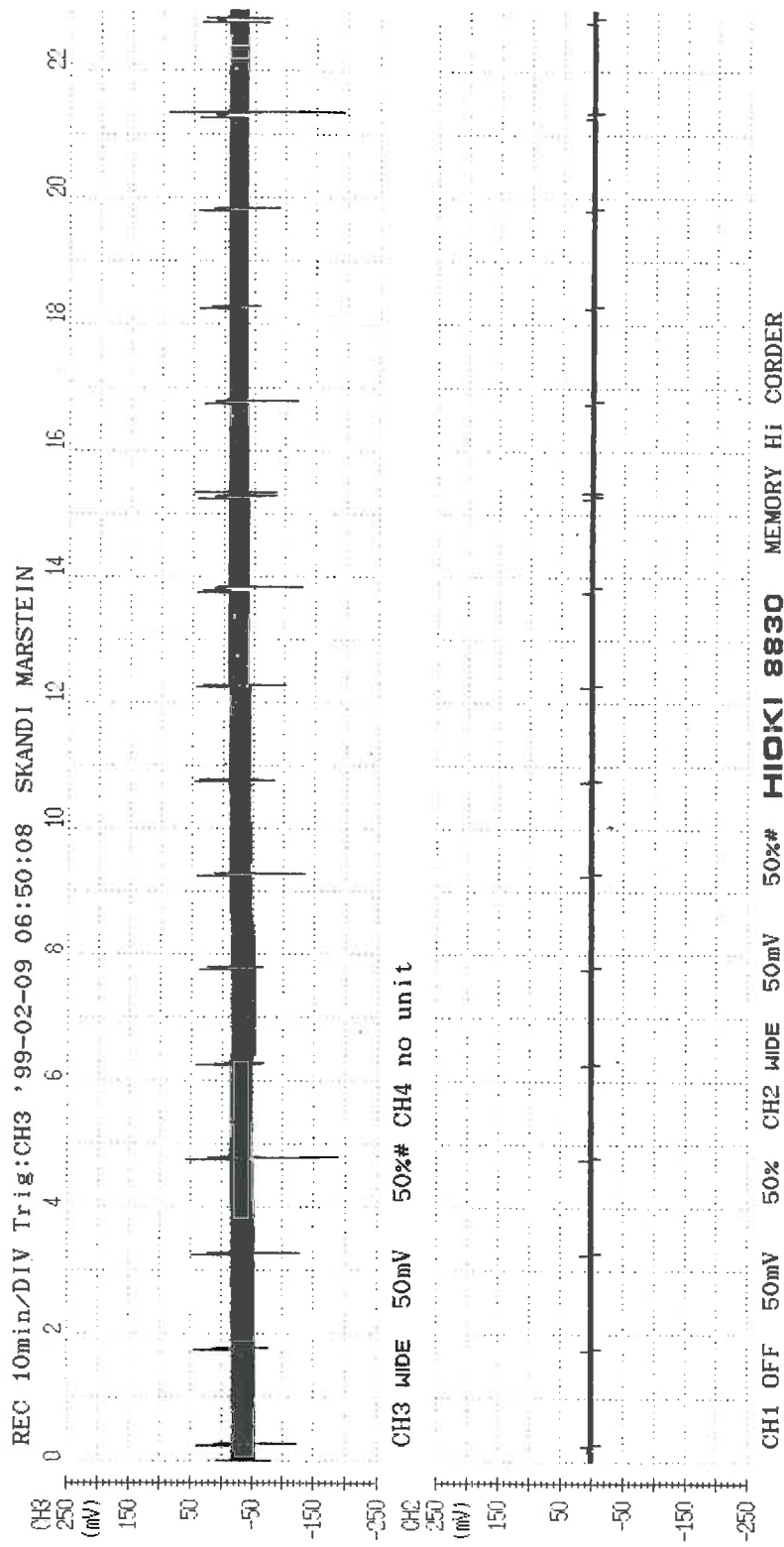


Figure A3: Record of the voltage measurements, from 210 to 440 minutes

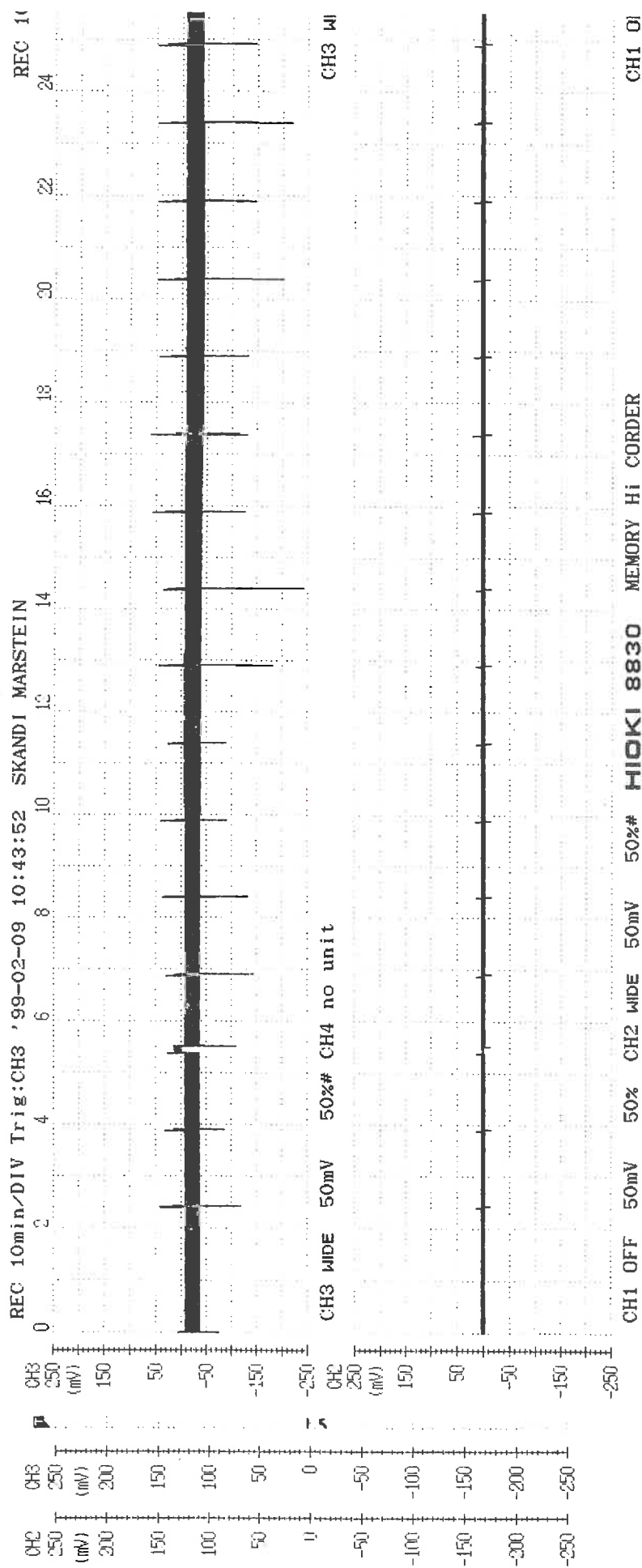


Figure A4: Record of the voltage measurements, from 440 to 700 minutes

# POLYMERISATION RECORD DATA SHEET

Software release: V 2.3

Company: SAGA

Field: Snorre

Well: 347 P12

Patch-Flex: 112

Job date: February 1999

Top 1700

Bottom 20000

Thermal capacity of ground Cp = 1700 J/kg.K

Lambda of Outer Buin 0.31 W/m.K

See Note  
Cas favorable Cp = 510 J/kg.K  
Cas défavorable Cp = 4500 J/kg.K

Time of record

record ↓	MAIN REAL VALUES						EVALUATED INDICATORS				THERMAL SIMULATION RESULTS										OTHER REAL VALUES					
	Computer time at beginning h:m:s	Computer time at end h:m:s	Phase polym. duration h:m:s	I Amps	U Volts	T1 Top °C	T2 Botom °C	POLYMERISATION PROGRESS		Hr	Composite temperature simulation	Necm. current Amps	Anticipated voltage Volts	Power per meter supplied w/m	Ground parameter (+ or -) %	T3 Electro. °C	T4 Puls °C	Pumping Yes or No	P after pumping Bar	Tension tool N	Comments					
								Top composite	Bottom composite																	
4:35	4:50	0:15	12.4	770	74.2	73.4	0	0			60.0	12.4	745	1000		66	59.0	15.0			1664	T1=Bottom; T2=Top				
4:50	5:05	0:30	12.4	770	80.8	78.2	0	0			67.8					61	59.0	16.5								
5:05	5:20	0:45	12.4	770	85.6	81.8	0	0			68.2					54	59.0	16.3			1527					
5:20	5:35	1:00	12.4	770	90.3	85.3	0	0			68.0					57	59.0	16.4			1507					
5:35	5:50	1:15	13	809	94.6	89.1	0	0			103.3	13.4	776	1175		59	59.0	16.5			1499					
5:50	6:05	1:30	13.5	839	101.2	93.0	0	0			107.7					59.5	59.8	15.8			1467					
6:05	6:20	1:45	13.5	840	105.7	95.9	0	0			111.6					59.5	59.8	15.8			1463					
6:20	6:35	2:00	13.5	840	110.3	98.4	0	0			116.0					59.6	59.8	16.0			1448					
6:35	6:50	2:15	14.1	877	115.9	101.8	0	0			120.9	14.1	816	1300		59.7	59.0	15.9			1437					
6:50	7:05	2:30	14.1	877	120.8	104.3	0	0			124.8					60	59.0	16.0			1432					
7:05	7:20	2:45	14.1	879	125.3	106.5	0	0			128.2					59.8	59.1	15.6			1409					
7:20	7:35	3:00	14.1	881	128.5	108.5	0	0			131.4					60	59.0	15.5			1411					
7:35	7:50	3:15	14.6	909	134.5	111.1	4	0			136.6	14.8	847	1400		60	59.0	15.4			1410					
7:50	8:05	3:30	14.6	909	138.7	113.0	7	0			138.9					60.3	59.4	15.6			1395					
8:05	8:20	3:45	14.6	909	143.5	114.6	12	0			143.0					60.4	59.4	15.4			1411					
8:20	8:35	4:00	14.8	909	146.0	115.9	17	0			146.9					60.5	60.5	15.3			1395					
8:35	8:50	4:15	14.8	923	148.7	117.7	22	0			148.1	14.5	837	1370		61	60.0	14.4			1400					
8:50	9:05	4:30	14.7	910	152.4	118.8	27	0			150.6					61	60.0	15.3			1389					
9:05	9:20	4:45	14.5	902	154.8	119.1	33	0			152.8					61	60.0	14.2			1408					
9:20	9:35	5:00	14	870	158.0	118.4	39	0			155.0					61	60.0	13.8			1400					
9:35	9:50	5:15	13.5	840	157.7	117.3	45	0			156.6	12.7	733	1050		60.7	59.9	8.6			1395					
9:50	10:05	5:30	12.4	770	157.7	117.3	51	0			159.5					60.7	59.9	8.6								
10:05	10:20	5:45	12.4	770	162.4	112.7	1	0			161.0					60.7	59.8	2.2	12.8		1472					
10:20	10:35	6:00	12.4	771	166.5	114.1	63	0			161.6					60.8	60.0	2.2	13.0		1466					
10:35	10:50	6:15	11.7	731	165.1	112.3	69	0			162.6	11.5	667	870		60.8	60.0	2.2	12.4							
10:50	11:05	6:30	11.5	714	153.8	110.8	74	0			164.1					61	60.0	2.0	14.0		1479					
11:05	11:20	6:45	11.5	715	155.4	110.8	80	0			167.9					60.5	60.0	2.0	14.2		1471					
11:20	11:35	7:00	11.5	714	162.2	108.7	86	0			168.0					61	60.0	2.6	12.5		1473					
11:35	11:50	7:15	11.5	715	161.3	108.2	91	0			168.0	11.5	667	870		61	60.0	2.9	13.1		1455					
11:50	12:05	7:30	11.5	715	160.8	108.0	96	0			168.2															
12:05	12:20	7:45	11.5	715	160.6	107.1	102	0			168.4					60	60.0				1368					
12:20	12:35	8:00	11.5	718	160.8	107.4	107	0			168.6					60	60.0	2.1			1341					
12:35	12:50	8:15	11.5	714	156.0	107.0	112	0			168.6	11.5	667	870		61	60.0	1.0	14.0		1491					
12:50	13:05	8:30	11.5	713	149.2	106.3	117	0			168.2					61	60.0	6.5			1498					
13:05	13:20	8:45	11.5	713	149.2	106.2	122	0			169.6					60.4	59.8	4.6			1434					
13:20	13:35	9:00	11.5	718	168.3	108.4	127	0			169.9					60.3	59.8	4.0			1420					

Notes:

Pour le cas d'un tubing:

- Si la simulation est au dessus (Cas peu probable), le peu extérieure est plus isolante que prévue. Action: augmenter le lambda de la peau extérieure.

- Si la simulation est en dessous, on n'est pas en vrai tubing. Action: Passer en casing avec Cp du sol de l'ordre de 16.000 (à faire varier)

Lambda pour extérieure autour de 0.31 (à faire varier éventuellement si problème avec Cp soil)

Table A1: Polymerisation record data sheet from Drillflex containing information of values of the operating current, the first 9 hours

# POLYMERISATION RECORD DATA SHEET

Software release: V 2.3

Company: SAGA

Field: Snorre

Well: 34/7 P-12

Patch-Flex: 112

Job date: February 1999

See Note

Cas favorable Cps = 910 J/kg.K  
Cas défavorable Cp = 4500 J/kg.K

Thermal capacity of plastic: Cp = J/kg.K  
Viscosity of Outer Skin: W/m.K

Time of record

MAIN REAL VALUES				EVALUATED INDICATORS			THERMAL SIMULATION RESULTS						OTHER REAL VALUES						
Computer time at beginning h:mm	Computer time at end h:mm	Phase polym. duration h:mm	I Amps	U Volts	POLYMERISATION PROGRESS		HI	Composite temperature simulation	Neces. current Amps	Anticipated voltage Volts	Power per meter supplied w/m	Estimated shrinkage (%)	T3 Electro. °C	T4 Puls. °C	Pumping before pumping Bar	Pumping Yes or No	P after pumping Bar	Tension tool N	Comments
					Top composite	Bottom composite													
13:35	0:00	0:15	12	745.0	133	0		148.9	12.4	715	1000		60.4	59.7	0.3			1430	T1=Bottom; T2=Top
13:50	0:30	0:15	12	745.0	138	0		64.9					60.8	59.9	8.0			1417	
14:05	0:45	0:15	12.4	769.0	143	0		87.2					60.4	59.7	11.1			1356	
14:20	1:00	1:00	12.4	771.0	149	0		81.8					60.4	59.7	15.8			1361	
14:35	1:15	1:15	12.4	771.0	155	0		86.6	13.0	750	1100		60.4	59.7	15.7			1328	
14:50	1:30	1:30	13	809.0	160	0		101.6					60.4	59.7	15.6			1319	
15:05	1:45	1:45	13	809.0	166	0		105.4					60.4	59.7	15.8			1315	
15:20	2:00	2:00	13	809.0	172	0		108.9					60.5	59.8	15.8			1312	
15:35	2:15	2:15	13	807.0	179	0		112.1	12.4	715	1000		60.6	59.8	15.1			1312	
15:50	2:30	2:30	12.8	797.0	185	0		113.0					60.6	59.8	14.2			1305	
16:05	2:45	2:45	12.4	771.0	191	0		116.1					60.6	59.8	14.1			1279	
16:20	3:00	3:00	12	744.0	197	0		117.3					60.6	59.8	1.7			1297	
16:35	3:15	3:15	12	744.0	203	0		119.3	12.4	715	1000		60.5	59.8	1.7			1296	
16:50	3:30	3:30	12	745.0	209	0		121.3					60.6	59.9	1.6				
17:05	3:45	3:45	FIN DE PHASE					124.9					60.6	59.9	1.6				
17:20	4:00	4:00	209		209	0		126.6											
17:35	4:15	4:15	209		209	0		132.4	13.5	764	1200								
17:50	4:30	4:30	209		209	0		135.2											
18:05	4:45	4:45	209		209	0		137.6											
18:20	5:00	5:00	209		209	0		139.9											
18:35	5:15	5:15	209		209	0		142.0	13.5	764	1200								
18:50	5:30	5:30	209		209	0		144.0											
19:05	5:45	5:45	209		209	0		145.8											
19:20	6:00	6:00	209		209	0		147.6											
19:35	6:15	6:15	209		209	0		148.3	13.5	764	1200								
19:50	6:30	6:30	209		209	0		151.0											
20:05	6:45	6:45	209		209	0		152.6											
20:20	7:00	7:00	209		209	0		154.1											
20:35	7:15	7:15	209		209	0		155.6	13.5	764	1200								
20:50	7:30	7:30	209		209	0		157.0											
21:05	7:45	7:45	209		209	0		158.3											
21:20	8:00	8:00	209		209	0		158.7											
21:35	8:15	8:15	209		209	0		160.9	13.5	764	1200								
21:50	8:30	8:30	209		209	0		162.2											
22:05	8:45	8:45	209		209	0		163.4											
22:20	9:00	9:00	209		209	0		164.6											

Notes:

Pour le cas d'un tubing:

- Si la simulation est au dessus (Cae peu probable), le pressurisation est plus lente que prévue.

- Si la simulation est en dessous, on n'est pas en vrai tubing.

Table A2: Polymerisation record data sheet from Drillflex containing information of values of the operating current, from 09.00 to 12.45 hours

## **Appendix 2: References to national regulations for electrical installations and international standards**

### **Safety for personnel**

The question about danger for personnel which comes in contact with current carrying components was not investigated because the accessible voltages are very low ( $< 100$  mV).

### **Danger of ignition of explosive gas mixtures**

The consideration is based on:

“Regulations relating to electrical installations in the petroleum activities”, established by The Norwegian Petroleum Directorate, 1998.

Section 14 “Special technical and operational requirements” in this regulation refers to:

“Regulation for electrical installations – Maritime installations – FEA-M”, established by The Norwegian Directorate for Product and Electrical Safety, March 1990 and

IEC Publication 6189 “Mobile and fixed offshore units – Electrical installations –Part 7: Hazardous areas, 1997-05.

When writing EFI TR A4596, the investigation about use of ac power supplies to well intervention the IEC Pub. 61892-7 was not yet available and the consequences of this standard are so far not completely evaluated.

The regulations and standards mentioned above, refer to FEB § 808.7.4.3 or/and to IEC Pub. 60079-11 when giving limits for electrical values as current, voltage, etc. in hazardous areas.

According to FEB 1991, §808.7.4.3 it is not necessary to certify equipment not exceeding following values in areas class I with gasses of group II A:

- voltage: 1.2 V
- current: 0.1 A
- energy: 20  $\mu$ J
- power: 25 mW

The maximum current in the steel screen of the wire line cable, which can be short circuited to ground is  $< 0.1$  A and the voltage does not exceed 100 mV. This means that the maximum power is 10 mW.

To exceed the energy of 20  $\mu$ J the spark had to last for 2 ms. With this low currents and voltages it will be very difficult, probably impossible to generate a spark at all.



Figure 5 of IEC Pub. 60079-11 gives the lowest limit for ignition current under consideration of the inductance of resistive-inductive circuits with a primary voltage of 24 V DC. To estimate the inductance of a loop in air we may assume an inductance of 1  $\mu\text{H}$  per square meter of the loop. For a loop of 100  $\text{m}^2$  (equivalent to 100  $\mu\text{H}$ ), the minimum ignition current is 0.95 A for gas mixtures of group II A.

Figure A5 in Appendix 2 shows this curves.

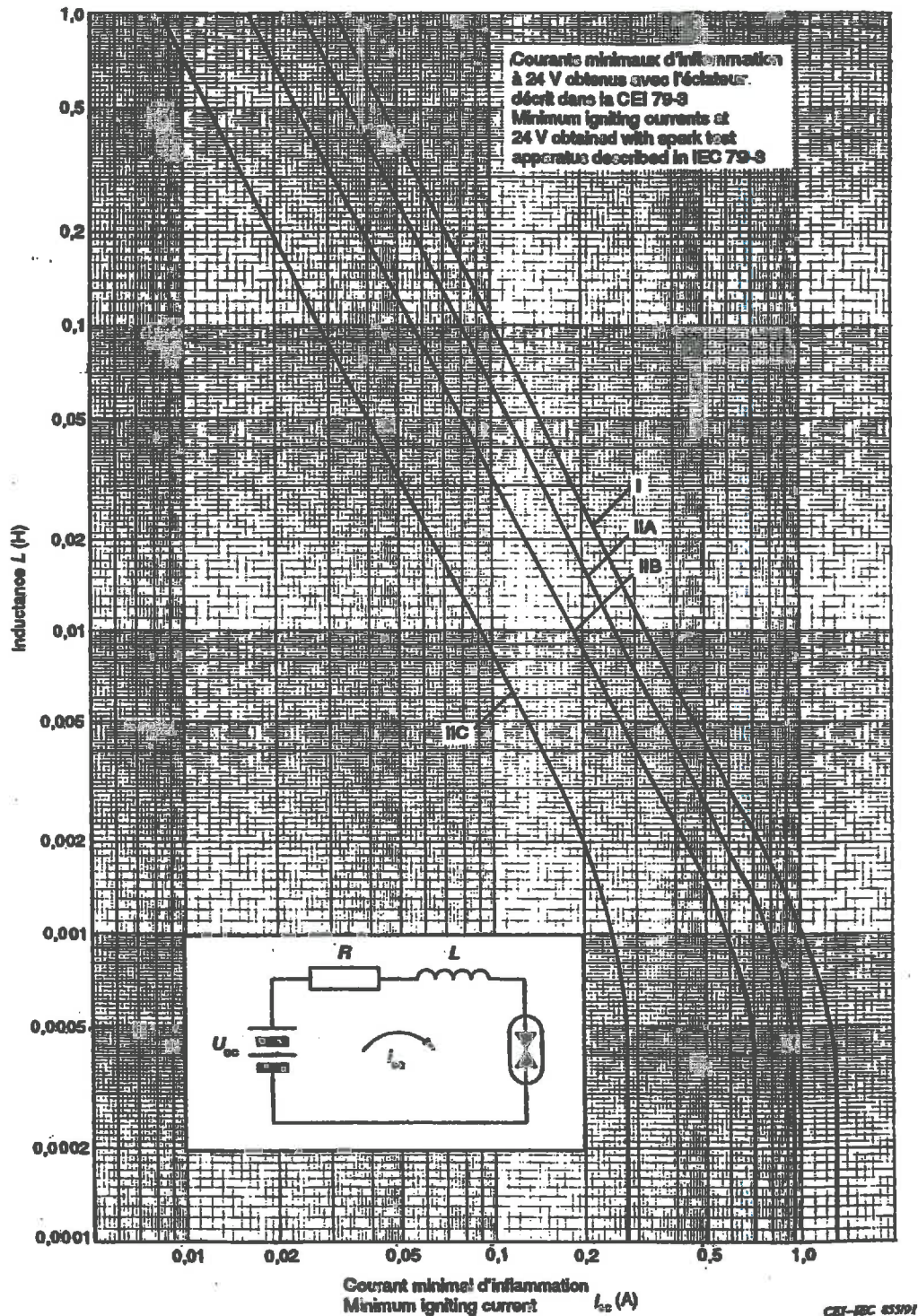


Figure A7: Minimum ignition currents of inductive circuits.



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