Partitioning of Non-ionic Surfactants Between CO₂ and 1

Brine 2

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7 Abstract: The partitioning of non-ionic surfactants in a CO₂/synthetic brine system was studied for a 8 selection of surfactants at reservoir conditions for CO₂ enhanced oil recovery and aquifer storage. Alkyl 9 and alkylphenol ethoxylates with different degrees of branching in their hydrophobic moiety were 10 chosen. Generally, higher temperature and pressure promoted increased solubility in CO2. Branching of 11 the hydrophobic moiety tends to favour CO₂ solubility (higher partition coefficient). Highly branched 12 moieties were found to hinder solubility probably due to a decrease of their conformational entropy. The 13 addition of an aromatic ring connecting the ethoxylate moiety and the hydrophobic moiety seemed to 14 have an adverse effect at lower temperatures. For two surfactants, the effect of concentration on 15 partitioning was also studied. The partition coefficient decreased for increasing concentrations until a 16 plateau was reached above the corresponding surfactant critical micelle concentration (CMC). This may 17 indicate micelle formation both in the CO_2 and in the aqueous phase.

18 Keywords: Mobility control of CO₂, foam, enhanced oil recovery, aquifer storage, surfactant 19 partitioning

20

21 **1. Introduction**

22 CO₂ is becoming a prominent solvent for different applications. Its foams and emulsions with water are 23 of interest due to its potential for various applications (Johnston and Rocha, 2009). Two large scale 24 applications are enhanced oil recovery (EOR) and subsurface sequestration. However, these methods 25 encounter various technical challenges. The relatively low density and low viscosity of CO₂ can lead to 26 gravity segregation and viscous fingering giving early CO_2 breakthrough and poor volumetric sweep 27 efficiency. The result of this may be low oil recovery (in EOR) and reduced utilisation of the storage 28 capacity (in CO₂ sequestration) (Solbakken et al., 2013; Tsau and Grigg, 1997).

- 29 Early breakthrough can be counteracted by decreasing the mobility of the CO₂. This can be achieved by
- 30 increasing the viscosity using additives to the CO₂ or by dispersing the CO₂ into another fluid (brine). It
- 31 is not easy to increase CO₂ viscosity. The additives (direct thickeners) must solubilize in CO₂ and
- 32 provide self-interactions that can give the desired viscosity enhancement. During decades efforts have
- 33 been made trying to find suitable additives (Enick et al., 2012). However, the best CO₂ additives found
- 34 are not practical due to their high costs and detrimental environmental impact.
- 35 The second method for decreasing CO₂ mobility is through creating dispersed systems. CO₂-in-brine
- 36 dispersions (hereafter called foams) may have high apparent viscosities depending on the surfactant
- 37 used. Foams can also be formed and stabilized by nanoparticles. Even though nanoparticles adsorb more
- 38 strongly at interfaces, larger energy input is required to form foam. This criterion is not met at reservoir
- 39 flow velocities which typically do not exceed few feet/day (except close to injection wells) (Binks, 2002;
- 40 Espinosa et al., 2010; San et al., 2016; Yu et al., 2012).
- 41 Surfactant-stabilized foam is so far the most promising CO₂ mobility reduction method. However, this
- 42 also faces several challenges. One potential problem is the presence of oil which may destabilize foam
- 43 through different mechanisms including spreading and entering phenomena (Manlowe and Radke, 1990;
- 44 Schramm and Novosad, 1990; Wasan et al., 1994). However, the sensitivity of foam to oil may have

- 45 both advantageous and disadvantageous consequences. During miscible CO₂ flooding, the foam may be
- 46 more stable in pores where the oil has already been displaced helping to divert CO_2 within the reservoir 47 to places where the oil is not displaced. There, the lamella will collapse and release CO_2 in the CO_2 /oil
- 47 to places where the on is not displaced. There, the famena will compse and release CO_2 in the CO_2/off 48 front. On the other hand, if the stability of the foam is sensitive to minute oil residues it can have an
- 49 adverse impact on foam propagation (Vassenden *et al.*, 2000).
- 50 Another challenge to face during surfactant-stabilized foam flooding is surfactant depletion due to
- adsorption on the pore walls of the reservoir rock. The adsorption will be determined by the pore wall
- 52 mineralogy and charge, type of surfactant, pH, temperature, ionic strength, electrolyte concentration
- (Bera *et al.*, 2013; Curbelo *et al.*, 2007). In traditional foam technology, the surfactant is transported in
 the denser water phase. At some distance from the injection well, the surfactant solution and CO₂ will
- 55 the denset water phase. At some distance from the injection wen, the suffactant solution and CO_2 with 55 segregate and foam cannot be formed. If the surfactant is transported in the CO_2 , foam may be formed
- 56 wherever gas and water coexist.
- 57 Mobility control can also be beneficial for aquifer storage of CO₂. In order to increase the storage
- 58 capacity and to avoid excessive build-up of pressure, formation water must be produced from the
- 59 formation. The total storage capacity of a formation can be significantly increased if the volumetric
- 60 sweep is improved. This can reduce the total storage cost if low-cost CO_2 soluble surfactants giving
- 61 suitable mobility control at low flow rates can be identified (Grimstad *et al.*, 2018).
- 62 Efforts for finding and developing CO₂ soluble surfactants have been made since early 1990. The first 63 effective surfactant developed was fluorinated (Hoefling *et al.*, 1991). These types of surfactants are 64 impractical due to their environmental impact and high costs. Since then, the effort has been focused on 65 finding non-fluorinated surfactants. Due to the amphiphilic nature of surfactants, CO₂-soluble
- 66 surfactants will also dissolve in the aqueous phase and thus, partition between both phases. CO₂
- 67 solubility and partitioning has been studied for several surfactant types such as dioctyl sodium
- 68 sulfosuccinates (AOT) (Le *et al.*, 2008), linear and branched alkylphenol ethoxylates (McLendon *et al.*,
- 69 2012; Xing *et al.*, 2010), branched alkyl ethoxylates (Xing *et al.*, 2012), ethoxylated cocoamines (Chen
- 70 *et al.*, 2012) and triblock copolymer surfactants (Adkins *et al.*, 2010).
- However, the partition and solubility studies reported in the literature only give values for specific temperatures, pressures and surfactant concentrations, and it is difficult to find data on how the partitioning is influenced by changes in these variables for CO_2 -brine systems.
- 74 Injection of surfactant through the CO₂ phase was introduced by Le *et al.* with promising core flooding
- results. With this novel injection strategy, the surfactant dissolved in the CO₂ phase will partition to the
- formation brine and foam can be formed in-situ, obtaining a delayed CO₂ breakthrough and an increased
- 77 oil recovery (Le *et al.*, 2008).
- 78 Knowing how partitioning is affected by pressure and temperature is important for foam flooding since
- 79 the mobility and strength of the foam depends on the surfactant concentration, which depends on
- surfactant adsorption onto rock and partitioning between the phases (Ashoori *et al.*, 2009). Partitioning
- 81 of surfactant and its concentration dependence are therefore important input data for a foam simulator.
- 82 The objective of the current work was to determine the CO₂ partition coefficients in CO₂-brine systems
- for a selection of commercially available non-ionic surfactants at variable pressures and temperatures
- relevant for CO₂ enhanced oil recovery and CO₂ aquifer storage on the Norwegian Continental Shelf.
- 85 The dependence of CO₂ partitioning with varying surfactant concentration was also addressed.

86 2. Materials and Methods

- 87 **2.1. Gas**
- 88 The CO_2 was obtained by AGA A.S. (99.7 %).

89 2.2. Synthetic seawater

- 90 The synthetic seawater (SSW) composition used in this study is shown in Table 1. The SSW was filtered
- 91 through 0.45 μm cellulose nitrate filters.

92 **Table 1.** Synthetic seawater composition.

Salt	Conc. [g/l]			
NaCl	23.612			
$CaCl_2 \cdot 2H_2O$	1.911			
MgCl ₂ ·6H ₂ O	9.149			
KCl	0.746			
Na ₂ SO ₄	3.407			

93

94 2.3. Surfactants

- 95 A selection of non-ionic surfactants was chosen for the CO₂ partitioning studies. The surfactants were
- 96 divided into two groups, alkyl ethoxylates and alkylphenol ethoxylates. Each group had hydrophobic
- 97 tails ranging from linear to highly branched alkyl groups. The surfactant chemical structures used are
- 98 described in Figure 1.





- 100 **Figure 1.** Surfactant chemical structures (EOn symbolizes the average number of ethoxy groups).
- 101 All surfactants were obtained from Sigma-Aldrich with a concentration of 100 wt.% of active material
- 102 except for Tergitol TMN 10, which was obtained with a concentration of 90 wt. % of active material.

103 3. Experimental

104 3.1. Cloud point determination

105 0.5 wt.% surfactant in SSW was placed in a water bath equipped with a temperature controller. The 106 temperature of the water bath was slowly increased using small increments until the cloud point of each

107 solution was observed.

108 3.2. Measurement of surfactant partitioning

109 Measurements of surfactant partitioning were performed in a high-pressure high-temperature pVT-cell

with an internal piston for pressure/volume control (DB Robinson). The cell temperature was controlled 110 111 by a heating cabinet with circulating air. A volume of 15 ml of aqueous surfactant solution was injected

112 into the cell kept at the desired temperature for the measurement. Afterwards, the cell was filled with

45 ml of CO₂ and the pressure was adjusted to the desired value. Once the cell was filled, the pressure 113

- 114 was kept constant by using a computer-controlled pump connected to the hydraulic side of the cell. The
- cell was tilted 50° 60° to increase the contact area between the phases. Then the system was left under 115
- 116 static conditions for 24 h.
- 117 After 24 h, a sample of approximately 6 - 8 ml of aqueous phase was extracted at a low rate, keeping
- 118 constant pressure inside the cell by moving the cell piston (assisted by the computer-controlled system).
- 119 Before collecting the sample, approximately 2 ml of sample were discarded. During the extraction
- 120 process, the system in the cell never exceeded 2 bar deviation from the target pressure. The extracted
- 121 sample was collected for further analysis.

122 3.3. Surfactant Analysis

- 123 The surfactant concentration in SSW was determined by HPLC using a LC-4A HPLC from Shimadzu.
- 124 The oven (Shimadzu CTO-2AS) was set at 50°C. The column used was a Supelcosil LC-18 (250 mm –
- 4.6 mm, 5 µm) and the samples were injected through a Rheodyne 7125 injector with a 20 µl loop. A 125 refractive index detector from Showa Denko K.K (RI SE-51) was used to detect the peaks. The
- 126

127 chromatograms were processed with the PowerChrom 180R system from eDAQ.

128 The eluent was prepared from measured amounts of methanol (HPLC grade from VWR) and water

(obtained from a purification system PURELAB-Option Q DV-25). The methanol:water volume ratio 129

- 130 used was 85:15 and the eluent had a concentration of 0.2 M NaNO₃ (analysis grade from Merck). The
- eluent was filtrated through a 0.45 µm nylon membrane and continuously degassed with helium. 131

132 3.4. Determination of partition coefficient

The partition coefficient, k_p , is determined by the expression in Eq. 1. 133

$$k_{p} = \frac{\frac{m_{sCO_{2}}}{m_{sCO_{2}} + m_{CO_{2}}}}{\frac{m_{sw}}{m_{sw} + m_{w}}}$$
(1)

- where, m_{sCO_2} is the mass of surfactant dissolved in CO₂, m_{CO_2} the mass of CO₂, m_{sw} the mass of 135 surfactant dissolved in the aqueous phase, and m_w the mass of aqueous phase. The solubility of water 136 137 in CO₂ and CO₂ in water were neglected.
- 138 Some initial tests were done with surfactant dissolved in distilled water (0.5 wt.%) and CO₂. The total 139 volume was 60 ml (15 ml aqueous phase, 45 ml of CO₂) and the experiments were carried at room
- temperature and 100 bar. In these tests, the aqueous samples were obtained as detailed above. 140
- Afterwards, a large and known volume of CO2 was extracted from the cell and flashed to ambient 141
- 142 pressure at a very low rate. The cell pressure was constant at 100 bar. The CO₂ extracted from the cell
- 143 was passed through a water trap. After the flash, the flow line from the cell to the trap was washed with

- 144 water. With known total masses of water and extracted CO₂ HPLC analysis of the water enabled the
- 145 determination of m_{sCO_2} . Then, m_{sCO_2} determined by HPLC was compared to m_{sCO_2} determined by mass
- 146 balance based on m_{sw} (Table 2).

147**Table 2.** Surfactant masses and partition coefficients determined by analysing both phases (HPLC) and only aqueous phase148(M.B.) for pure water/CO2 systems at room temperature and 100 bar.

Surfactant	M.B. <i>m_{sC02}</i> [g]	HPLC m_{sCO_2} [g]	M.B. <i>k</i> _p	HPLC k _p
Tergitol 15-S-9 (1)	0.031	0.031	0.28	0.28
Tergitol 15-S-9 (2)	0.034	0.029	0.33	0.28
Tergitol TMN 10(1)	0.028	0.026	0.23	0.23
Tergitol TMN 10 (2)	0.028	0.029	0.23	0.22

149

- 150 The two methods for determining the surfactant mass dissolved in CO_2 and the partition coefficient gave
- 151 same results. Thus, it was decided to proceed by only analysing the aqueous phase and determine m_{sCO_2}
- 152 from the surfactant mass balance. In this manner the measurements could be performed more rapidly.
- 153 In order to ensure that the systems were in equilibrium at the time of sampling, a series of sampling tests
- 154 were performed to determine the equilibration time required. It was observed that 20 h were enough for
- 155 the systems to have unalterable concentrations of surfactant in both phases, so it was decided that all
- 156 systems would age 24 h in the cell to ensure equilibrium.

157 **4. Results**

158 **4.1. Cloud point determination**

159 The cloud points for the surfactants used are shown in Table 3. For Brij L23 was not possible to

- 160 determine the cloud point due to its high value (above 100°C). The solution of 0.5 wt.% Brij C10 in
- 161 SSW was already cloudy at room temperature. This was unexpected since it is specified to be above
- 162 50°C (1 wt.% in water) from its producer. This surfactant was discarded for further measurements.

163 **Table 3.** Measured cloud points in SSW (0.5 wt.%).

Surfactant	Cloud Point [°C]			
Tergitol 15-S-9	50			
Tergitol NP 10	55			
Tergitol TMN 10	70			
Igepal CO 720	75			
Igepal CA 720	80			
Brij L23	> 92			

164

165 **4.2. Partition coefficients**

166 Determination of partition coefficients was carried out at pressures of 100, 200, and 300 bar, and at room 167 temperature, 40°C, and 80°C. The room temperature was typically around 20 - 22°C but is hereafter 168 referred to as 20°C. All measurements were repeated at least twice. The error bars in the figures show 169 the standard deviation for each experimental condition.

- 170 4.2.1. Linear alkyl ethoxylates
- 171 Brij L23
- 172 Brij L23 showed low CO₂ solubility at room temperature and at 40°C. Figure 2 depicts the surfactant
- 173 distribution in each phase for the studied conditions. More than the 90 wt.% of the surfactant remained 174 in the SSW at temperatures of 20° C and 40° C. However, the surfactant content in CO₂ increased
- significantly at pressures of 200 and 300 bar when the temperature was increased to 80°C. It can be

176 observed how the 85 wt.% of the surfactant migrated towards the CO_2 phase when the pressure was 177 200 bar. At 300 bar, the 93 wt.% was found solubilized in the CO_2 phase.



178

179 **Figure 2.** Surfactant distribution in SSW (blue) and in CO₂ (orange) for Brij L23.

Figure 3 depicts the partition coefficients, the surfactant concentrations in SSW, and the surfactant concentration in CO₂. At room temperature, the variation of the partition coefficient with pressure was almost negligible. At 40°C, a trend to increase the partition coefficient with increasing temperature was seen. A significant pressure effect on the partition coefficient was observed at 80°C. Note that the scale of the partition coefficients varies in Figure 3 and the following figures.



- Figure 3. Partition coefficients for Brij L23 (bars). In red line, surfactant concentration in SSW; in purple, surfactant concentration in CO₂.
- 188 The concentration of surfactant decreased in SSW and increased in CO₂ as the partition coefficient was
- 189 increased. However, at 80°C, this trend was not followed for the surfactant concentration in CO₂ for
- 190 pressures of 200 and 300 bar. The decrease in concentration was due to the constant volume condition
- during the measurements. At 300 bar, 45 ml of CO₂ corresponds to 33.9 g CO₂ (0.746 g/ml) while, at
- 192 200 bar, the mass of 45 ml CO_2 was 26.8 g (0.594 g/ml). The mass of surfactant solubilized into the CO_2
- 193 was, therefore, larger at 300 bar (0.069 g) compared to 200 bar (0.062 g). The increase of the CO_2 mass
- 194 when the system was at 300 bar, translates into a lower surfactant concentration.

195 4.2.2. Branched alkyl ethoxylates

196 *Tergitol 15-S-9*

197 Of all surfactants studied in this work, Tergitol 15-S-9 showed the highest partition in CO₂ at room

temperature. At 100 bar, 47 wt.% of the surfactant solubilized into the CO₂ (Figure 4). A temperature

199 increase from 20°C to 40°C did not promote any significant variation. When the temperature was

- increased further approaching the cloud point (2°C below), a significant solubility increase in the CO_2
- 201 phase was observed. Increased pressure increased the surfactant preference for the CO_2 phase. Both at 202 200 bar and 300 bar the partition towards the CO_2 phase increased significantly with increased
- 202 1200 bar and 500 bar and 48°C, only 0.9 wt.% of the surfactant remained in SSW.
- 200 temperature. Fit 500 our and 10 C, only 0.5 wei/0 of the surfactant remained in 55



204



The partition coefficient increased as temperature and pressure increased (Figure 5). At 48°C, no significant variation of the surfactant concentration in SSW was observed at 100 bar and 200 bar. However, a significant decrease in the surfactant concentration in the CO_2 was observed at these conditions. This decrease was partly a consequence of density effects, as explained before. As seen in Figure 4, the surfactant content in the CO_2 phase decreased from 88 wt.% (100 bar) to 86 wt.% (200 bar). Due to the mentioned effect, the decrease in the concentration was from 0.34 wt.% to 0.18 wt.%.





Figure 5. Partition coefficients for Tergitol 15-S-9 (bars). In red line, surfactant concentration in SSW; in purple, surfactant concentration in CO₂.

215

216 Tergitol TMN 10

217 Tergitol TMN 10 also exhibited a preference for the CO₂ phase. The surfactant solubility in the CO₂

218 phase increased with pressure (Figure 6). Increased temperature also promoted surfactant partitioning

towards the CO_2 phase except at 100 bar when the temperature was increased from 20°C to 40°C where

220 the surfactant content in the CO_2 decreased from 39 wt.% to 16 wt.%. At 69°C, the residual surfactant

in SSW decreased to 2.6 wt.%, 2.1 wt.% and 1.3 wt.% at 100 bar, 200 bar and 300 bar, respectively.

222 Tergitol TMN 10 was highly CO₂-philic at this temperature.



223

Figure 6. Surfactant distribution in SSW (blue) and CO₂ (orange) for Tergitol TMN 10.

The partition coefficient increased as pressure increased for 20° C and 40° C (Figure 7). However, at 100 bar the partition coefficient decreased when the temperature increased from 20° C to 40° C. At 69° C, a deviation from this trend was observed. The highest coefficient was obtained at 100 bar. When the pressure was increased to 200 bar, the coefficient decreased significantly. A further increase of pressure to 300 bar resulted in an increased partition coefficient. The surfactant concentration in the CO₂ phase decreased. Meanwhile, the surfactant content in the same phase increased (Figure 7 and Figure 6). This observation is explained by the density effect as explained previously.



Figure 7. Partition coefficient for Tergitol TMN 10 (bars). In red line, residual surfactant concentration in SSW; in purple,
 surfactant concentration in CO₂.

- 4.2.3. Linear alkylphenol ethoxylates
- 236 Igepal CO 720
- 237 The preference of Igepal CO 720 for the CO₂ phase generally increased as both temperature and pressure
- 238 increased (Figure 8). One exception was observed at 100 bar, however. When the temperature increased
- 239 from 20° C to 40° C the surfactant content in the CO₂ phase decreased. This surfactant had preference for
- 240 the CO_2 phase as the temperature approached its cloud point (75°C, see Table 3). At this temperature,
- the content of surfactant in SSW was 3.0 wt.%, 0.8 wt.%, and 0.4 wt.% at pressures of 100 bar, 200 bar,
- and 300 bar, respectively.



243

Figure 8. Surfactant distribution in SSW (blue) and in CO₂ (orange) for Igepal CO 720.

245 The partition coefficient followed the expected trend, it increased with temperature and pressure (Figure

246 9). The same exception was observed at 100 bar at temperatures of 20°C and 40°C, where the

247 partitioning coefficient decreased for increasing temperature.





Figure 9. Partition coefficient for Igepal CO 720 (bars). In red line, residual surfactant concentration in SSW; in purple,
 surfactant concentration in CO₂.

4.2.4. Branched alkylphenol ethoxylates

253 Igepal CA 720

254 Igepal CA 720 showed similar surfactant distributions as Igepal CO 720. The same observations at

- 255 100 bar and 40° C were made (Figure 10) as the preference for the CO₂ phase decreased compared to
- 256 20°C. At 78°C, most of the surfactant was dissolved in the CO₂, 97.8 wt.% (100 bar), 98.2 wt.%
- 257 (200 bar), and 98.9 wt.% (300 bar).





Figure 10. Surfactant distribution in SSW (blue) and in CO₂ (orange) for Igepal CA 720.

The partition coefficient followed the expected trend at 20°C and 40°C. It increased as both temperature and pressure increased with the exception of 100 bar (Figure 11). At 78°C, the partitioning coefficient decreased when the pressure was increased from 100 bar to 200 bar. The reduced partitioning coefficient, as well as the diminishing concentration in the CO_2 phase, is caused by the density effect

264 explained previously.



²⁶⁵

Figure 11. Partition coefficient for Igepal CA 720 (bars). In red line, residual surfactant concentration in SSW; in purple,
 surfactant concentration in CO₂.

268 Tergitol NP 10

Tergitol NP 10 did not follow any clear trend in its distribution between CO_2 and SSW (Figure 12). At 20°C, the preference for the CO_2 phase increased as the pressure was increased. At 40°C, the CO_2

distribution was higher 100 bar, lower for 200 bar, and higher for 300 bar, compared to 20°C. The lowest

272 content in CO_2 was observed at 40°C and 200 bar where only 20 wt.% of the total surfactant was

273 solubilized in the CO_2 phase. The largest content of surfactant in CO_2 was at 53.7°C both for 200 bar

and 300 bar, where approximately 60 wt.% of the surfactant was in the CO_2 phase.



275



At 20°C, the partition coefficient increased with pressure in accordance with the relative surfactant content. The largest coefficient was observed at 40°C and 100 bar (Figure 13). At 200 bar the coefficient decreased compared to 100 bar and increased when the pressure was increased to 300 bar. At 53.7°C, right below its cloud point, an opposite trend when compared to 40°C was observed. The coefficient increased from 100 to 200 bar and decreased again when the pressure was 300 bar.



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Figure 13. Partition coefficient for Tergitol NP 10 (bars). In red line, residual surfactant concentration in SSW; in purple,
 surfactant concentration in CO₂.

285 **4.3. Effect of concentration on partitioning**

- 286 The effect of surfactant concentration on the partitioning was also studied for two surfactants, Tergitol
- TMN 10 and Brij L23. The results are depicted in Figure 14. The concentrations plotted are the residual

concentration in SSW after equilibration at 40°C. The pressures used were 100, 200, and 300 bar.

For both surfactants, the increase of pressure promoted partitioning towards the CO_2 phase. However, as the concentration of surfactant in SSW increased, the partition coefficients decreased until plateau

- values were reached (Figure 14). At 100 bar the partition coefficient for Tergitol TMN 10 exhibited an
 almost constant value (Figure 14.a) seemingly unaffected by concentration.
- 293 The partitioning coefficients were fitted to the exponential functions of the form:
- 294

$$k_n = A + Be^{-C \cdot Conc} \tag{2}$$

where k_p is the partition coefficient, *Conc* is the surfactant concentration in SSW expressed in wt.%, and *A*, *B*, and *C* are empirical constants determined by the least-squares non-linear regression (Table 4).

Table 4. Equation 4 empirical constants determined for Tergitol TMN 10 and Brij L23.

Tergitol TMN 10			Brij L23				
	Α	В	С		Α	В	С
100 bar	0.1944	0.1390	4.3653	100 bar	0.0069	0.0518	5.7471
200 bar	0.2897	1.2740	4.3653	200 bar	0.0052	0.0439	2.2624
300 bar	0.5929	3.9281	5.9617	300 bar	0.0155	0.1054	4.3842

298

Figure 14 depicts the partition coefficient as a function of the surfactant concentration in SSW at equilibrium. The model gives a fair fit for all measurements.



301



305

306 **5. Discussion**

The surfactants selected for this research can be classified into two groups, alkyl ethoxylates and alkylphenol ethoxylates. Each group have similar ethoxylation numbers (except Brij L23) with carbon tails varying from linear to more branched structures. Nonetheless, a small variation on the CO₂-philic moiety can have an important impact on the partition between aqueous and CO₂ phase. Also, some trends can be identified. One constant observation in all measurements (excepting Tergitol NP 10) was a decrease in the CO₂ solubility as temperature increased from 20°C to 40°C at 100 bar.

314 **5.1.** Alkyl ethoxylates

The partition in CO₂ was generally promoted as the degree of branching increased for the alkyl 315 ethoxylates. However, at temperatures up to 40°C, highly branched carbon chains could cause a 316 317 solubility decrease in CO₂. This could be explained by an increase in the "stiffness" of the CO₂-philic 318 moiety. Thus, as the solubility increases by the effect of increasing the methyl branching, it is counteracted by a decrease of its conformational entropy, according to Flory and Huggins (Flory, 1953). 319 320 Above 40°C, Tergitol TMN 10 obtained a larger preference for the CO_2 phase than Tergitol 15-S-9. 321 However, the highest temperatures studied were not the same for both surfactants as the highest 322 temperature measured for each surfactant is limited by their cloud point.

- Brij L23, the highly hydrophilic non-branched linear alkyl ethoxylate, the partitioning decreased as temperature increased for 100 bar. This observation is in agreement with the research reported by Chen
- 325 *et al.* for similar surfactants at 117 bar for 24 and 40°C (Chen *et al.*, 2015). They explained it as a
- 326 lowered solvent strength of CO₂, which reflected a lowered tail solvation due to the decrease of density
- and a weakened hydrogen bonding between the head groups due to the temperature increase. However,
 the opposite trend was observed at pressures of 200 and 300 bar for increasing temperature. Here, as
- CO_2 density decreased with increasing temperature, the surfactant solubility in CO_2 increased. Thus,
- 330 this observation cannot be explained by the lowered solvent strength and decreased tail solvation in CO₂.
- 331 A plausible explanation for the increased partitioning is that as solubility in the aqueous phase is
- 332 decreased with increasing temperature, surfactant partitions to the CO₂ phase and eventually starts
- 333 forming micelles. Thus, even if tail solvation in CO_2 is reduced, surfactant partitions to the CO_2 and
- increases the micelle concentration.
- 335 A similar observation was made for Tergitol TMN 10 at 100 bar, where partition coefficient decreased
- as temperature increased from 20 to 40°C. However, a further increase of temperature to 69°C, just
- 337 below systems cloud point, drastically increased the coefficient. Close to the cloud point, the weakened
- 338 hydrogen bonding between ethoxy-groups and water would favour surfactant migration towards CO₂.

339 5.2. Alkylphenol ethoxylates

- 340 Generally, increased pressure and temperature contributed to larger partition coefficients also for the 341 alkylphenol ethoxylates. At 100 bar, when the temperature was increased from 20°C to 40°C, the same 342 decrease in the partition coefficient observed with alkyl ethoxylates was also noticed.
- Both Igepal CO 720 and Igepal CA 720 had similar solubilities into the CO_2 , meaning that high ramification of the CO_2 -philic moiety did not have a major effect on their partition. Igepal CO 720 is a linear alkylphenol ethoxylate with 9 carbons on its hydrophobic tail. Igepal CA 720 contains 8 carbons but arranged in a highly ramified structure as it can be seen from Figure 1. It is also possible that the aromatic ring in the CO_2 -philic moiety influenced the partitioning. From the comparison between alkyl ethoxylates and alkylphenol ethoxylates, it is observed that the presence of a benzene ring in the CO_2 philic moiety has a slight detriment on its solubility and partitioning into CO_2 when temperatures were
- 350 not close to their respective cloud point.
- 351 For both surfactants, a decrease in the partition coefficient was observed at 100 bar when the temperature
- 352 was increased from 20 to 40°C. Further increase of temperature increased the coefficient, the same
- 353 observation noticed for the branched alkyl ethoxylates. The variations on the partitioning as pressure 354 and temperature are varied can only be explained by the balance between tail solvation in CO₂,
- micellization in CO_2 , and strength variation of the hydrogen bond interactions between water molecules
- and hydrophilic headgroups.
- 357 Tergitol NP 10 can be considered as a medium branched alkylphenol ethoxylate. This surfactant did not
- 358 follow apparently any specific trend. When the temperature was increased from 20 to 40°C the partition
- 359 coefficients at 200 and 300 bar were reduced, while it increased for 100 bar. At 53°C, the effect was the
- opposite; the partition coefficients increased at 200 and 300 bar but decreased at 100 bar (Figure 13).

- 361 Compared to the other alkylphenol ethoxylates, Tergitol NP 10 had a low partition coefficient even
- when the temperature was 2°C below its cloud point. For all studied conditions, the partition coefficient never was above 1, obtaining the largest partition at 53.7°C and 200 bar ($k_p = 0.68$). Hence, Tergitol
- hever was above 1, obtaining the largest partition at 53.7°C and 200 bar ($k_p = 0.08$). Hence, Tergitor
- 364 NP 10 was the surfactant with the lowest observed CO₂ solubility in the study, the very hydrophilic Brij L23 excluded. According to the conformational entropy approach, this surfactant should have
- 366 obtained the largest CO₂ solubility among the studied alkylphenol ethoxylates. However, this was the
- 367 case only for the measurements at 20°C and the measurement of 100 bar at 40°C, where the partition
- 368 coefficient was larger. Thus, the partitioning behaviour of this surfactant could not be properly 369 explained.

370 **5.3. Effect of concentration on partitioning**

- 371 In an ideal system, chemical components should have concentration-independent partition coefficients, but for surfactants, there is a strong concentration dependence. Harusawa et al. studied the distribution 372 373 of octylphenol ethoxylates with different ethoxylation between isooctane and water system (Harusawa et al., 1980). For high ethoxylation numbers (EO 6 and 8) the surfactant concentration in the oil 374 375 increased up to the CMC and then remained constant for higher surfactant concentrations in the water. For a low ethoxylation number (EO 4) the surfactant in the water phase remained constant after the 376 377 CMC was reached, whereas the concentration in the oil increased. This indicated that micelles were 378 formed in the oil phase. For an intermediate ethoxylation number (EO 5), the concentrations in both 379 phases remained constant after the CMC was reached and a separate surfactant-rich phase was formed. Similar behaviour with constant concentrations in the oil phase (EO 6) or water phase (EO 8) after 380 381 reaching the CMC was observed in a system composed by water and cyclohexane using nonylphenol
- 382 ethoxylates (Harusawa et al., 1980; Harusawa and Tanaka, 1981).
- 383 The systems studied in this work exhibited different behaviour. The continuous increase of the surfactant
- 384 concentration in the CO₂ phase beyond their respective CMCs, as it can be seen in Figure 15, has already
- been observed and discussed (Balcan and Anghel, 2005). They noticed a slope change of the partition
- isotherm at the CMC studying systems composed of n-hexane, water, and a commercial nonylphenol ethowalete with an evenese EQ number of 10 as a surfactory. This behaviour resembles the one from
- 387 ethoxylate with an average EO number of 10 as a surfactant. This behaviour resembles the one from 388 surfactant mixtures, where the partitioning increases beyond the CMC (Cowell *et al.*, 2000; Harusawa
- *et al.*, 1982; Harusawa and Tanaka, 1981; Warr *et al.*, 1983). Commercial surfactants are molecules with
- 390 the same CO₂-philic moiety but with polydisperse EO numbers. Thus, they are surfactant mixtures with
- 391 dissimilar hydrophilic-lipophilic properties. After equilibration, the ethoxymer distribution was
- 392 measured in both phases and they observed that the aqueous phase contained larger mean EO numbers
- 393 than the n-hexane phase.
- 394 In the present study, the amount of surfactant in the CO_2 increased with an increased concentration in
- the brine, as it can be observed in Figure 15. The CMCs of Tergitol TMN 10 and Brij L23 in water are
- 396 0.11 wt.% and 0.01 wt.%, respectively (given by the provider). These results are consistent with
- 397 previous observations (Balcan and Anghel, 2005) and with the theoretical partition model of
- 398 polydisperse ethoxylated surfactants.



399

400 Figure 15. Equilibrium surfactant concentrations in CO₂ and SSW for Tergitol TMN 10 (left) and Brij L23 (right).

401 6. Conclusions

The effects of branching, temperature, and pressure on the partitioning of non-ionic surfactants for SSW-CO₂ systems have been studied. Two main surfactant types were studied, alkyl and alkylphenol ethoxylates. Aside from Brij L23, all surfactants had a similar ethoxylation number. The effect of concentration on the partition coefficient was also studied for the surfactants Tergitol TMN 10 and Brij L23. For both surfactants, it was observed that the partition coefficient decreased with increasing surfactant concentration in the aqueous phase. The observations resemble the behaviour of surfactant mixtures as commercial surfactants have polydispersed EO numbers.

409 In general, alkyl ethoxylates showed a tendency of increased solubilization in CO₂ as both pressure and 410 temperature increased. Branched alkyl ethoxylates (Tergitol 15-S-9 and Tergitol TMN 10) showed the 411 largest solubilization in CO₂ at low temperature and pressure. At 100 bar and 20°C, 53 wt.% and 412 62 wt.% of the surfactants solubilised in the CO₂, respectively. Brij L23, which is a linear alkyl ethoxylate with an ethoxylation number of 23, exhibited low solubilization up to 40°C. However, at 413 414 80°C most of the surfactant solubilized in the CO₂ when the system was pressurized to 200 bar and 415 300 bar. This observation was explained by the competitive effect between different mechanisms such 416 as micellization in the CO₂, tail solvation in CO₂, and hydrogen bonding between ethoxylate groups and 417 water molecules. Ramification increase of the hydrophobic tail is beneficial to increase CO₂ solubility 418 to a certain degree for alkyl ethoxylates. Highly ramified tails might be detrimental possibly due to an 419 increase of conformational entropy.

420 Alkylphenol ethoxylates showed lower solubilization than branched alkyl ethoxylates at 20°C and 40°C. 421 However, high solubilisation in CO₂ was obtained both for Igepal CO 720 and Igepal CA 720 when the 422 temperature was 2°C below their respective cloud points. The increase in solubilisation can possibly 423 also be attributed to favourable interactions between ethoxylate groups and CO₂ as the hydrogen bonding 424 with water molecules becomes weakened. Igepal CA 720 (branched alkylphenol moiety) obtained lower 425 partition coefficients than Igepal CO 720 (linear alkylphenol moiety). This difference could be explained 426 from the diminished conformational entropy that a more branched structure would have. No clear trend 427 of tail ramification effect on CO₂ solubilization was identified for alkylphenol ethoxylates. 428

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440 **7. References**

- Adkins, S.S. *et al.*, 2010. Morphology and stability of CO₂-in-water foams with nonionic hydrocarbon
 surfactants. Langmuir, 26(8): 5335-48.
- 443 Ashoori, E., van der Heijden, T. and Rossen, W.R., 2009. Fractional Flow Theory of Foam
- 444 Displacements With Oil (SPE-121579-MS), SPE International Symposium on Oilfield Chemistry.
 445 Society of Petroleum Engineers, The Woodlands. Texas, pp. 17.
- Balcan, M. and Anghel, D.F., 2005. The partition of ethoxylated non-ionic surfactants between two non miscible phases. Colloid and Polymer Science, 283(9): 982-986.
- 448 Bera, A., Kumar, T., Ojha, K. and Mandal, A., 2013. Adsorption of surfactants on sand surface in 449 enhanced oil recovery: Isotherms, kinetics and thermodynamic studies. Applied Surface Science, 284:
- 450 87-99.
 451 Binks, B.P., 2002. Particles as surfactants—similarities and differences. Current Opinio
- Binks, B.P., 2002. Particles as surfactants—similarities and differences. Current Opinion in Colloid &
 Interface Science, 7(1): 21-41.
- 453 Chen, Y. et al., 2015. CO2-in-Water Foam at Elevated Temperature and Salinity Stabilized with a
- 454 Nonionic Surfactant with a High Degree of Ethoxylation. Industrial & Engineering Chemistry Research,
 455 54(16): 4252-4263.
- 456 Chen, Y. et al., 2012. Ethoxylated Cationic Surfactants For CO₂ EOR In High Temperature, High
- 457 Salinity Reservoirs, SPE Improved Oil Recovery Symposium. Society of Petroleum Engineers, Tulsa,
 458 Oklahoma, USA.
- Cowell, M.A., Kibbey, T.C.G., Zimmerman, J.B. and Hayes, K.F., 2000. Partitioning of Ethoxylated
 Nonionic Surfactants in Water/NAPL Systems: Effects of Surfactant and NAPL Properties.
- 461 Environmental Science & Technology, 34(8): 1583-1588.
- 462 Curbelo, F.D.S. et al., 2007. Adsorption of nonionic surfactants in sandstones. Colloids and Surfaces A:
- 463 Physicochemical and Engineering Aspects, 293(1): 1-4.
- 464 Enick, R.M., Olsen, D., Ammer, J. and Schuller, W., 2012. Mobility and Conformance Control for CO₂
- EOR via Thickeners, Foams, and Gels A Literature Review, SPE Improved Oil Recovery Symposium.
 Society of Petroleum Engineers, Tusla, Oklahoma, USA.
- 467 Espinosa, D., Caldelas, F., Johnston, K., Bryant, S.L. and Huh, C., 2010. Nanoparticle-Stabilized
 468 Supercritical CO₂ Foams for Potential Mobility Control Applications, SPE Improved Oil Recovery
 469 Symposium. Society of Petroleum Engineers, Tulsa, Oklahoma, USA.
- 470 Flory, P.J., 1953. Principles of Polymer Chemistry Cornell University Press, Ithaca, New York.
- 471 Grimstad, A.-A., Bergmo, P., Nilsen, H.M. and Klemetsdal, Ø., 2018. CO₂ Storage with Mobility
- 472 Control, 14th International Conference on Greenhouse Gas Control Technologies, GHGT-14,
 473 Melbourne, Australia.
- Harusawa, F., Nakajima, H. and Tanaka, M., 1982. The Hydrophile-Lipophile Balance of Mixed
 Nonionic Surfactants. Journal of the Society of Cosmetic Chemists, 33(3): 115-129.
- 476 Harusawa, F., Saito, T., Nakajima, H. and Fukushima, S., 1980. Partition isotherms of nonionic
- 477 surfactants in the water—cyclohexane system and the type of emulsion produced. Journal of Colloid
- 478 and Interface Science, 74(2): 435-440.
- Harusawa, F. and Tanaka, M., 1981. Mixed micelle formation in two-phase systems. The Journal ofPhysical Chemistry, 85(7): 882-885.
- Hoefling, T.A., Enick, R.M. and Beckman, E.J., 1991. Microemulsions in near-critical and supercritical
 carbon dioxide. The Journal of Physical Chemistry, 95(19): 7127-7129.
- 483 Johnston, K.P. and Rocha, S.R.P.d., 2009. Colloids in supercritical fluids over the last 20 years and 484 future directions. The Journal of Supercritical Fluids, 47(3): 523-530.
- 485 Le, V.Q., Nguyen, P. and Sanders, A.W., 2008. A Novel Foam Concept With CO₂ Dissolved
- 486 Surfactants, SPE/DOE Improved Oil Recovery Symposium. Society of Petroleum Engineers, Tusla,
 487 Oklahoma, USA.
- 488 Manlowe, D.J. and Radke, C.J., 1990. A Pore-Level Investigation of Foam/Oil Interactions in Porous
- 489 Media. SPE-27787-PA: 495-502.
- 490 McLendon, W.J. et al., 2012. Assessment of CO₂-Soluble Surfactants for Mobility Reduction using
- Mobility Measurements and CT Imag, SPE Improved Oil Recovery Symposium. Society of Petroleum
 Engineers, Tulsa, Oklahoma, USA.

- 493 San, J., Wang, S., Yu, J., Lee, R. and Liu, N., 2016. Nanoparticle Stabilized CO₂ Foam: Effect of
- 494 Different Ions, SPE Improved Oil Recovery Conference. Society of Petroleum Engineers, Tulsa,
- 495 Oklahoma, USA.
- Schramm, L.L. and Novosad, J.J., 1990. Micro-visualization of foam interactions with a crude oil.
 Colloids and Surfaces, 46(1): 21-43.
- 498 Solbakken, J.S., Skauge, A. and Aarra, M.G., 2013. Supercritical CO₂ Foam The Importance of CO₂
- 499 Density on Foams Performance, SPE Enhanced Oil Recovery. Society of Petroleum Engineers, Kuala
 500 Lumpur.
- 501 Tsau, J.-S. and Grigg, R.B., 1997. Assessment of Foam Properties and Effectiveness in Mobility
- 502 Reduction for CO₂-Foam Floods, SPE International Symposium on Oilfield Chemistry. Society of
- 503 Petroleum Engineers, Houston, Texas, USA.
- 504 Vassenden, F., Holt, T., Moen, A. and Ghaderi, A., 2000. Foam Propagation in the Absence and
- 505 Presence of Oil, SPE/DOE Improved Oil Recovery Symposium. Society of Petroleum Engineers, Tusla,
 506 Oklahoma, USA.
- 507 Warr, G.G., Grieser, F. and Healy, T.W., 1983. Distribution of polydisperse nonionic surfactants 508 between oil and water. The Journal of Physical Chemistry, 87(22): 4520-4524.
- 509 Wasan, D.T., Koczo, K. and Nikolov, A.D., 1994. Mechanisms of Aqueous Foam Stability and
- 510 Antifoaming Action with and without Oil, Foams: Fundamentals and Applications in the Petroleum
- 511 Industry. Advances in Chemistry. American Chemical Society, pp. 47-114.
- Xing, D. *et al.*, 2012. CO₂-Soluble, Nonionic, Water-Soluble Surfactants That Stabilize CO₂-in-Brine
 Foams. SPE-169104-PA, 17(04): 1172-1185.
- 514 Xing, D. et al., 2010. CO₂-Soluble Surfactants for Improved Mobility Control, SPE Improved Oil
- 515 Recovery Symposium. Society of Petroleum Engineers, Tulsa, Oklahoma, USA.
- 516 Yu, J., Liu, N., Li, L. and Lee, R., 2012. Generation of Nanoparticle-Stabilized Supercritical CO₂ Foams,
- 517 Carbon Management Technology Conference. Carbon Management Technology, Orlando, Florida,518 USA.
- 519