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Development of technology for autonomous, bio-interactive and high-quality data acquisition from aquaculture net cages

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 **NTNU – Trondheim**
Norwegian University of
Science and Technology

 **Hes-50**
Haute Ecole Spécialisée
de Suisse occidentale
Fachhochschule Westschweiz
University of Applied Sciences and Arts
Western Switzerland

 **The Research Council
of Norway**

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The CageReporter project adapts the use of autonomous and tetherless underwater vehicles as a carrier of sensor systems for data acquisition, where the data are transferred from sea-based fish cages to a centralized land base (Figure 1). The vehicle will use active motion control and acquire data from the cage environment while exploring the fish cages. The main project objective is to develop technology for autonomous functionality for adaptive mission planning to achieve high quality data acquisition from the cage space. One of the most important capabilities within this context is to operate in a dynamically changing environment in interaction with the biomass (bio-interactive) and the aquaculture structures. The project addresses many challenges within the aquaculture industry related to poor accuracy and representative sampling of important variables from the whole volume of the cage. A successful project outcome will lead to new technology for collection of high-resolution data that could be utilized for assessment of the fish farm state, grouped within three main areas: A) fish, B) aquaculture structures and C) production environment. Examples of areas of applications are detection of abnormal fish behaviour, net inspection and mapping of water quality. CageReporter will provide a solution for continuous 24/7 inspection of the current situation and will be the mobile eyes of the fish farmer in the cage environment. The project idea is based on using low-cost technology for underwater communication, vehicle positioning, and camera systems for 3D vision.

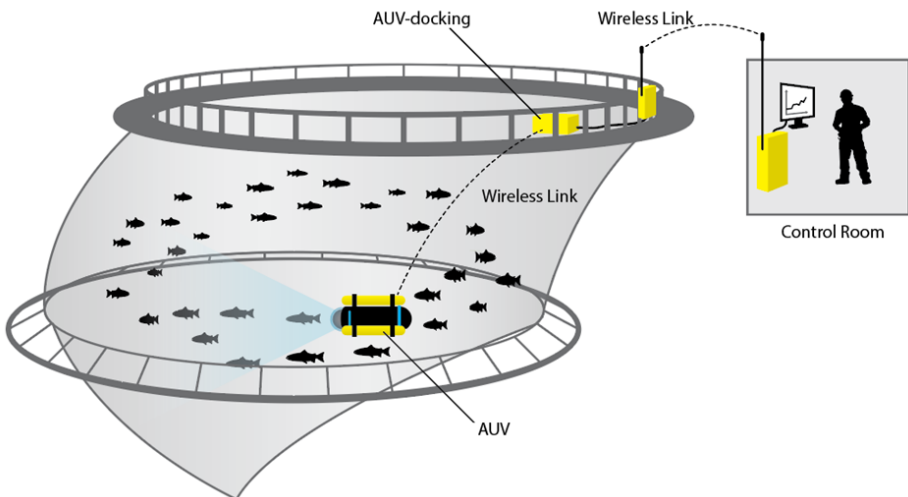


Figure 1: Resident (24/7), autonomous, non-tethered vehicle (AUV) for high quality data acquisition

The project will address many challenges within the aquaculture industry related to poor accuracy and representative sampling of important variables to describe both details and the whole picture. CageReporter will provide continuous and close follow up of the current situation and be the "eye" of the fish farmer inside the cage (Figure 1). The project idea is based on using low-cost technology for underwater communication, vehicle positioning and camera systems for 3D vision.

MAIN GOAL

The project will develop autonomous resident technology for high quality data capture describing the conditions in the cage volume associated with the fish, infrastructure and production environment.

Sub-Goal 1: Develop application-adapted underwater communications technology, position reference and 3D vision systems that reduce the cost by a factor of 5-10 compared to conventional technology.

Sub-Goal 2: The underwater vehicle will have autonomous functions that enable adaptive operation planning and bio-interactive data capture, with a minimum of operator interaction.

Sub-Goal 3: High quality data and metadata must be obtainable from the entire cage volume.

Sub-Goal 4: The integrated system consisting of underwater vehicle with autonomous functionality, the underwater positioning system and the 3D vision system will be validated in full-scale trials for the following case studies: A) Fish Conditions, B) Cage Inspection, and C) Production Environment.

RESEARCH AREAS

- H1: Underwater communication and position reference system
- H2: Data acquisition and real-time analysis of high-quality vision data
- H3: Autonomous systems
- H4: Underwater docking system

The CageReporter project will perform breakthrough work regarding which sensors, communication technology and autonomous systems should be combined to perform data capture in interaction with the fish, infrastructure and production environment.

INNOVATION AND VALUE CREATION

Within the aquaculture industry, there is currently only a minimum of technological solutions that can assist in bringing the fish through the production cycle into the sea, and within several areas the production process is suboptimal. Key variables such as feed mode and feed play, the number of fish, average weight and growth, sleep state, state of health and the condition of the cage are either inadequate control or the accuracy and detail level is inadequate. Innovation will help address three of the industry's main challenges: escapes, salmon lice and

mortality, which today are factors that hinder further growth in the industry. Innovation will also provide the authorities with a new tool for monitoring the facilities in accordance with current rules and regulations. Documentation and standardization of operating conditions are becoming increasingly important. The Norwegian Food Safety Authority has called for better documentation from breeders, including better technology and methods for counting lice. Innovation addresses these challenges, thus enabling sustainable growth for future aquaculture.

There are currently no similar commercial products that the project page outlines, and the partners in the project therefore have the opportunity to be first in the market with new and ground-breaking technology and associated services.

CONCLUSION

Underwater robots are today used in a variety of different applications in different industrial segments. In most present applications, the vehicle is beneath the wave zone, where environmental impacts are less challenging, and relates to fixed features. However, the external features a robotic system faces in an aquaculture situation differ from those encountered in conventional operations. This project targets a novel research area by investigating the challenges of using underwater robots in "application-realistic" environments such as fish farms, where structures are flexible, and robotic systems must interact with animals during operations.

PROJECT PARTICIPANTS

- Water Linked AS (Project owner)
- SINTEF Ocean AS (Project leader)
- Sealab AS
- Norsk Havservice AS
- NTNU
- University of Applied Sciences and Art Western Switzerland (HES-SO)

CONTACT

Eleni Kelasidi
+4745185796
Eleni.kelasidi@sintef.no



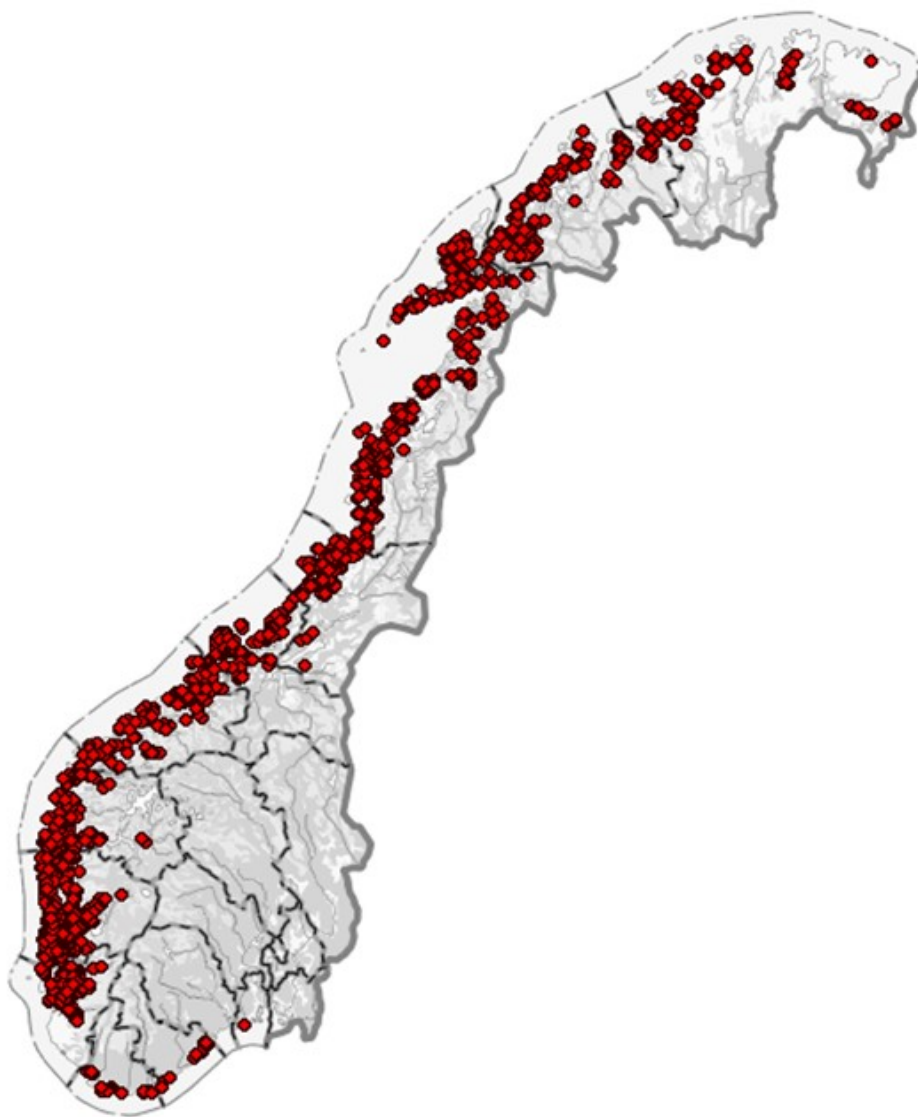
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SINTEF



The Research Council
of Norway



Aquaculture sites in Norway for

- Salmon
- Rainbow trout
- Trout

CageReporter project (RCN 296476)

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H1: UNDERWATER COMMUNICATION AND LOCATION REFERENCE SYSTEM

B.SU, E. KELASIDI, E. S. THORBJØRNSEN

H1.1: UNDERWATER COMMUNICATION

A robust high-bandwidth and low cost communication system is a key element of the project, and the realization of such a solution requires significant research efforts. Hydroacoustic communication is highly demanding in the presence of biomass in the signal path, as the acoustic signals are subjected to scattering and damping. Note that the density of biomass changes considerably in the course of the production cycle, where the fish grows from an average weight of approx. 100g to 5kg. Consequently, an important requirement is that the system will be able to handle this variability in biomass during the operations in fish cages. This brings significant R&D challenges related to further developing underwater communication system to achieve stable real-time communication with good coverage throughout the entire cage.

The research need is also related to the development of a cage-relative position reference system that reports the position of an underwater vehicle relative to the fish cage. Such a system is required for accurate positioning and motion control of an underwater vehicle inside the fish cages. The positioning of the vehicle in fish cages is an extra demanding task compared to conventional operations with fixed structures, since the fish net is deformed by waves and currents (Rundtop and Frank, 2016). In the following, this report describes the development and

validation of the underwater communication technology and the position reference system. In this study, the underwater positioning system developed by WaterLinked AS (i.e. wLink) has been used in combination with numerical methods to realize a position reference system, and the research need lies in developing a wLink configuration that provides good performance in combination with the numerical methods. In particular, in order to realize a cage-relative position reference system, wLink has been used in the Short Base Line (SBL) configuration with four acoustic receivers attached to the cage and an acoustic transmitter placed on the vehicle to measure the position of the vehicle relative to the cage. In addition, three acoustic transmitters have been placed in different locations in the fish cage, where the measured positions have been used in combination with a numerical model of the fish cage, to estimate an updated real-time map of the deformable fish cage.

Based on the wLink technology, a low cost hydroacoustic subsea communication system was developed and adapted for use in the cage. The development and adaptation included the optimization of sender and receiver technology, as well as development of algorithms for advanced signal processing to optimize bandwidth while ensuring stable real-time communication under conditions that affect the communication link. The developed solution was tested and validated at full scale farm sites.

DEVELOPED TECHNOLOGY

In the project CageReporter, Water Linked has continued the development of the underwater communication technology wLink. This development has resulted in the acoustic modem named 'Water Linked Modem M64', Figure 2.



Figure 2: Modem M64

The Modem M64 uses WaterLinked's own transducer and electronics. It has a transmission rate of 64 bits per second and a range of 200 meters. The modem is omnidirectional, meaning that the modem transmits and receives in all directions. What makes the M64 modem unique is its small physical size and the highly robust datalink provides to the user. These capabilities are what makes the Modem M64 suitable for use in fish cages and other high reflective and noisy environments like in harbors.

In many operations it is not practical to use cabled sensors since the cable itself can amount to significant cost. In addition, the installation can be cumbersome and time consuming which further adds cost. Cables are also by their nature prone to damage which may cut off the sensor entirely and trigger extensive costs for replacement. To avoid all this, the WaterLinked modem M64 can be utilized to remove the need for the cable entirely (Figure 3). By connecting the M64 with the sensor and a battery pack, one receives a fully wireless sensor with a very robust setup. The sensor can be read by another Modem M64 which can reside in a

fixed place topside. The M64 modems can also be mounted on ROVs, ships or other moving vehicles for dynamic interrogation of the sensors (Figure 4). By utilizing the Water-Linked Underwater GPS system, all locations (i.e. position of a net, vehicle, feeding camera, etc.) can easily be documented real-time during daily operations in fish cages.

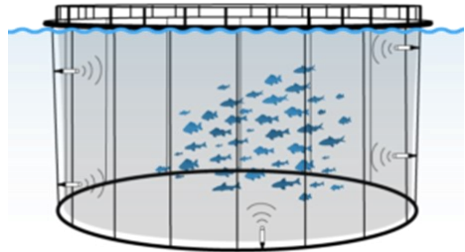


Figure 3: Illustration of wireless sensors installed on a fish cage

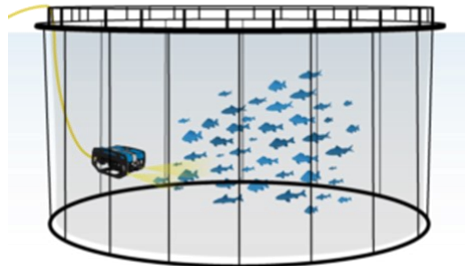


Figure 4: Illustration of wireless sensor installed on the ROV

The algorithms and protocols that Water-Linked uses are designed to handle the demanding environments of a sea cage. Water-Linked's own signal processing has been optimized considerably to filter out noise and other error sources which can lead to drop out of communication. These adjustments are both in hardware of the modem and software. Legacy modems typically use the carrier frequency to decide if the value sent is "0" or "1". This is very vulnerable to inter-

ference and packet loss and makes them unsuited for use in fish cages and other reflective environments. In contrast, the Modem M64 uses modern error correction techniques which are more robust. In addition, the Modem M64 not only has an advanced auto-sync feature which makes it extremely easy to use, it is also, other than classic modems, fully omnidirectional. The omnidirectional property is especially important for underwater vehicle applications where the modems are in constant motion and can be turned around all axes while still maintaining its robust data link. With WaterLinked's Modem M64, real time communication in fish cages is possible. The specification of the developed Modem M64 are given in Table 1 and Figure 5.

Communication	Two-way communication, 64 bit per second net data link, both ways
Typical latency	~500ms
Directivity	Omnidirectional
Acoustic range	200 m
Depth rating	300 m
Device length	112 mm
Device diameter	30 mm
Device weight	128 g
Input voltage	10-18 V

Table 1: Specifications of Modem M64

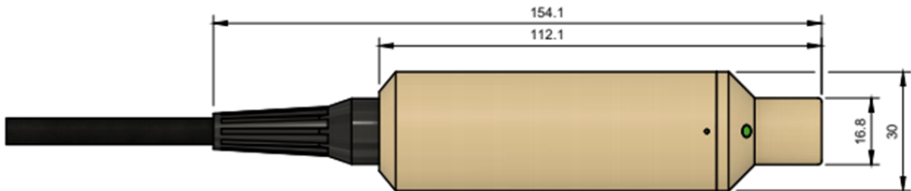


Figure 5: Dimensions of Modem M64 [mm]

WaterLinked has developed several locators and receivers. In this project, the WL-21009 Locator-A1, WL-21018 Locator-U1 and WL-21005 Receiver-D1 were used in order to obtain results for the underwater positioning reference systems. The specifications and dimensions are given in Tables 2-4 and Figures 6-8.

Directivity	Omnidirectional
Depth sensor	None
Depth rating	300 m
Default cable length	1 m
Max cable length	300 m (custom order)
Signaling	1x twisted pairs
Cable type	PUR 6.3 mm
Cable connector	None
Device length	41 mm
Device diameter	20 mm
Device weight in air	30 g
Operating temperature	-10 to 60 °C

Table 2: Specifications of WL-21009 Locator-A1

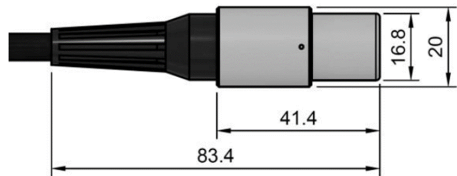


Figure 6: Dimensions WL-21009 Locator-A1 [mm]

Directivity	Omnidirectional
Depth sensor	Integrated
Depth rating	300 m
Max operational range	100 m (wireless)
Battery size	3.7 volt, 3300 mAh
Battery lifetime	10 hours
Device length	121 mm
Device diameter	32 mm
Device weight (air)	175 g
Operating temperature	-10 to 60 °C

Table 3: Specifications of WL-21018 Locator-U1

Directivity	Omnidirectional
Depth rating	300 m
Max cable length	100 m
Signaling	2x twisted pairs
Cable type	PUR 6.3 mm
Cable connector	Binder Series-770 (IP67)
Device length	71 mm
Device diameter	20 mm
Device weight	36 g
Input voltage	10-18 V
Input current	35 mA
Operating temperature	-10 to 60 °C

Table 4: Specifications of WL-21005 Receiver-D1

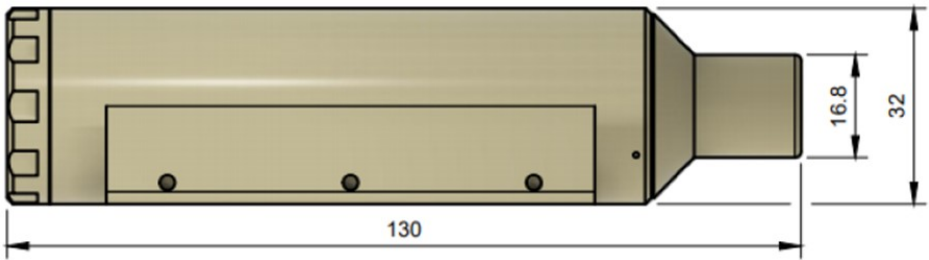


Figure 7: Dimensions WL-21018 Locator-U1 [mm]

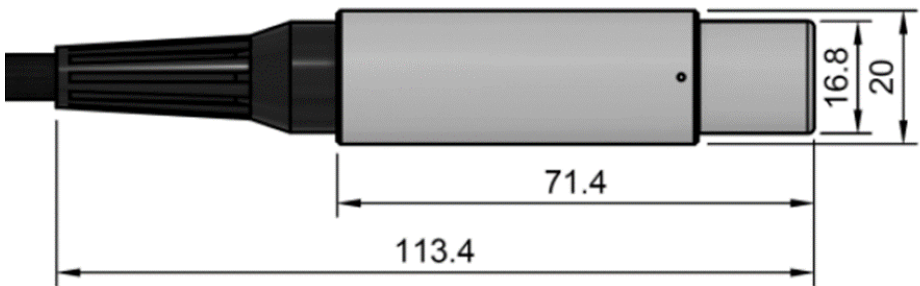


Figure 8: Dimensions WL-21005 Receiver-D1 [mm]

H1.2 MODEM M64 VALITADION TESTS

WaterLinked has performed multiple tests of the acoustic Modem M64. Initially tests were performed at WaterLinked's office in a test tank to verify and optimize the hardware, software and algorithms. The test tank is made of plastic and creates a test environment with lots of reflections and noise. Up to 50 reflections of the initial signal have been observed before it disappears. This creates a very good test environment for developing the modem and algorithms used to remove noise and reflections. After these initial

tests, the modem has been tested in Brattøra (Figure 9,10,12) and Monkholmen (Figure 11) in Trondheim. These areas both provide a reflective environment. The tests have been performed to verify that the communication link works well over longer distances and also when moving in water. Testing distance varied from a couple of meters up to 200 meters. These tests, together with the results from the test tank, confirmed that the modem M64 provides a robust and very stable communication link in reflective and noisy environment (Figure 13).



Figure 9: Test in Brattøra – highly reflective environment



Figure 11: Munkholm test with one modem M64 on dock and the other on the boat



Figure 10: Online monitoring system in Brattøra tests



Figure 12: Obtained trajectory and accuracy of the underwater positioning system in Brattøra tests

Figure 13: Data from four receivers showing acoustic signals over time

HL.3 POSITION REFERENCE SYSTEM

This activity presents the development of a relative position reference system where the main challenge was to develop a realistic real-time map of the fish cage. The analytical study was conducted in order to decide on the placement of the acoustic transmitters. The proposed configuration has been tested in full scale. The obtained experimental data have been used to develop and validate numerical methods that estimate a high-

LAB AND FIELD DEPLOYMENT

The WaterLinked positioning system consists of a topside positioning computer and a certain number of locators and receivers: the locators are sending acoustic signals which are picked up by the receivers and the topside positioning computer uses advanced algorithms to triangulate and calculate the positions of the locators based on the signals received by the receivers. This system has been tested at the Hosnøya and Rataren sites (SINTEF ACE full-scale laboratory facility) in 2018 and 2019, and at the Ocean Basin Laboratory (SINTEF Ocean) in 2019 (Figure 14). Based on the results of the model-scale testing at the lab and the initial full-scale tests at Hosnøyan and Rataren, the WL-21009 Locator-A1, WL-21018 Locator-U1 and WL-21005 Receiver-D1 were chosen for the final deployment at the Rataren site-Cage 7 (Figure 15) in 2019.

As shown in Figure 16, three locators (WL-

resolution real-time map of the fish cage. The work further included the development of algorithms for state estimation to increase accuracy and reduce target noise. Well established methods of processing and state estimation were used (Fossen, 2011). The position reference system was validated through multiple trial series where positioning accuracy was evaluated.



Figure 14: ROV testing at the Ocean Basin Laboratory (SINTEF Ocean)

21009 Locator-A1) were installed in a cage (Cage 7) at the Rataren site: the first one was attached to the lower edge of the sea-lice skirt (in 6.3 m depth), the second one was attached to the bottom tip of the net (in 32 m depth), the third one was attached to the connection rope between the net and the sinker tube (in 16.2 m depth). Four receivers (WL-21005 Receiver-D1) were used to pick up the acoustic signals from each locator. Receivers #1-3 were placed along a rope connecting two points along the walkway (xm distance) and hanging down to

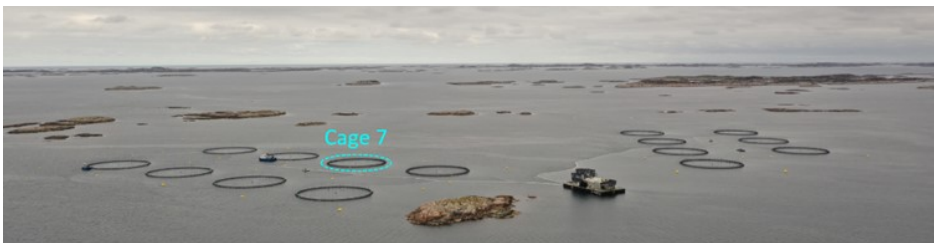


Figure 15: SINTEF ACE Rataren site

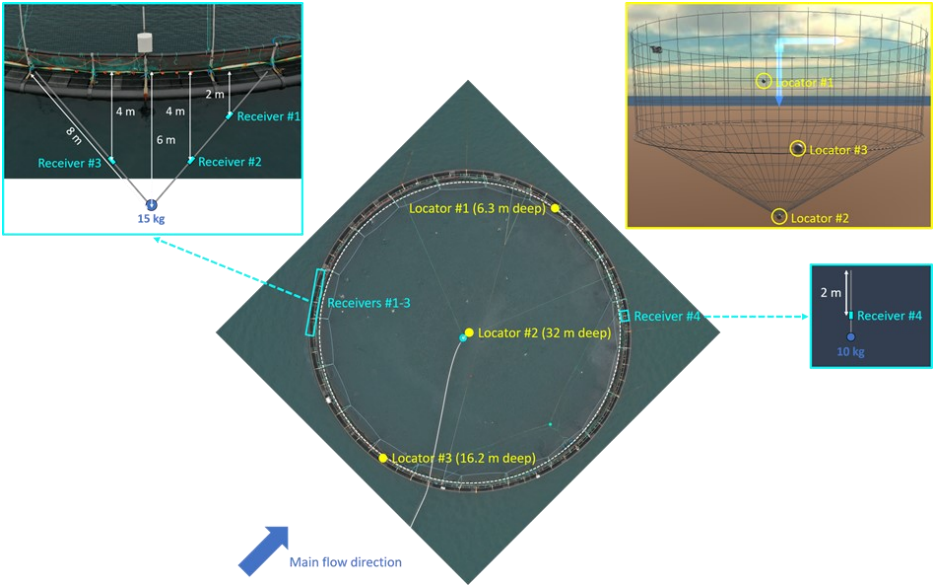


Figure 16: Field deployment at the Rataren site

6m depth in the middle where a weight was attached (Figure 16): two of the receivers were placed at 4 m depth on both sides of the weight, and the third one was placed at 2 m depth. Receiver #4 was placed at 2 m depth on the opposite side of the cage (Figure 16). All locators and receivers were connected by cables to the topside cabinet,

from where the obtained signals were sent out through the integrated 4G modem.

WaterLinked also provides an online monitoring system (Figure 17) for data collection and setting up parameters for the positioning system, e.g. locator type, search range and the local coordinate system for calculating

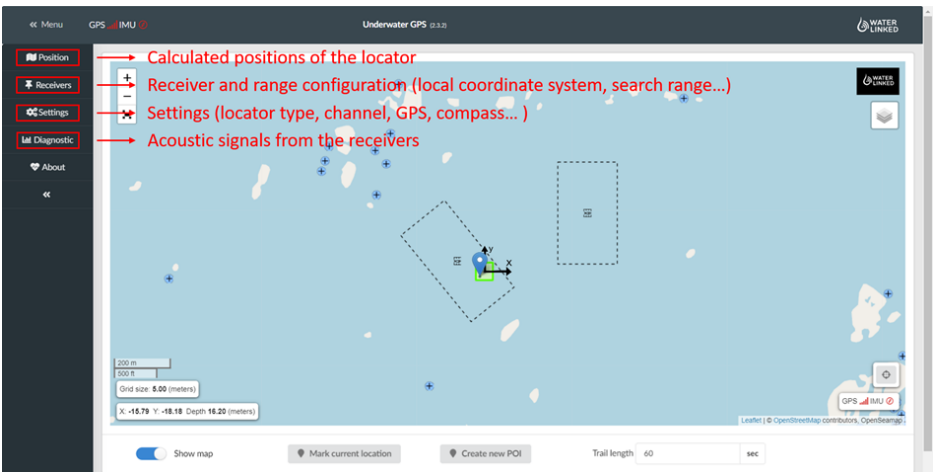


Figure 17: WaterLinked online monitoring system

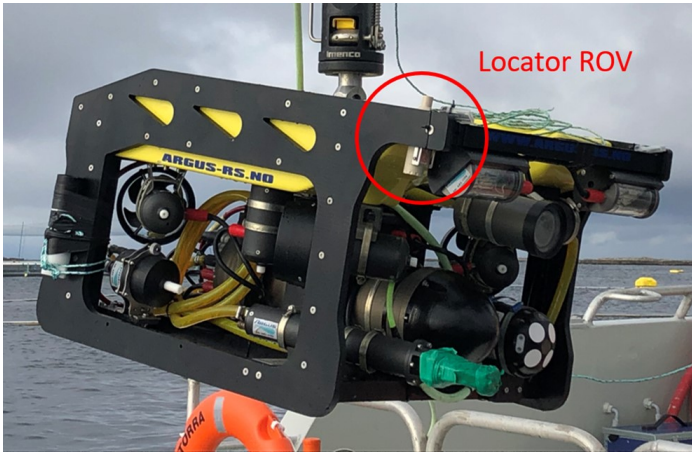


Figure 18: WL-21018 Locator-U1 used to obtain real-time position of the ROV in fish cage

relative positions of the locators. Acoustic signals from the receivers and calculated positions of the locators can be displayed and recorded instantaneously through the designated web address.

For positioning the ROV in the field trial, a wireless locator (WL-21018 Locator-U1) attached to the ROV and four separated

receivers (WL-21005 Receiver-D1) were used (Figure 18). The configuration of the receivers was adjusted in order to calculate ROV positions in the same local coordinate system as that used for the net (Figure 19). Instead of using 4G, a PC was directly connected to the topside cabinet through a local network for importing real-time positioning data to a numerical estimation model.

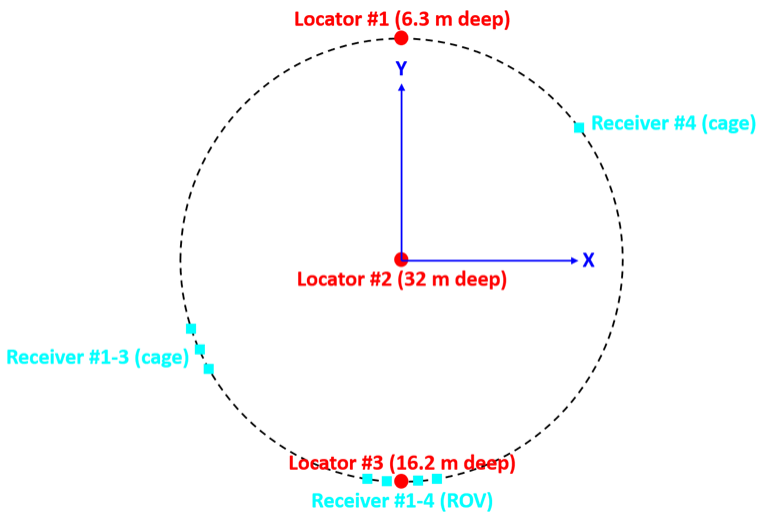


Figure 19: Configuration of the local coordinate system in the field trial

Figure 20 shows an example of the recorded trajectory of a ROV (Remotely Operated Vehicle) at the Ocean Basin Laboratory, where the ROV was lying on the bottom of the tank and a wireless locator was used for positioning. The corresponding time series of the measured positions is shown to be reasonably stable (Figure 21). As it was not possible to have the ROV lying on the bottom of the cage during the field trial in order to assess the precision of the measurements, the ROV was controlled to keep the desired position by using a nonlinear Dynamic position (DP) controller. Figures 22 - 27 show that the measured positions were stable and no significant errors occurred (i.e. jumping signals or loss of signals) on the measured positions. The precision of the measurements during both the lab tests and field trials show that the accuracy of the positioning system is suited to obtain accurate position measurements of static (i.e. tests in the tank where the ROV is sitting on the bottom of the tank) and moving objects (i.e. tests in the cage where the ROV is keeping the desired position in the cage using DP controller) underwater and for the implementation of autonomous control functions for the navigation of the underwater vehicle.

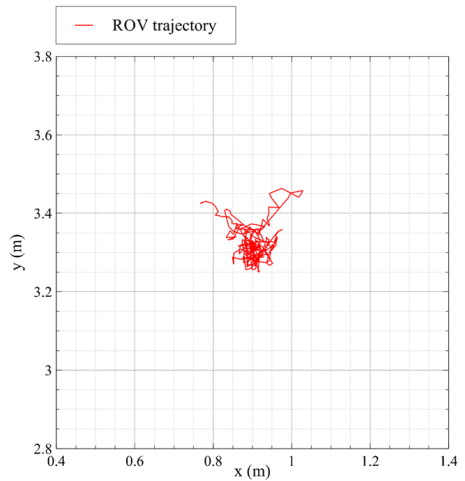


Figure 20: Recorded trajectory of the ROV sitting at the bottom of the Ocean Basin Laboratory

In addition, it should be mentioned that with better tuning of the control gains of the DP controller we were able to obtain even better accuracy for the position of the system during dynamic positioning of the vehicle, thus enabling the ROV to navigate in the cage without inputs from the ROV operator or the site manager of the fish farm.

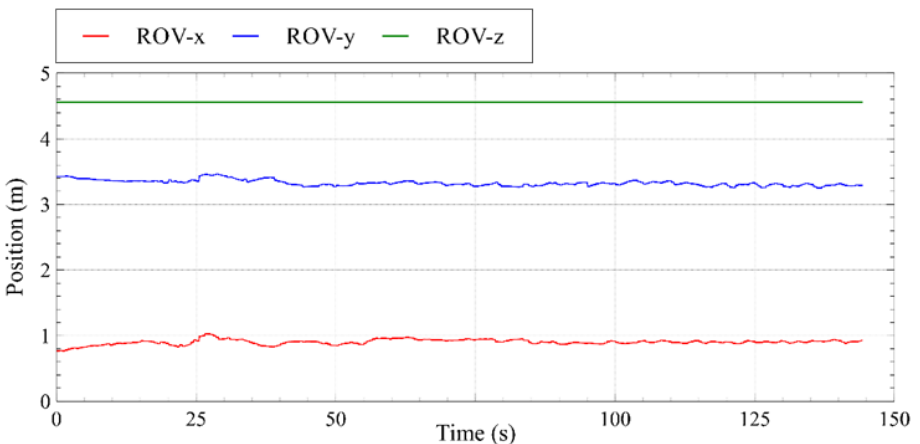


Figure 21: Time series of the measured ROV positions (corresponding to Figure 20)

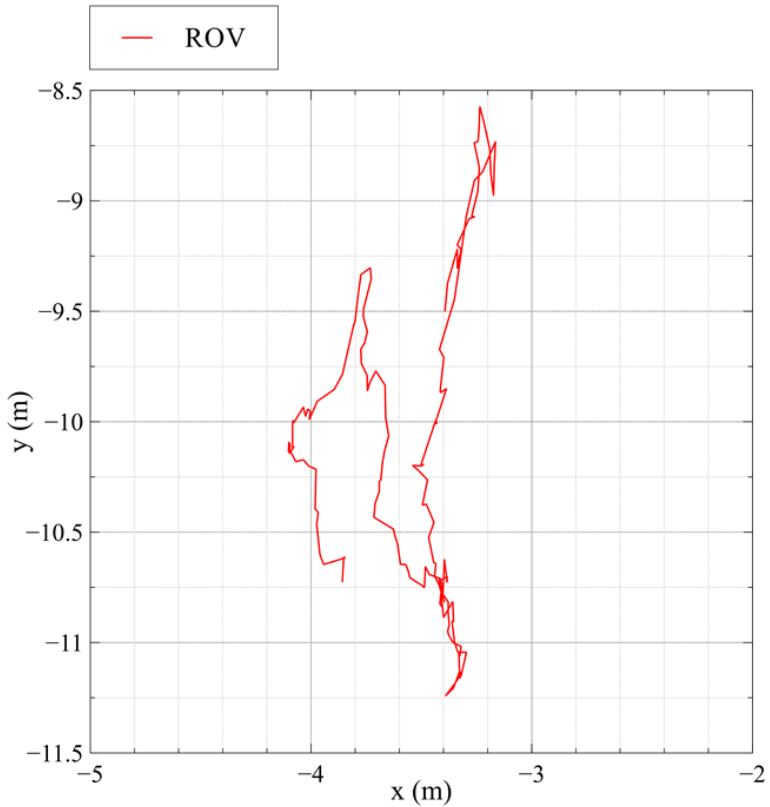


Figure 22: Recorded trajectory of the ROV in the field trial for desired position $X=-3.3\text{m}$, $Y=-9.9\text{m}$ and $Z=4.5\text{m}$

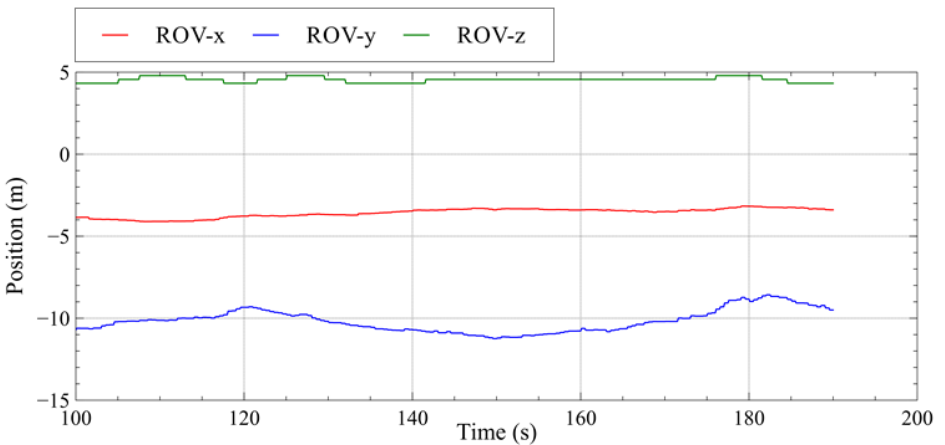


Figure 23: Time series of the measured ROV positions in the field trial (corresponding to Figure 22)

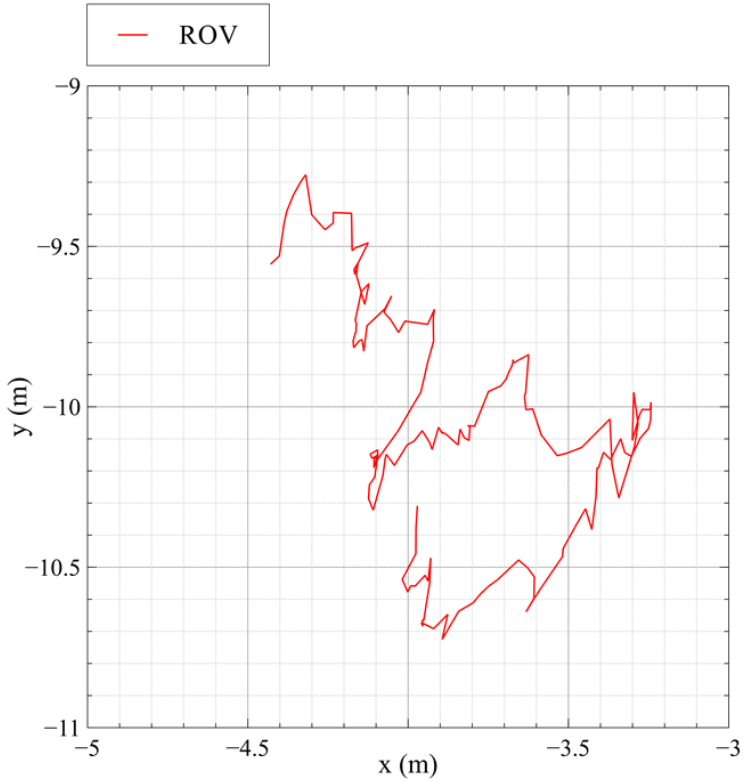


Figure 24 :Recorded trajectory of the ROV in the field trial for desired position $X=-3.3m$, $Y=-9.9m$ and $Z=2.5m$

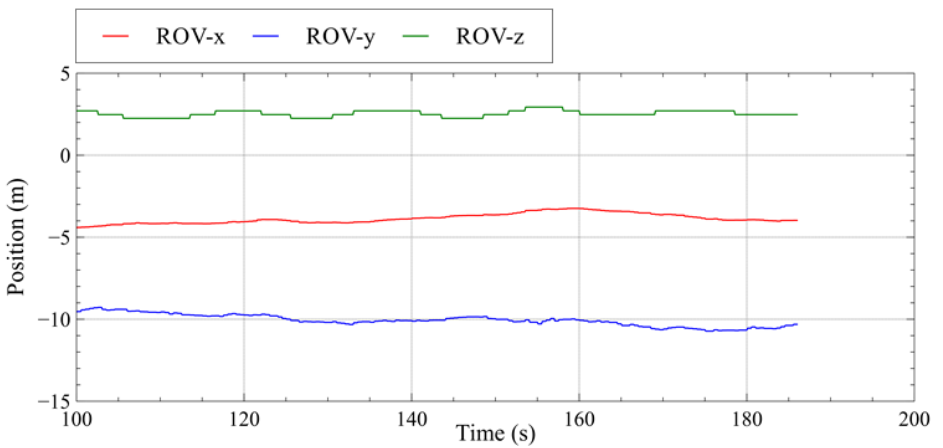


Figure 25: Time series of the measured ROV positions in the field trial (corresponding to Figure 24)

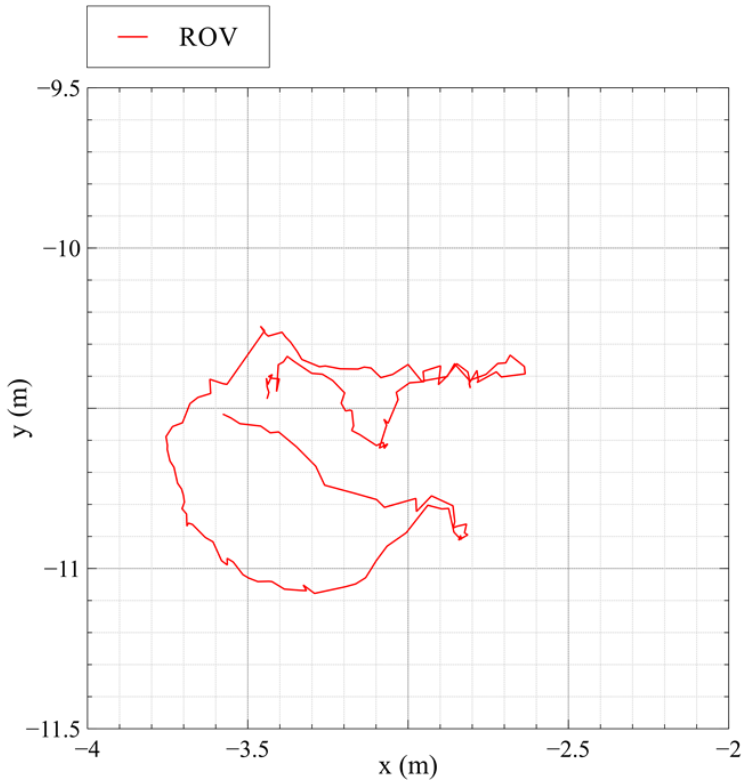


Figure 26: Recorded trajectory of the ROV in the field trial for desired position $X=-3.3m$, $Y=-9.9m$ and $Z=0.5m$

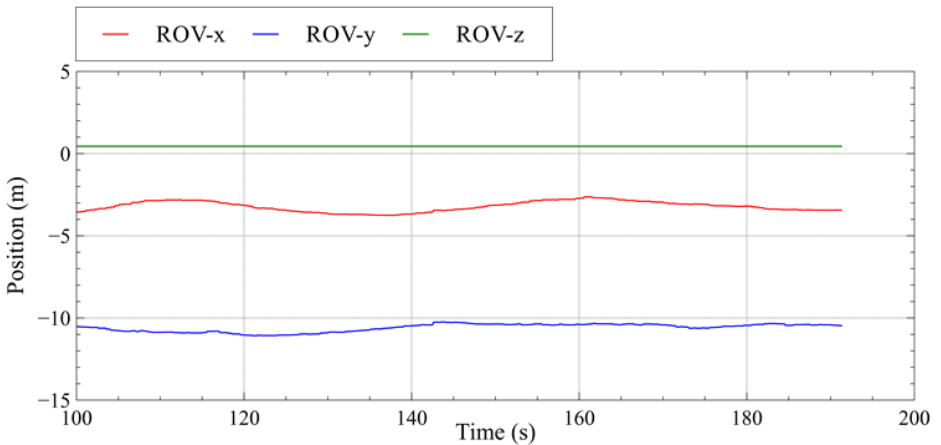


Figure 27: Time series of the measured ROV positions in the field trial (corresponding to Figure 26)

Figure 28 shows an example of the measured positions from the three locaters on the net cage over a period of 37.5 hours (3 tidal periods). It is evident that the measured positions deviate from the idealized configuration (Figure 19), because the actual net cage

did not have an exactly cylindrically-conical shape at all times. The trajectory of Locator #1 shows the displacement of the net elements at 6.3 m depth to be in accordance with the main direction of tidal flow, while the displacement of the net at 16.2 m depth (Locator #3) is shown to be in another direction. This indicates a possible change of flow direction with water depth due to local variations (e.g. geomorphology or fluid-structure interactions). The corresponding time series of the measured positions (e.g. Figure 29) show that the positioning system had a noise level of about 2 m, which is suited for the estimation of cage deformations on an average level (i.e. neglecting short-period deviations).

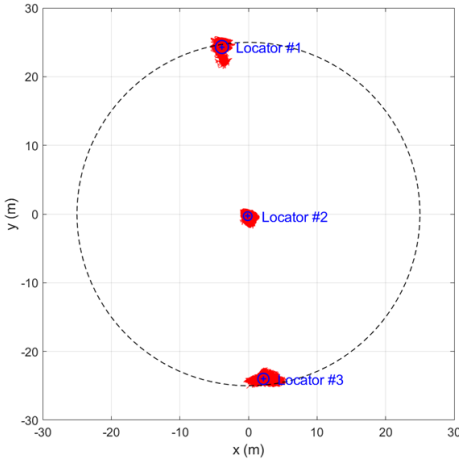


Figure 28: Recorded trajectories (red) of the three locaters on the net. The blue crosses denote the calculated mean positions and the blue circles denote the corresponding standard deviations

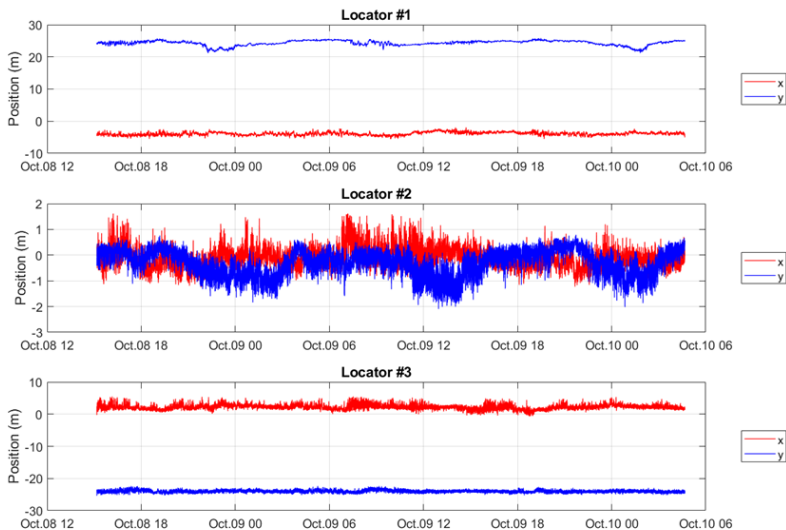


Figure 29: Time series of the measured locator positions (corresponding to Figure 28)

NUMERICAL ESTIMATION MODEL

FhSim is a software framework that has been under continuous development at SINTEF Ocean since 2006 (Reite et. al. 2014; Su et. al. 2019). It provides numerical models for time-domain simulation of flexible net cages in current and waves. FhSim also contains a module for system state estimation based on a nonlinear extended Kalman filter (Einicke and White, 1999). By using this method, a numerical model can be combined with sensor data to create a more realistic estimation of the actual system. However, it is found to be difficult for real-time implementation considering a net-cage system with a large number of states. For this reason, a simplified net-cage model with an adaptive current field was used to estimate net-cage deformations based on the measured positions of the net (Figure 30). Error signals, i.e. the deviation of the estimated positions compared to the measured positions, are used to

adapt the magnitude and direction of the current at various depths. The adaptation is using a PID controller with integral saturation for each error signal.

This method was first tested with simulated data, i.e. two simulated positions of the net under given current and wave conditions. In the estimation model, the magnitude and direction of the current were unknown and they were continuously adapted. At the same time, the adapted current forces were also applied in the estimation of net-cage deformations, until a best fit to the simulated data was achieved. Figure 31 and Figure 32 show an example of the position errors (i.e. estimation errors which are defined as differences between the measured and estimated positions) and the estimated current velocities, which demonstrates the potential of using two measured positions (in the horizontal plane) for the estimation of net-cage deformations by adapting the current profiles (i.e. current velocities and directions at various depths).

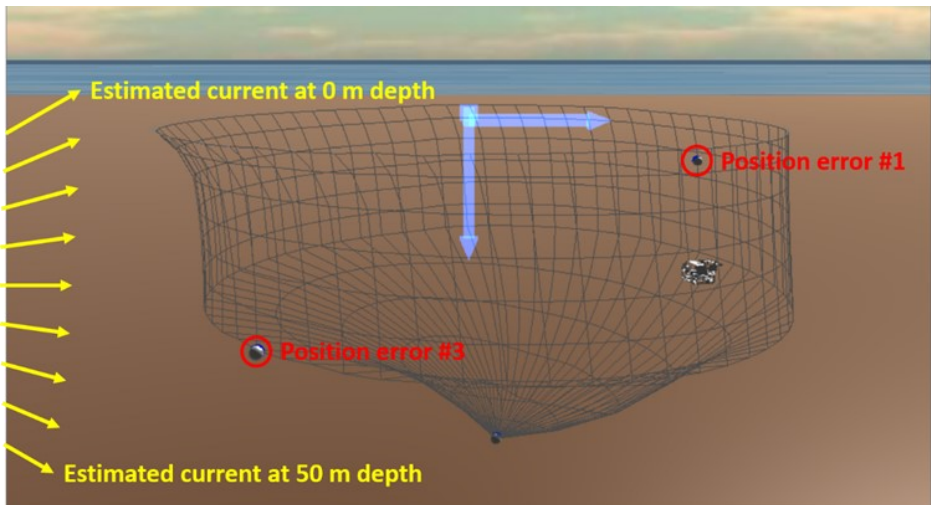


Figure 30: A simplified net-cage model with an adaptive current field based on two measured positions of the net

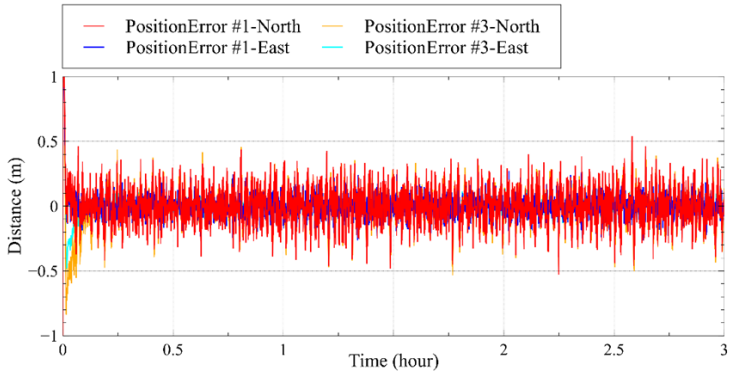


Figure 31: Errors of the estimated positions relative to the "measured" positions

The mean positions of the three locators measured during three tidal periods in the field trial (see e.g. in Figure 28) and were used to determine a representative configuration of the positioning system in the simplified numerical estimation model (Figure 33), where each locator is related to a fixed point on the net cage. Figure 34 shows an example of the estimated net deformation based on the two measured positions (Locator #1 and Locator #3) from the field trial. The time series of measured positions and the corresponding errors of estimations are shown in Figure 35 and Figure 36, respectively. It should be noted that only two locators were used in the estimation model, while the third

one (Locator #2) was used for verification. As shown in the example, for all three locators, the maximum estimation error was below 3 m (Figure 36), which was in the same range as the deviation of the measured data in a period of 1 hour (Figure 35). Figure 37 shows another example of the positions measured on another day where the deviations of one locator (x-position of Locator #3) were significantly higher, while the estimation results (Figure 38) were found to be still as good as the previous one (Figure 36). The estimation model has been verified by 11 data sets (each lasted one hour) from the field trials, and it proved to be suitable for real-time applications.

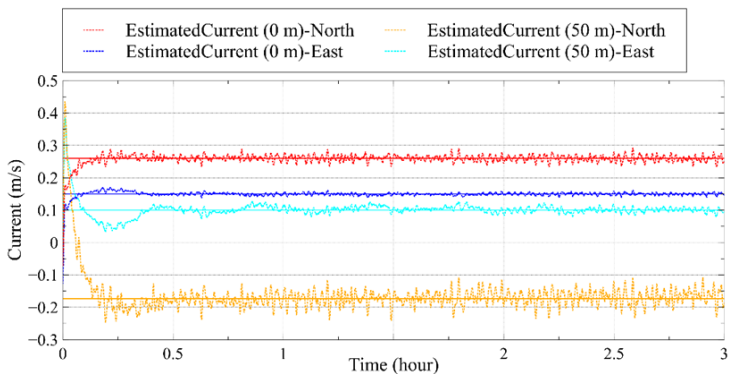


Figure 32: Estimated current velocities (dotted lines) and the comparison with the "actual" current velocities (solid lines)

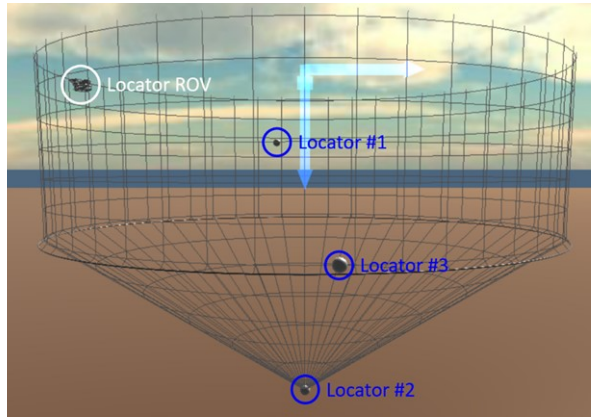


Figure 33: Configuration of the positioning system in the numerical estimation model

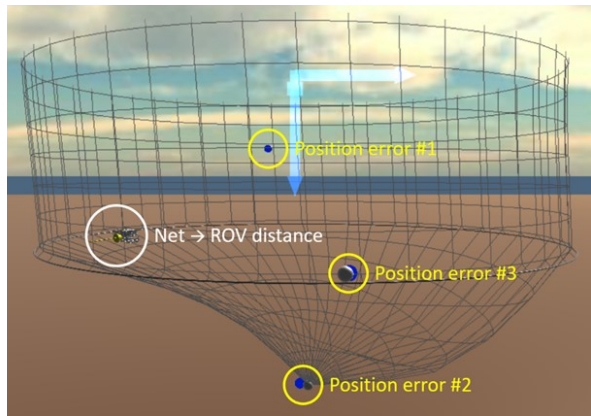


Figure 34: An example of the estimated net deformation where the blue points denote the measurement data and the grey points denote the estimated positions of the net cage

Figure 35: An example of the time series of measured positions

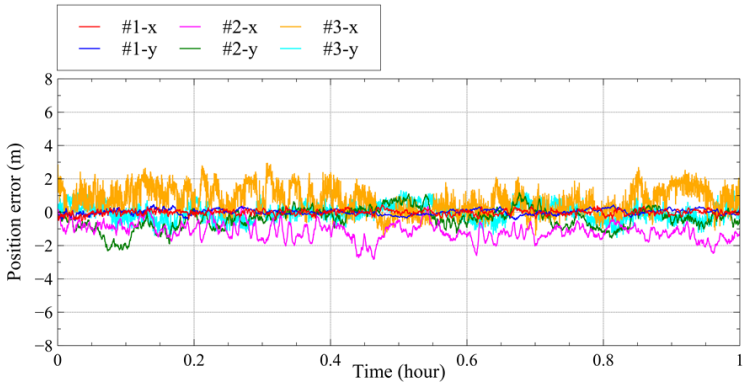


Figure 36: Errors of the estimated positions relative to the measured positions (corresponding to Figure 35)

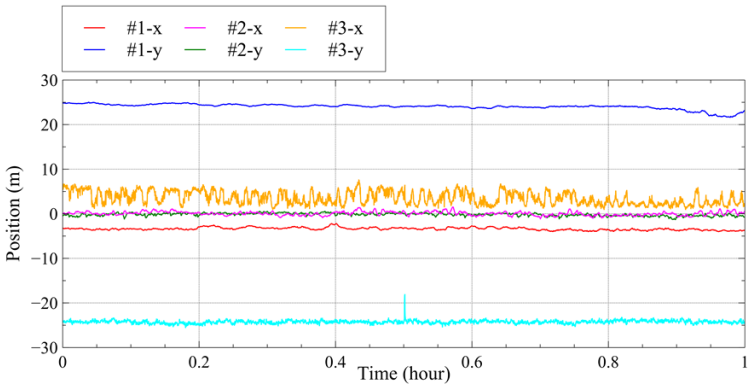


Figure 37: An example of the time series of measured positions with higher noise level

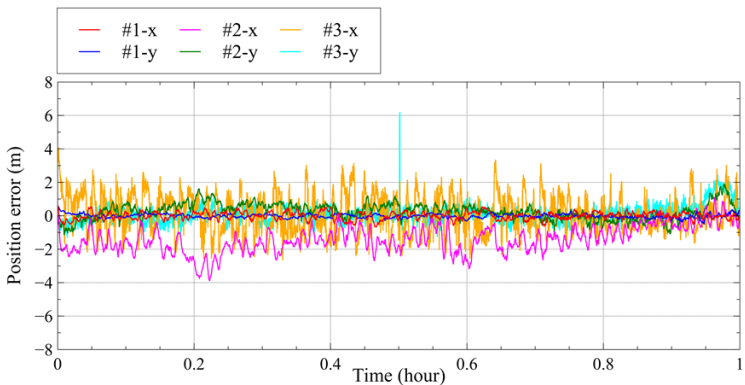


Figure 38: Errors of the estimated positions relative to the measured ones (corresponding to Figure 37)

The estimation model is furthermore able to calculate the distance between the ROV and the closest net panel, considering net deformation and measured positions of the ROV. Figure 39 shows an example of the recorded trajectories of the ROV and the three locators on the cage, where the ROV was first aiming to keep a constant position (Figure 39) and then follow a straight line (Figure 39) by using a DP (dynamic positioning) controller (Fossen 2011). The calculated distance between the ROV and the net is shown in Figure 40, where the ROV is aiming to keep its position in the first 40 seconds and follow a straight line afterwards. Herein the minus distance means the ROV is inside the cage: when following the straight line it was

moving further away from the net before it reached the central line of the cage and then moving closer to the net on the other side. By taking into account net deformation and the resulting orientation of surrounding net panels, this result is reasonably accurate and shown to be suitable for autonomous net-following navigation. As shown in Figure 41, all the measured data and estimation results can be instantaneously visualized in FhSim, which is also useful for real-time applications with regards to both autonomous navigation and manual operations. During the field trial, FhSim had been used as a tool to display cage deformation and for instant observation of the distance between the ROV and the net.

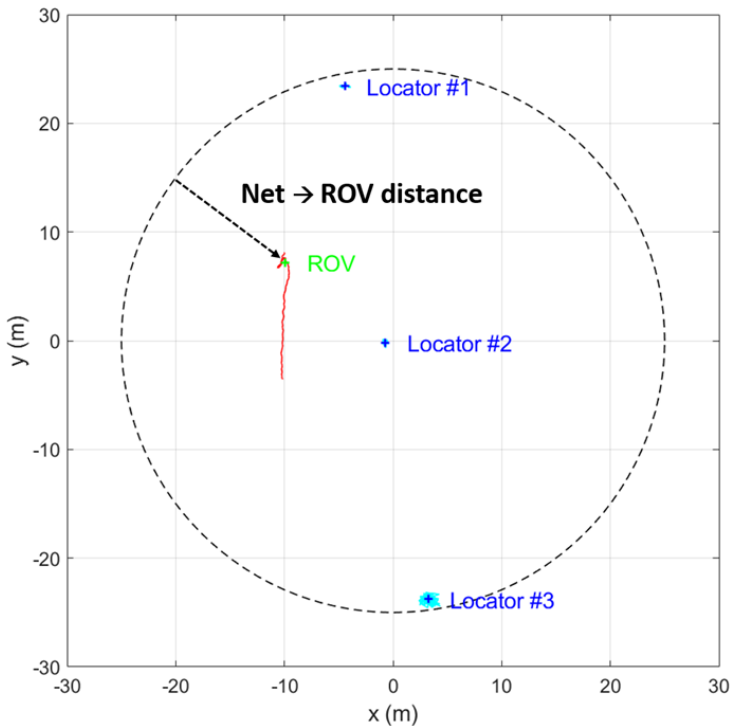


Figure 39: An example of the recorded trajectories of the ROV and the three locators on the net cage where the green cross denotes the constant position from the net and the red line denotes the followed straight line by the ROV

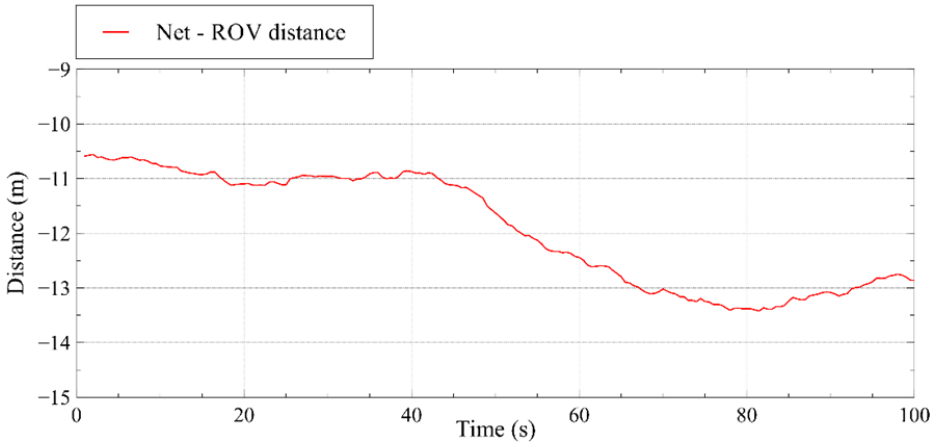


Figure 40: Time series of the calculated distance (minus distance means the ROV is inside the cage) between the ROV and the closest net panel (corresponding to Figure 24)

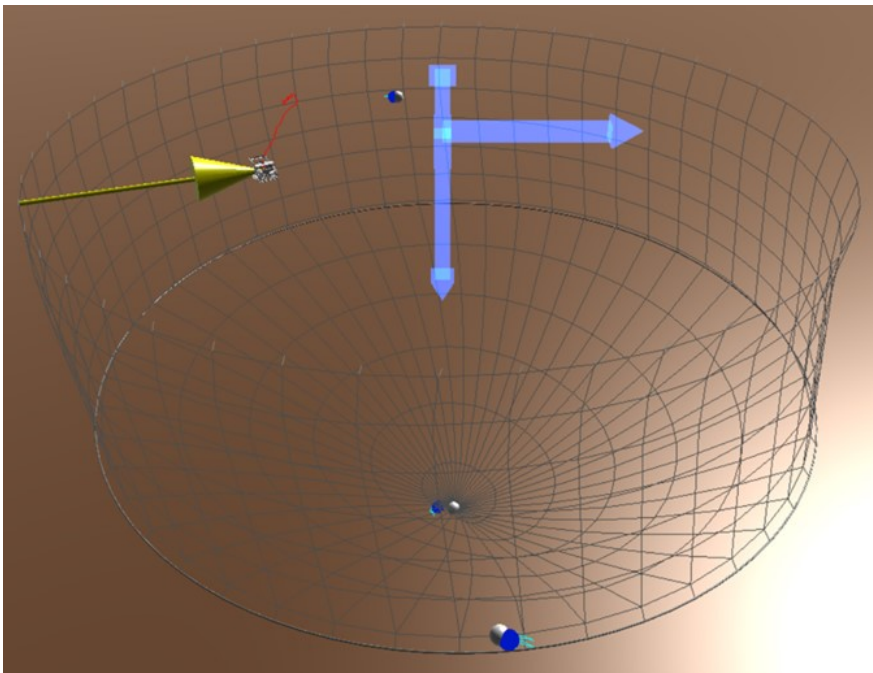


Figure 41: Real-time visualization of net deformation and ROV operations in FhSim (corresponding to Figure 24)

CONCLUSION

This report presents the development and validation of a low cost and hydroacoustic subsea communication system adapted for use in the cage. In particular, the obtained experimental data have been used to develop and validate numerical methods that estimate a high-resolution real-time map of the fish cage. The developed underwater positioning system from WaterLinked AS (i.e. wLink) have been used in combination with numerical methods to realize a position reference system, and the research need lies in

developing a wLink configuration that provides good performance in combination with the numerical methods. The position reference system is validated through multiple trial series where positioning accuracy is validated. The obtained results both for the real-time map estimation and underwater positioning of the vehicle showed good accuracy and will be further used for autonomous navigation concepts of underwater vehicle moving in the cage that are developed in this project.

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H2: DATA CAPTURE AND REAL-TIME DATA QUALITY ANALYSIS

E. KELASIDI, E. MOEN, C.SHELLEWALD, M. YIP, B.M. REMMEN

A key element of the project is to capture high-quality vision data from the cage. To obtain relevant high-quality vision data using the currently available state-of-the-art systems (e.g. systems based mostly on stationary sensors) is highly demanding process, and in many cases fails to obtain data describing the dynamic farming environment with sufficient resolution and accuracy. Bio-mass production at a single site can have up to 15.000 tonnes of salmon, in a water volume up to 50.000 m³. In the future, these volumes are expected to increase even more, meaning that such large volumes cannot be considered as homogeneous environments, and thus it is not possible to obtain accurate and detailed information based on vision data collected using stationary sensor systems. The distribution of fish and variables related to the production environment vary in the cage, both through the day and with season. An autonomous underwater vehicle being equipped with a 3D vision system will be able to collect data from the whole volume of the cage. It is essential to develop a system that is able to capture data that describes the conditions of fish, cage net and production environment since this information can be used for a better mapping of environmental effects (escapes, feed lice, lice), improvement of fish welfare and economics. An important feature of the developed system is the real-time quality control of the obtained data in order to sort out data that does not meet objective quality criteria. Based on quality-assured data, a better decision support system can be developed for more objective decisions during operations in fish farms.

H2.1 SENSOR SYSTEM FOR 3D VISION

This section present results regarding the development of an underwater 3D vision system for use in fish cages, aiming to monitor the condition of the fish, inspect the fish cage facility as well as provide vision for a Remotely Operated Vehicle (ROV), which it will be mounted to. The R&D challenges to develop a 3D vision sensor system are related to the development of a camera and lighting systems that provide high-quality data under varying light conditions and visibility in the water (Figure 42). This is particularly demanding for high turbidity water, which provides optical dispersion and damping, limiting the observation volume. To prevent artificial lighting interfering with the fish, wavelengths invisible to the fish are assessed in combination with light-sensitive camera sensors. The project partner, SEALAB, has since its founding had ambitions to utilize and develop an underwater stereo vision system. Different applications have been tested earlier, including plenoptic cameras as well as rigs with two 2D cameras. This, SEALAB had knowledge and experience concerning stereo applications prior to this project. However, prioritizing other necessary work areas over stereo projects meant that the CageReporter project was essential to push this in a progressive direction. In this activity, SEALAB has provided hardware and software to capture and store the desired stereo data. This data has subsequently been used both by SINTEF and SEALAB for developing algorithms to achieve stereo vision.



Figure 42: Frame from video of salmon with SEALAB camera system

SENSOR SYSTEM WITH HARDWARE AND SOFTWARE

For the development of the 3D vision system (Table 5) two 4K cameras were mounted on a stereo rig to capture the left and right video stream representing the main components in a stereoscopic vision. The specifications of this camera are summarized in Table

5. This equipment has to be encapsulated in a waterproof casing and arranged in such a way that it can be mounted as payload on a ROV. Figure 43 shows a 3D rendering of the stereo camera setup, taken during development stages.


3D stereo system with two 4K cameras and lights	Camera specifications	
	Sensor:	1/2,5- type Exmor R CMOS
	Video format	4K, 1080p, 720p, 480p
	Optical zoom	20x
	Video Output	Y/Cb/Cr 4:2:2, R/G/B 4:4:4
	Dimensions:	
	Length	250 mm
	Diameter	125 mm
	Weight in air	11 kg
	Weight in water	2.3 kg

Table 5: Underwater camera used to develop the 3D vision system



Figure 43: Render of the stereo camera

SETUP

As indicated above, two 4K cameras have been used to build the stereo vision system. Figure 44 shows an illustration of the system architecture. *Topside* refers to the location of the operator and represents the control center of this system as well as where the data is collected and image processing techniques will be executed. This topside was located on the boat MS *Torra* for full scale demonstrations in this project. The *Main Pod* connects all the components together and communicates with the *Camera Housings*,

Lights and the *Topside*. The *Camera Housing* and *Light* are the components where the cameras and the lights are located. A figure of the lights and a summary of their specifications can be found in Table 6. This system was mounted to an underwater vehicle in this project, however, as the system is inde-

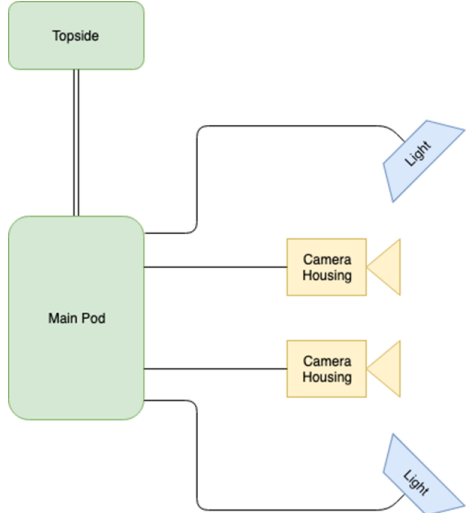


Figure 44: System architecture


Light System Photo	Specifications	
	Brightness	8000 Lumen
	Control Interface	RS485
	Electric Specifications	48VDC, 1.4A (Max)
	Dimmable	255 steps

Table 6: Light system used to develop the 3D vision system

pendent it could also be used independently. The umbilical from the *topside* to the *main pod* will be attached on the underwater vehicle's umbilical.

TOPSIDE

At the *Topside*, video and control signals from both camera housings as well as the control signals for the lights are transferred by fibre optic cables. This is achieved over three separate fibre optic cables, one for each camera housing and one for the light control. Together with these signal cables, a set of copper cables are required to supply

the system with 48 VDC. Between the *Topside* and the *Main Pod*, a hybrid subsea umbilical is used consisting of 4 single mode fibre optic cables, 4 multi-mode fibre optic cables and 4 copper wires

(Hybrid cable Type 3444; MacArtney). Table 7 shows some of the specifications of this cable. It was decided to use a Y-split at the end of the umbilical connected to the *Main Pod*, as they did not have a hybrid connector which fulfilled the requirements regarding the number of copper pins and optical fibre connections. Figure 45 shows the Y-Split, where the black connector is for the optical fibre and the red for the copper.



Figure 45: Y-Split

Umbilical Illustration	Specifications ¹	
	Brightness	8000 Lumen
	Control Interface	RS485
	Electric Specifications	48VDC, 1.4A (Max)
	Dimmable	255 steps

Table 7: Hybrid cable used between topside and camera system

¹MacArtney Underwater Technology, "Hybrid cable, Kevlar - Type 3444", <https://www.macartney.com/what-we-offer/systems-and-products/stock-cables/hybrid-cables/hybrid-cable-kevlar-type-3444/>

The topside computer that was used was configured and installed for this specific purpose. Table 8 shows the specifications of this computer containing a *Pro Capture Dual HDMI 4K Plus LT*. This is a video capture card from *Magewell* which connects the camera inputs. This card has both Windows and Linux compatible drivers and has proven to be a good choice. In addition, the software used to capture video was OBS Studio v24.0.3 as well as FCB control software v6.1.0.0 for configuring the cameras.

CPU	INTEL Core i9-9900K
GPU	MSI GeForce RTX 2080 Ti VENTUS 11G
CAPTURE CARD	Pro Capture Dual HDMI 4K Plus LT
MEMORY	32GB DDR4
STORAGE	14 TB (4GB SSD + 10GB SATA)

Table 8: *Topside computer specifications*

MAIN POD

Connecting the *Topside* with the cameras and the lights is the main functionality of the *Main Pod*. Figure 46 illustrates the hardware contained in the *Main Pod*. The *Power* block distributes power through the system with the corrector's voltage levels and the required capacity. The *Light Control System* sends commands from the *Topside* to the lights. The *Camera Synchronization Generator* supplies both cameras with synchronization signals, an essential component in stereo vision. Lastly, the *Fibre Optic Termination* block connects the fibre optic cables from the cameras to the *Topside* umbilical. This

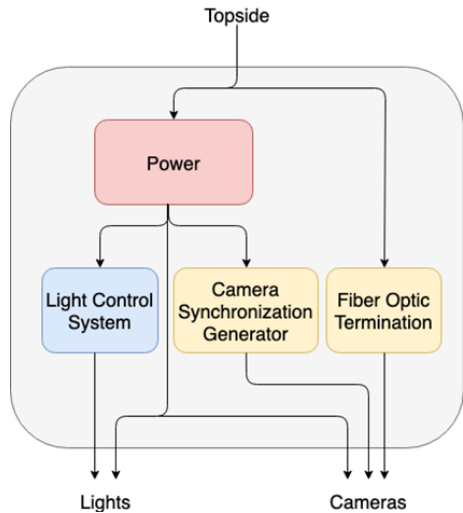


Figure 46: *Main Pod*

hardware is encapsulated in a waterproof container with connectors to the topside umbilical for both cameras and both lights. Table 9 shows a figure of the developed casing and some specifications.

Length	320 mm
Diameter	125 mm
Weight in air	7.5 kg
Weight in water	2.7 kg

Table 9: *Main Pod Specifications*

Figure 47 shows the *Main pod* connector interface towards the topside umbilical. This is where the Y-Split is supposed to be connected. The left connector is for the optical fibre and the right connector for copper. Figure 48 shows the *Main pod* connector

interface towards the cameras and the lights. The lights are connected to the two top connectors. The two connectors at the bottom are the optical fibre connectors for the cameras. Lastly, the two middle connectors are the copper connectors for providing power and sending steering-signals to the cameras.

CAMERA HOUSING

The *Camera Housing* is a waterproof encapsulation, which contains a camera and a video signal transmitter. The *Camera Housing* is connected to the *Main Pod* with two cables, a fibre optic cable for the video signals and a copper cable with 8 separate wires for power and synchronisation signals. The *Camera Housing* requires two connectors, both for the fibre cable and the copper cable. Figure 49 shows the connector interface of the stereo camera, consisting of two camera housings mounted together. The fibre connector used is *OptoLink single fibre BCR drybox* from *Macartney* and the copper connector is the *Macartney MCBH8M*.



Figure 47: *Main pod* connector interface towards the topside umbilical

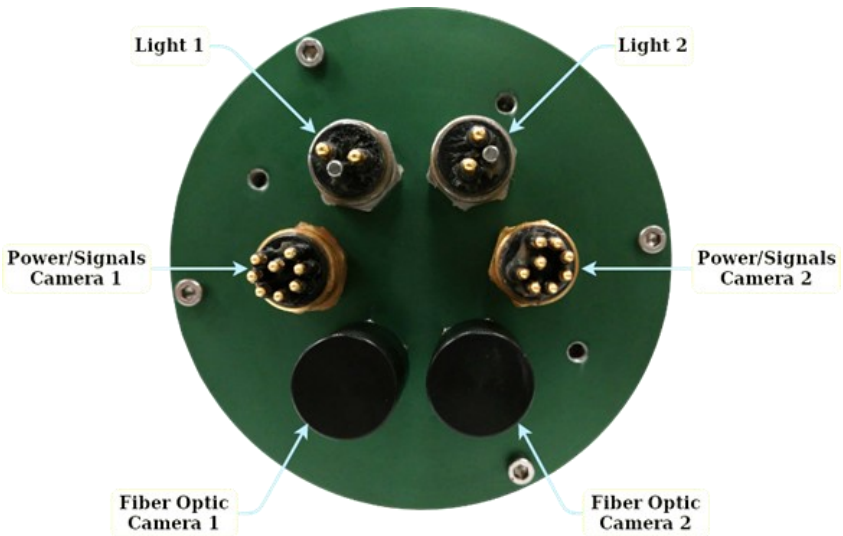


Figure 48: *Main pod* connector interface towards the cameras and the lights. Connectors are identified by labels

LIGHT

The lights consist of an LED-chip encapsulated in a waterproof housing. Two of these are connected to the *Main Pod*, each using a subsea cable from *Macartney* with the connector *MCIL2F*. These LEDs are able to produce a luminous flux of up to 8000 lumen per chip, they are dimmable and easy to integrate using a RS485 interface. Figure 50 shows a single frame from a video recording at night-time within a fish cage. This light allows monitoring of salmon when daylight is absent, thus collecting information about the Salmon at night time, but also in winter time when daylight is limited.

CAMERA HOUSING

To be able to control the camera and lights from the topside, the system provides an interface to the user. Figure 51 illustrates the *Topside Interface*. Four fibre optic cables are available. These are distinguished by colours;



Figure 49: Connector interface for the stereo camera

green, blue, brown and orange. Green and blue are the stereo video channels. The brown cable is for the light control and the orange cable is currently not in use but available for additional functionality. To fetch frames from the camera channels, an optical fibre to HDMI converter was used. The HDMI outputs from this card is then connected to a grabber card inside a computer. This made the video streams available as devices in `/dev/video0` and `/dev/video1` at the Linux operating system. Thus the user may access



Figure 50: Night-time video recording using SEALAB lights

the streams as required by the application. It can be seen from Figure 51 that the computer is connected with an ethernet cable to the *Brown* fibre cable. By connecting to the light control system located in the main pod via SSH, the user can control the lights.

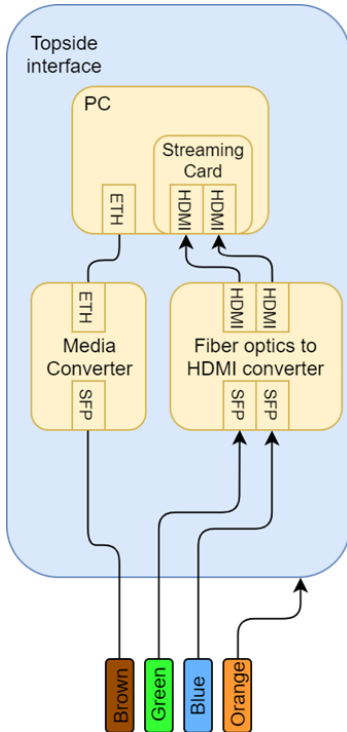


Figure 51: Topside Interface

INTEGRATION AND TESTING

A test of the cameras was performed to ensure its correct functionality. This included verification that both cameras were synchronised, and to see that the system did not produce any unwanted effects. Figure 52 shows the result from this testing. The two upper images are the left and right camera frames recorded at the same time. The lower images are from the left and right camera at

the next frame. It can be seen that the flash-light of the mobile phone turns on when comparing the second to the first frame. Both cameras captured this transition of light, confirming that they are synchronised. No artefacts or unwanted effects were discovered confirming the functionality of the system.

Afterwards, all of the individual components were connected and tested together to confirm correct functionality. Figure 53 shows the stereo camera system integrated on the ROV. During the field tests conducted at the SINTEF ACE facility Rataren on autonomous navigation control concepts, one of the fibre cables between the *Main Pod* and the *Camera* got damaged and malfunctioned. Therefore, it was not possible to do recordings with this setup during the field trials. Since all of the parts are customised and expensive which means long production time and thus full-scale validation of the system had to be postponed. However, to ensure the results of the project, a stereo setup with two Go-pro cameras was used during the full-scale trials to obtain the images necessary for the validation of the developed image processing algorithms reported in the following sections.



Figure 53: Stereo camera integrated on the ROV

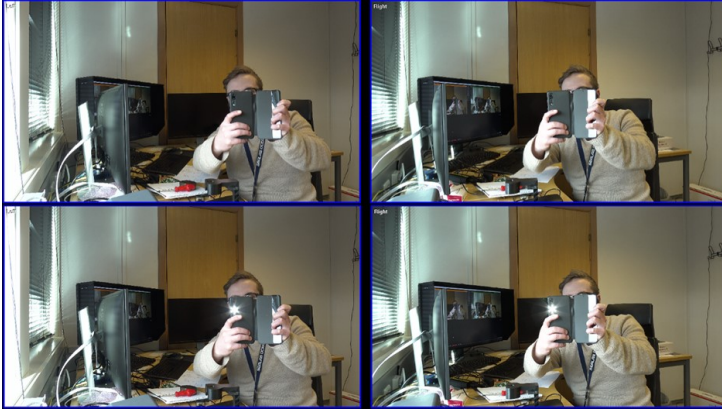


Figure 52: Stereo camera test, showing two subsequent frames recorded by the left and right camera simultaneously

H2.2 REAL-TIME ANALYSIS OF DATA

In order to develop a vision system that is able to obtain high-quality data, there are R&D challenges related to the data quality analysis. Data quality is here defined as a term, not only related to image quality, but also to the extent that the obtained data is relevant and thus can be used to assess fish, structure and environment conditions. A study has been carried out to define objective criteria for data quality, as well as to develop the algorithms that assess data quality. Note that this is particularly demanding for identification of fish conditions, where the objective criteria, in addition to the image quality of the fish, should ideally also assess the behaviour of the fish, including for example the flight response. For the structure conditions, it is vital to ensure that the images are of sufficient quality to enable, for example, the detection of holes in individual trends in the net. Therefore, the task for this work package was to explore whether we are able to develop algorithms for analysing the quality of the recorded data from fish cages. This was performed in two stages: 1. the first stage consisted of a brief study to define the quality requirements of the data in relation to monitoring the condition of the

fish, inspection of the cage facility and/or environment and 2. the second stage was to implement algorithms which evaluate the data towards the criteria set in stage one. In order to identify the quality requirements for videos for monitoring fish/structure and/or the environment within fish-cages, this study specifically provides insight into what minimal quality requirements are needed to record video-data that can be analysed automatically by classic computer vision algorithms and state-of-the-art machine learning algorithms. Generally, the quality analysis of captured video-data can be divided into two parts. The first part refers to the *technical aspects* of the image quality which depends mainly on the hardware, but also on some fixed camera parameters used during the recording, and the employed compression algorithms when sending the video-stream to any processing unit. The second part involves the *analysis of the quality* of the recorded video material itself. Note that as the interpretation of the content of the videos is beyond the scope of this project, our analysis focused on measures that were able to work on the pixel level of the images.

TECHNICAL IMAGE DATA ASPECTS

The resolution of the provided video-stream is one key-variable to evaluate the capability of the cameras. A higher resolution generally indicates that we can see more detail within an image. Digital cameras often allow to select a specific resolution. Image/Video resolutions that can be considered to be of good quality (from today's perspective) include:

- *HD [1280 × 720 progressive scan]*
- *Full HDi [1920 × 1080 two interlaced fields of 540 lines]*
- *Full HD [1920 × 1080 progressive scan]*

The progressive scan (vs. interlaced), i.e. consecutive image pixel lines being recorded subsequently, has the advantage that the image can be used “as it is” for image processing and analysis. Interlaced recordings are performed by updating only every second line in the video-image at each timestep. This effectively represents a reduction of the resolution in y (vertical) direction and requires the images to be deinterlaced before processing. An example is shown in Figure 54.

Currently, many fish-farming companies still rely on grey-value-video-streams from the fish-cages that have a D1/DV PAL Wide-screen resolution (i.e. 720x576). Such a low resolution combined with an interlaced mode makes the automatic analysis of the data difficult, even if some aspects can be seen by a human. Examples are shown in Figure 55.

Objects that one wishes to identify should cover a minimal area of about 32x32 to 64x64 pixels in order to enable machine

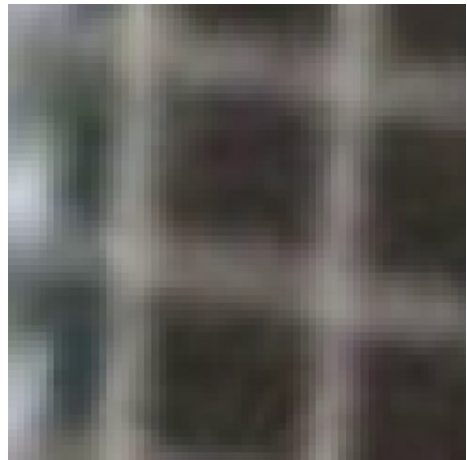


Figure 54: A small part of a net of a fish cage recorded in “interlaced” mode (upper image). “A deinterlacing is necessary before the image can/should be further processed. Deinterlacing the upper image results in the image seen on the lower image

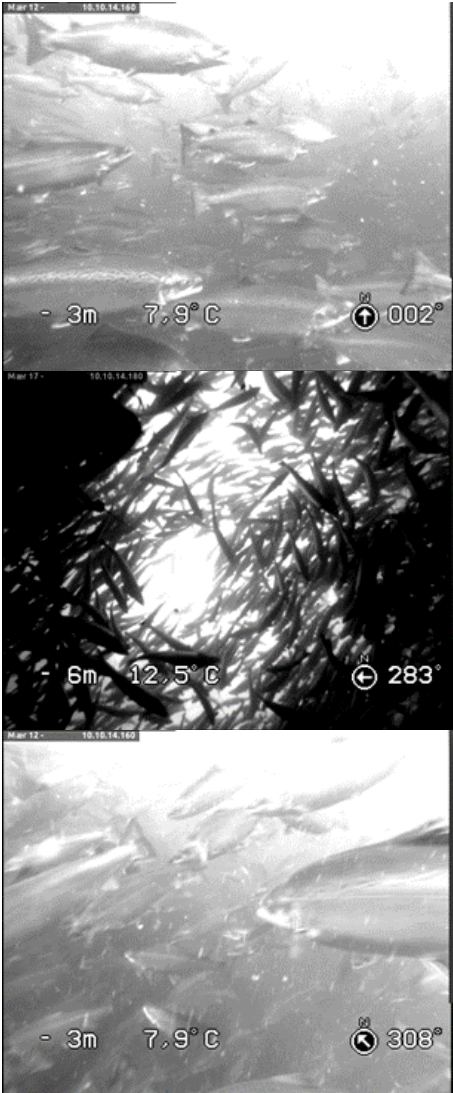


Figure 55: Example images from video-cameras commonly used for cage-observation. These often have a relatively low resolution (i.e 720x576) and a low dynamic range that quickly leads to overexposed areas in the image

learning approaches to be trained with labelled regions of that size. For underwater fish cage observations, a typical video frame rate is about 25 fps (frames per second), which is sufficient for many applications (higher frame rates are desired when fast motions are to be analyzed). A fixed focus defines the distance where the sharpness of an object is optimal. If the autofocus is switched on the intrinsic camera parameters may change. However, standard 3D reconstruction methods require/assume that the intrinsic camera parameters do not change and autofocus is usually avoided in these cases. The Aperture, often represented by f (e.g., $f2.8$, $f8.0$ etc. where larger numbers correspond to smaller aperture openings), influences the amount of light that passes through the lens and is received by the image sensor. The aperture size also has an impact on the sharpness-range. Smaller openings lead to a larger range where objects appear sharp in the image. Lower light conditions generally require longer shutter times and lead to observable motion blur in the images. In addition, this is dependent on the sensitivity of the image sensor, with a higher sensitivity increasing the observable noise in the images. For all scenarios considered, including A) the State of the fish (behavior/welfare) in a fish cage, B) Inspection of structures in cages and/or C) the production environment, one should aim to record images with the highest possible technical image quality. Note also that color cameras can provide additional information that is useful for special tasks (e.g. open wound detection). Size estimation, speed, distance and density related to the cases A-C may require underwater stereo imaging/3D cameras as these allow for metric measurements.

COMON DEFECTS IN DIGITAL VIDEO STREAMS

To set criteria for video data recorded in fish cages, a summary of common defects in digital video streams is necessary. Figure 56 shows an overview of different compression artefacts that can be found in the literature. They are separated in two main branches,

spatial artefacts and *temporal artefacts*. The former describes location-based artefacts while the latter describes time-based artefacts². In this section three common compression artefacts will be presented in detail and with examples. Further, a assessment of the existing results with regard to how image quality affects Deep Neural Network applications will be performed.

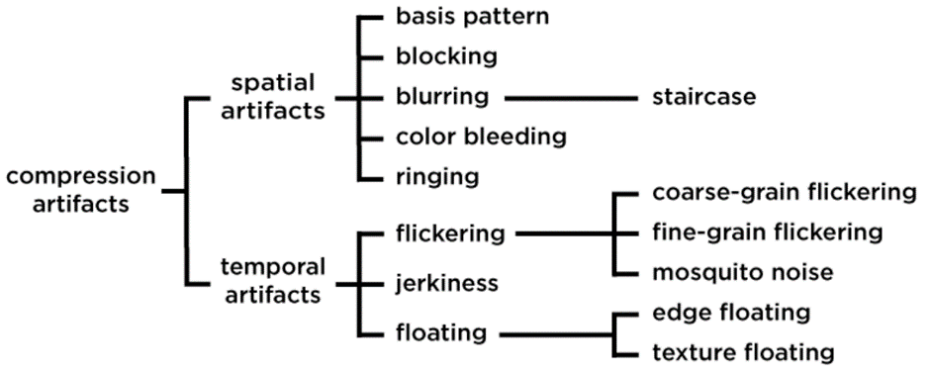


Figure 56: Overview of different compression artefacts

BLOCKING

One of the most common video artefacts in real time video streams is blocking. This artefact is recognisable as small squares or blocks in the video image instead of smooth edges and detail. It can be seen in Figure 57 where the image has "square blocks" in the

highlighted area within the black box. This can occur in small areas of the frame or be present in the whole frame. Often triggered by fast motion in the frame and when there is a lot of motion in the image sequence. The main reason for these artefacts is the compression of the video stream. Figure 57 shows blocking in the red highlighted squares.

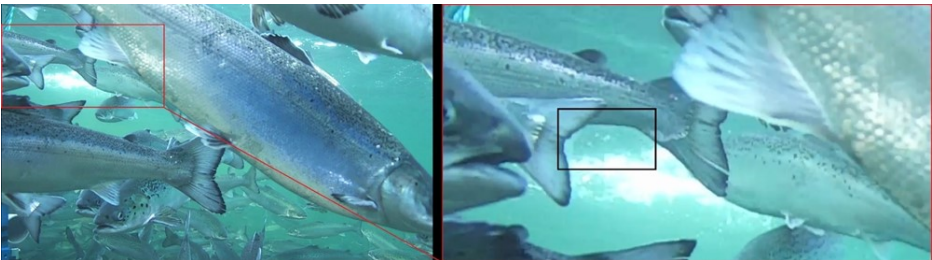


Figure 57 :Illustration of blocking indicated by the black rectangle

² <https://blog.bjamp.com/understanding-video-compression-artifacts/>

PIXELATION ERROR

A less common (compared to *blocking*) video artefact are *Pixelation Errors*. They typically occur when data is lost in transmission and the receiving end cannot correctly decode and recreate the correct pixel values. Figure 58 shows an example where a keyframe was lost from the data transmission during the decoding of a video stream. This is recognizable in the subsequent video frames as many areas show the wrong color/grey values. Small transmission errors usually have a smaller effect but may still result in color-values that are off compared to the surroundings.

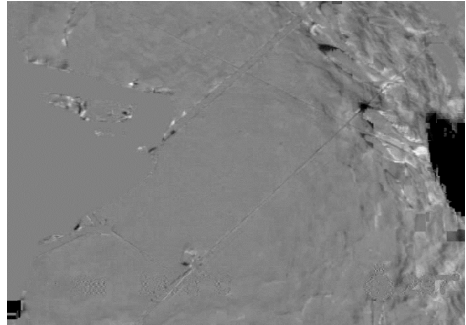


Figure 58: Illustration of a pixelation error. A missing keyframe results in pixelation artefacts (snapshot from a feeding camera)

ANALYSIS OF THE QUALITY OF CAPTURED (VIDEO)-DATA

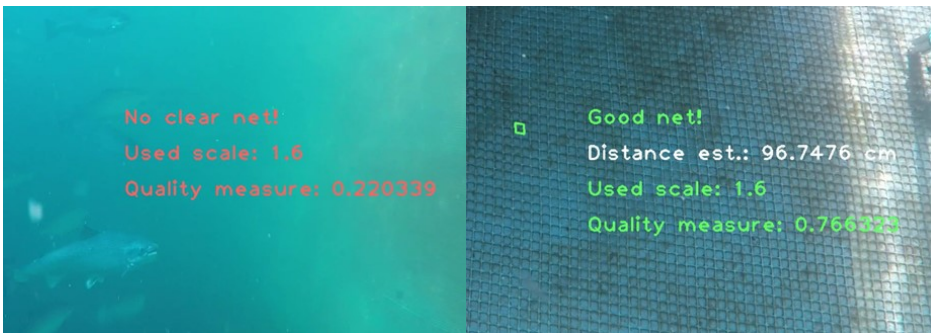


Figure 59: Analysis of an ROV video providing an indication whether a regular net-structure is visible or not

The aim of determining the 'image quality' of videos in the context of aquaculture is to evaluate how suitable a particular image sequence is to provide information for a specific computer vision task. Here we consider application tasks where we wish to obtain the information related to A) the State of the fish (behaviour/welfare) in a cage, B) Inspection of cages and/or C) the production environment.

Towards this aim we designed an approach to analyse video data based on their spatial

spectra resulting in an algorithm that can distinguish whether one is seeing a net of a fish cage or if the regular net structure is not present. Knowing the camera-parameters and the mesh size of the net, an estimate for the distance can be computed. An example from a test-video recorded with an ROV in a fish cage during the test trials is shown in Figure 59. In addition to the specific net-inspection quality analysis, we also searched for and explored approaches that may serve as a more generic indicator for the quality of recorded video-sequences.

VISUAL SEQUENCE EXPERIMENTS

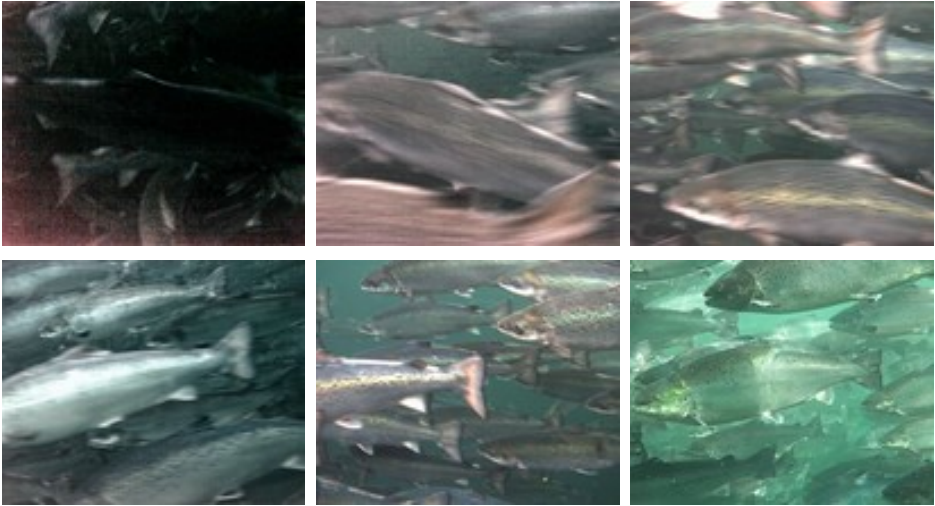


Figure 60: Illustration of six concatenated video-segments ordered according to increasing video quality (subjective opinion). Each film-segment has 100 frames and was evaluated by six video-quality measurements candidates

For an initial evaluation of algorithms providing low level quality indicators, we concatenated six image/video-sequences (with increasing quality [subjective opinion]) and evaluated some quality measurement candidate approaches on them. The six film parts (each part is 100 frames long, corresponding to a duration of ~4s) of the test video are illustrated in Figure 60. Note that we ordered the six video-segments based on our subjective opinion with increasing quality (i.e. the first very dark segment, represents the part with the lowest video-quality and the last segment corresponds to the part showing a high-quality underwater recording.)

The measurement criteria of video-quality we finally tested include the following six approaches:

- Fast Noise Variance estimation (Immerkær96)
- Modified Laplacian (Nayar89)
- Tenengrad: Sum/thresholded gradient measure (Tenenbaum70)
- Variance of Laplacian LAPV (Pech2000)
- Normalized Gray Level Variance (Santos97)

We applied the above measures to the test video sequence. Figure 61 shows the results we obtained for each of the six measurement criteria of video-quality applied to the concatenated video-sequences. Each sub-figure shows the measurement for a single criterion applied to the video-sequence with 600 frames. As we ordered the video se-

quences according to increasing quality, we searched for a criterion that would reflect this sequence. This means that the measure should increase (or decrease) for each of the subsequent video-segments. However, the experiments did not consistently reflect our subjective ordering of video-quality. Regarding the “expected” behaviour, the Tenengrad approach turned out to be closest to the desired outcome, but likely more advanced machine learning algorithms are necessary for mirroring a human quality assessment of such underwater videos.

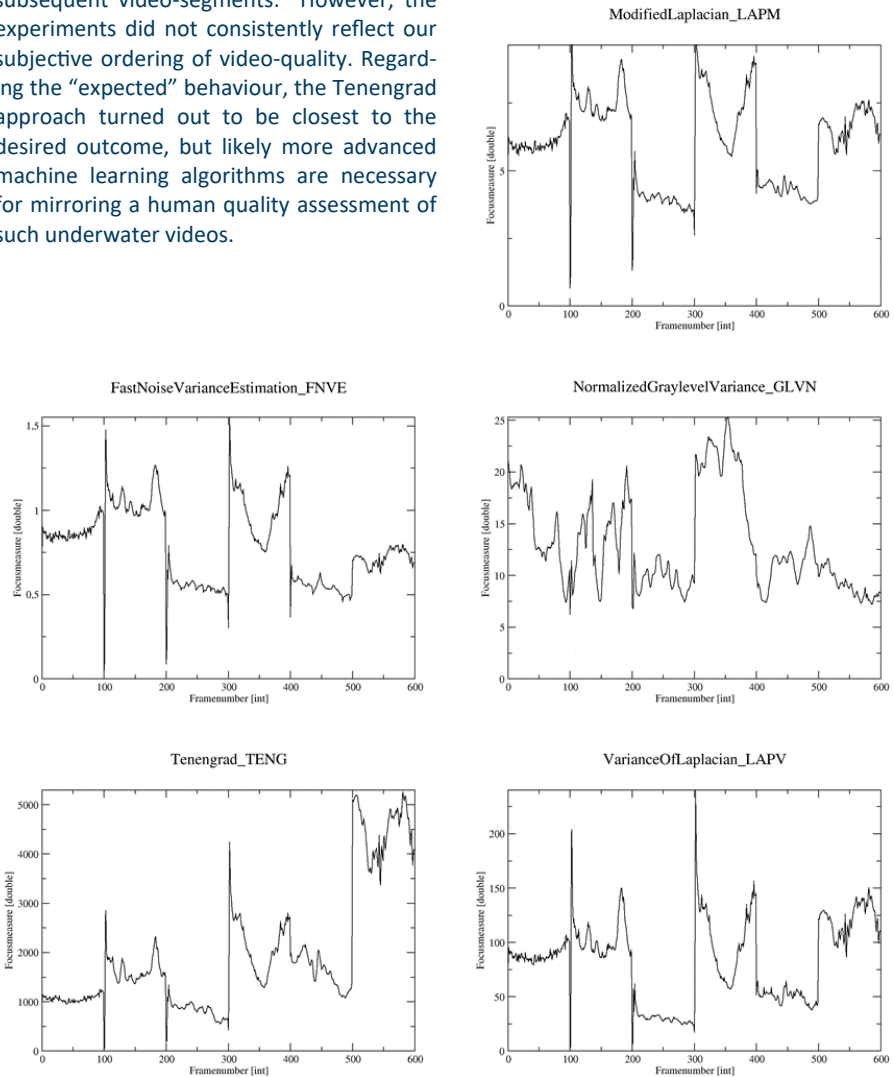


Figure 61: This figure shows the results of the five measurement criteria of video-quality applied to the concatenated video-sequences. None of the measures comply with an “expected” consistent increase (or decrease) of the measurement values

REAL-TIME CONSIDERATIONS

In this section we briefly consider which of the explored algorithms can be applied in real time.

Algorithms that perform on video-streams with a processing-rate faster or equal to 24 frames per second are considered to run in “real-time”. Note that a video-stream may be downsampled -- still showing the essential details we wish to analyse – before a quality measurement algorithm is applied.

Below we list the processing speed we obtained on a desktop-PC indicating that all are able to work close to real-time (except for two that would need some code optimization):

- “Fast Noise Variance Estimation:”
//Realtime >=24fps
- "Modified Laplacian: " // ~10fps
- "Tenengrad: " // ~15FPS
- "GLVN: " // Realtime >=24fps
- "LAPV: " // Realtime >=24fps

H2.3 ESTIMATION OF THE DISTANCE AND ORIENTATION FROM THE INSPECTION OBJECT

DECISIONS OF THE 3D CAMERA SYSTEM

At the time of the project-application the most promising candidate for a 3D image acquisition system was the Raytrix camera (PRODUCER) that exploits the plenoptic camera technology. Due to the costs of a single camera-system and additional difficulties of getting depth images of sufficient quality in real fish cage environments, Sealab AS decided to explore other solutions. One option

was the use of the ZED-camera (PRODUCER), but drawbacks such as the constraints resulting from the use of an USB 3.0 adaptor and the difficulties to perform the underwater-calibration properly finally resulted in the decision to build a side-by-side underwater high-end stereo camera from scratch. Unfortunately, this led to a delay of a operational camera-system but finally resulted in likely the best 3D underwater-camera built for use in aquaculture (compare section 2.1).

MOTIVATION

The underwater camera system that was developed to obtain high-quality data from fish cages, will be used to measure the distance and the physical dimensions of inspection objects, which is central for several operations in cages. In addition to the high-quality data capture, the camera system will be used as the 'eye' of an underwater vehicle in order to estimate the distance, orientation and relative speed from the inspection object. SEALAB has a vision to help fish farmers see and understand what happens under water. One of the problems fish farmers can have is the escape of fish from the cage due to damage of the net. Therefore, autonomous inspections of the net are a desired feature (Figure 62). One of the first problems to solve towards this aim is to estimate the distance to the net and the relative orientation to the two cameras placed on the Remotely Operated Vehicle (ROV). These inputs are crucial to the control system that enables

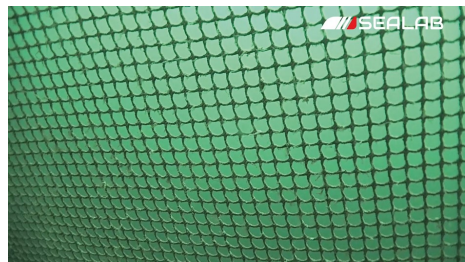


Figure 62: Picture of the net of a fish cage, recorded with a SEALAB AS camera

the ROV to navigate autonomously inside the cage and inspect the whole net area. In a later stage when the steering is working robustly, the goal is to detect holes before the fish can escape, thereby decreasing the total amount of fish escapes. SEALAB is currently developing algorithms that can detect holes in the net.

ESTIMATION OF DISTANCE AND ORIENTATION FROM THE INSPECTION OBJECT

Multiple approaches are possible to estimate the distance from the ROV to the fish net. The approaches differ in hardware setup, e.g. single or multiple cameras. Because of the differences in the setup there are different assumptions that drive the use of different algorithms.

Distance estimation using a single camera

Initially, we investigated the potential of using a single camera to estimate the distance to the inspection object. We explored an algorithm based on a Fourier analysis to determine if a regular net structure is present in an image. Some of the strengths and limitations of the use of mono cameras are discussed here. The following two cases can be considered when using a single camera for estimating the distance to the net and its relative orientation to the camera:

1. Knowing the size of the nets mesh openings and the intrinsic camera parameters, it is possible to calculate the real distance to the net. This approach requires some assumptions including that a single mesh opening can be approximated by a flat rectangle/square.
2. By taking two pictures at slightly different time and knowing or tracking corresponding features on the net, it is possible to calculate the distance to the net by so called "structure from motion" algorithms.

Both cases are challenging with regard to a generic application in fish cages. The first one requires the knowledge of the mesh size which may vary from cage to cage. The second approach requires a reliable tracking of feature points which is especially challenging for repeating regular structures like a net. An advantage of using a mono camera is that processing is typically faster as the amount of data from a single camera is lower than the amount of data from two cameras in a stereo setup.

Distance estimation using stereo camera

Within this project we decided to use a stereo camera setup for the distance and orientation estimation of an inspection object (Figure 63). This enables to calculate metric distances from images more easily and more reliably without making many assumptions. The necessary extrinsic parameters can be obtained by calibrating the stereo camera and include the distance between the two cameras (baseline) and the relative orientation of the two cameras (Figure 64).

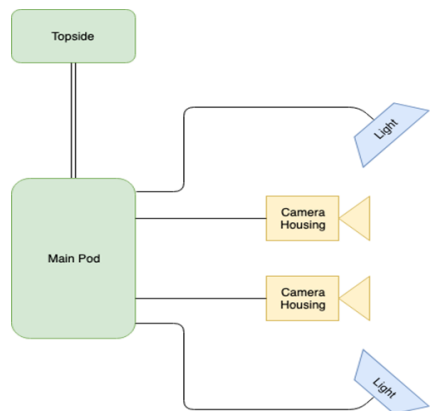


Figure 63: Illustration of the stereo camera architecture setup

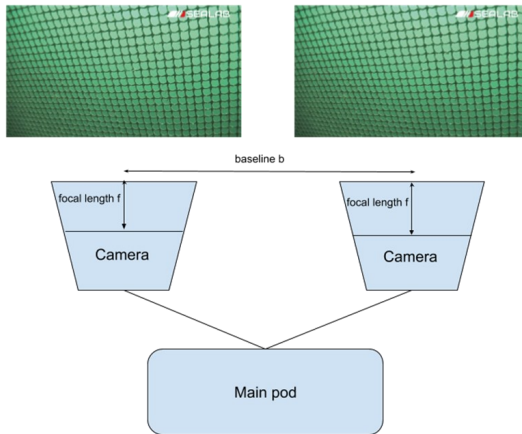


Figure 64: Illustration of the approach adapted to calculate the distance with a stereo setup

Following, we provide an illustrative example how one can in principle calculate the distance of an object seen in both images of a stereo camera. For the computations we exploited the following variables:

Baseline, b : The distance between the two cameras used for distance calculation.

Pixel size, ps : The size of the individual pixels in an image sensor given in μm . Note that the two cameras should have the same pixel size in the image sensor. The pixel size typically seen in most cameras is ranging between $6\mu\text{m}$ - $14\mu\text{m}$.

Focal length, f : The distance between lens and image sensor.

Pixel disparity, ds : This refers to the relative pixel difference between the two pictures, creating a map that shows the differences which in turn can be used to calculate the distances.

Depth calculation, d : The following equation can be used to calculate the distance to the object using the parameters above:

$$d = \frac{f * b}{ds * ps}$$

A simple example to for distance calculation³.

Focal length f = 4.3mm

Baseline b = 60 mm

Disparity value ds = 64

Pixel size ps = 0.006

$$d = \frac{4.3 * 60}{64 * 0.006} = 671.875\text{mm} \approx 67\text{cm}$$

This is a single calculation related to one point. However, if the calculation is repeated for an area in the two compared images, it will result in different measures for distance d .

To calculate a disparity map which shows the difference between the two pictures, it is possible to use a block matching algorithm from OpenCV. OpenCV is a library that can be used either from C++ or Python and has many computer vision algorithms readily available⁴. Note that the calculation of disparity maps generally requires more computational power than the computations with single image cameras, but it also depends on a number of other parameters such as image resolution, frame rate, etc.

³Vision-systems Depth Calculation - <https://www.vision-systems.com/content/dam/VSD/NextGen/5-3D-2.pdf>

⁴OpenCV documentation - <https://docs.opencv.org/3.0-beta/index.html>

DECISIONS OF THE 3D CAMERA SYSTEM

As indicated earlier, due to the technical issues the 3D vision system described in Section 2.1 was not functional during the full-scale field trials. However, we attached two GoPro cameras on the ROV as a backup plan. Even though the GoPro cameras show more motion blur than SEALAB's camera, the ad-hoc setup turned out to be sufficient for the aim of depth estimation and was able to show that the developed algorithms verify the underlying concept. The following procedure was adapted to estimate the depth using the recordings from the full-scale trials:

1. Stereo camera calibration
2. Rectification of stereo image exploiting the epipolar Geometry
3. Determine the disparity map and estimate 3D position

STEREO CAMERA CALIBRATIONS

A chessboard of known size can be used to perform the stereo camera calibration under water when the relative position and relative orientation of the two cameras are fixed. In addition, the intrinsic camera calibration parameters are used to correct for image distortions.

After image distortion correction and stereo camera calibration, the baseline and relative orientation are known, and can be used to rectify the stereo image. Note that functions for

1. finding chessboard corner locations
2. single camera calibration
3. stereo camera calibration

were exploited to obtain the results in this report. The chessboard pattern was placed in front of the stereo camera set to obtain underwater video recordings. Afterwards, the

images from these recordings were used to calibrate the 3D vision camera system. Some samples of images can be seen in Figure 65. The right image is suitable for calibration while the left image is less suitable due to motion blur. To filter suitable calibration images, we created a program to extract the frames from the stereo camera recordings while sorting out blurry images. We extracted 60 frame-pairs and a total of 120 images were used for calibration. Afterwards, the 60 images from left camera were used to correct the distortion of the left camera, and the 60 images of the right camera were used to correct the distortion of the right camera. Then, we used the image pairs to perform stereo calibration. For this purpose, one needs to know the size of the chessboard pattern. This also determines the unit of the measured metric distance results. In our case, the square length of our chessboard was 31.1 mm. Note that the quality of the calibration is crucial to the following estimation of depth.

RECTIFICATION AND EPOPOLAR LINE CORRESPONDENCE:

After the rectification of the stereo images, epipolar lines are drawn parallel to the x-axis of the image and corresponding features should lie on the same horizontal line. Figure 66 shows an example of an undistorted and rectified stereo image pair.

An example for a stereo recording in a fish cage is shown in Figure 67. For any point in the image of the left camera, the corresponding point can be found at the same horizontal axis in the right image and vice versa, except for occlusion. This is guaranteed by the "Epipolar Geometry". The displacement in the horizontal axis needs to be identified to calculate the depth.

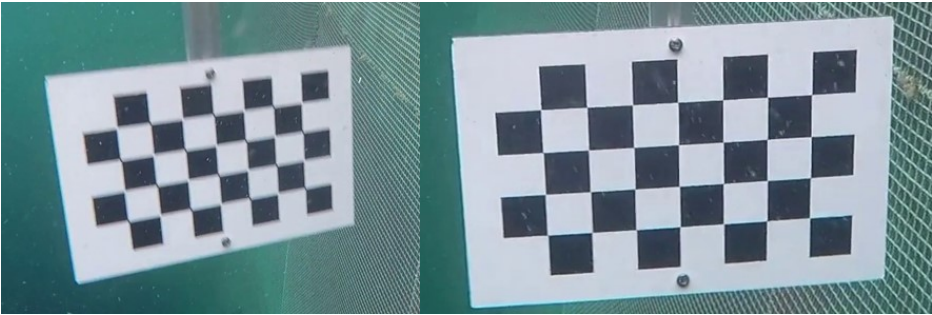


Figure 65: Samples of recordings of the chess board from the GoPro cameras

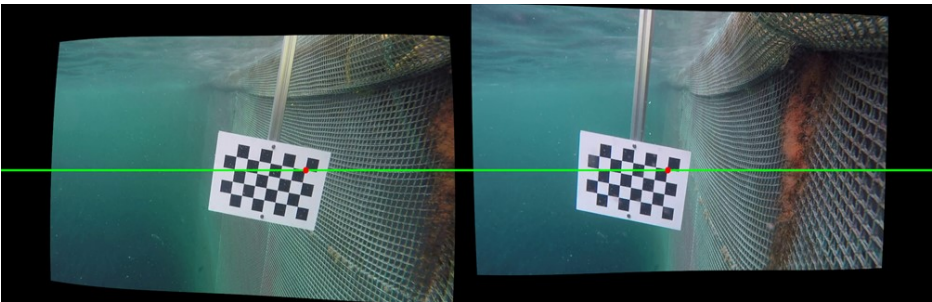


Figure 66: Visualization of the stereo image pair corrected for distortion and rectified. Corresponding features lie on the same horizontal epipolar line (green)

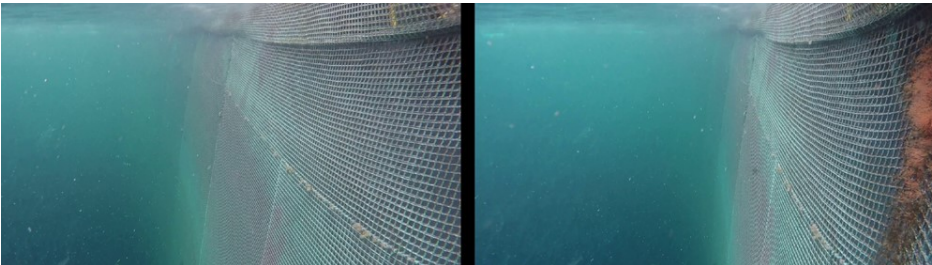


Figure 67: An example of a stereo recording close to the net of a fish cage

DETERMINING THE DISPARITY MAP

The stereo block matching was used to calculate the disparity map after rectifying the undistorted stereo images. OpenCV provides functions like “stereoBM” and “stereoSGBM” to do this. How well these algorithms perform is decided by visual inspection. Two methods were tested in this project: 1. Block matching and 2. Interactive matching.

The functions for block matching depend on many parameters (compare Figure 69) that all need to be optimized simultaneously. Automation is difficult to obtain and specific sets of parameters may work acceptably in specific lighting conditions. Even after tuning, it is still very hard to obtain a point cloud representing the cage net, as shown in Figure 70. However, the same set of parameters does not work equally well for other cases with different light conditions. In many net-related scenarios the net can appear very regular, which makes it difficult to find the correct correspondences in the images. Assuming the ground truth of the disparity is

d_{true} , and the disparity $d_{false} = 2d_{true}$ gave us equally good visual results due to the spatial repeating pattern of the net structure. Subsequently, the distance to the net was estimated to be closer to the camera than it is (factor 1/2). In addition, noise due to ocean particles cause the block matching algorithm to ignore the net. Towards a more

automated solution, a module for estimating the distance and orientation of an object was created. As input, this module required 3 corresponding stereo points. The 3D plane that is defined by these 3 points is used to compute the orientation of this plane. In a later step we plan to obtain these 3 points automatically.

To summarize the problems that need solving, the algorithms need to be more robust against lighting changes and noise originating from floating particle and the water turbidity. In addition, the disparity estimation needs to be more consistent when the ambiguity – due to a regular net structure – is high.

The manual labelling allows a distance and orientation estimation of any object in the stereo images as long as we are able to find 3 corresponding features on the object. Note that corresponding features in the rectified stereo images lie on the same horizontal line (i.e. the green line in Figure 66). For an automated approach to determine the distance and orientation of a net, one needs to determine 3 unique features on the net. Fortunately, some net nodes have fouling organisms on them, and such easily identifiable and unique features help to avoid ambiguities resulting from the regularity of the net. Figure 68 demonstrates an example of the interactive interface that lets user label corresponding features in two mouse clicks.

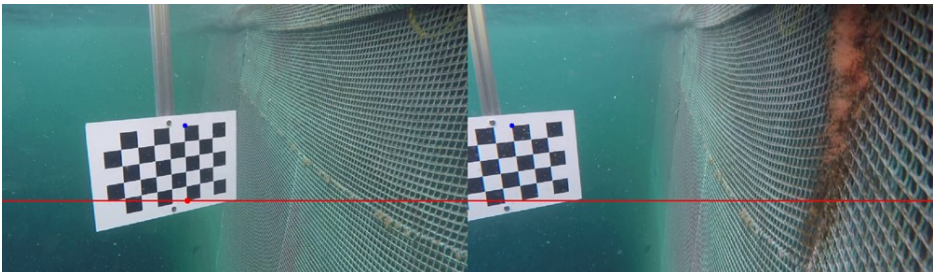


Figure 68: Demonstration of the interactive interface (the interface is waiting for the user to click on the corresponding feature in the right image after marking a feature (red dot) in the left image)

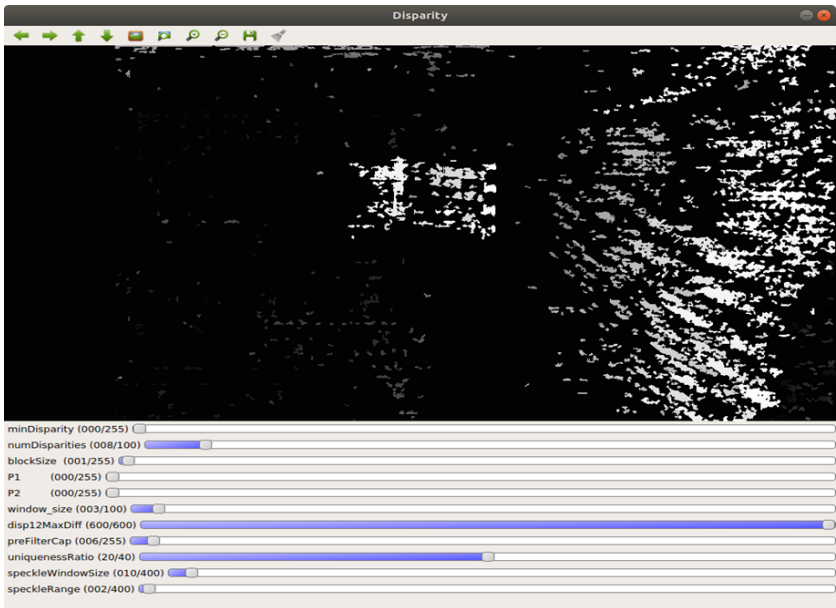


Figure 69: Example of OpenCV stereo SGBM being used to produce the 3D point cloud

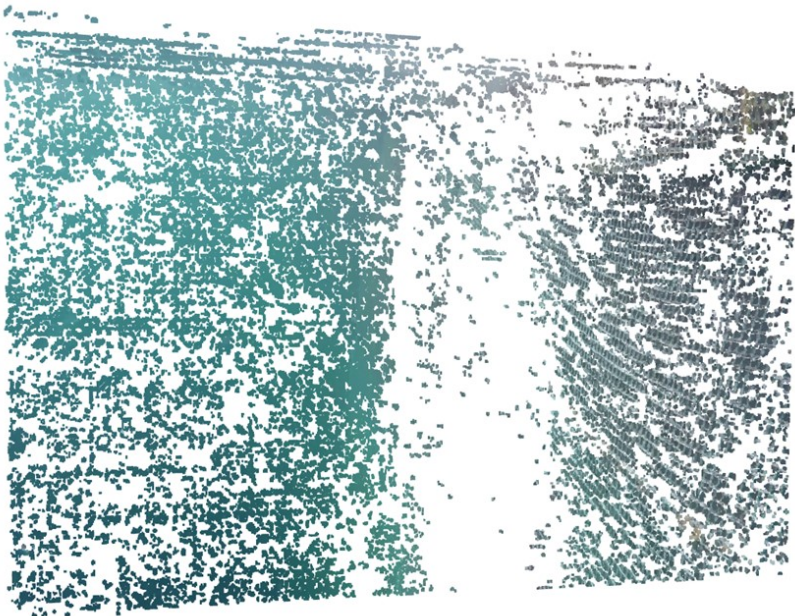


Figure 70: A point cloud of the fishnet using block matching

Once the labelling of three points of interest is finalized, we can define their 3D coordinate in units of the checkerboard measurement and estimate the distance and orientation of the triangle build by these three points. Based on optical physics and multiple view geometry we are able to use the following equation:

$$\underbrace{\begin{bmatrix} 1 & 0 & 0 & -x_c \\ 0 & 1 & 0 & -y_c \\ 0 & 0 & 0 & f \\ 0 & -\frac{1}{T} & 0 & \frac{x_c - x'_c}{T} \end{bmatrix}}_{\mathbf{Q}} \underbrace{\begin{bmatrix} x \\ y \\ d(x,y) \\ 1 \end{bmatrix}}_{\mathbf{A}} = \underbrace{\begin{bmatrix} X \\ Y \\ Z \\ W \end{bmatrix}}_{\mathbf{B}}$$

to calculate the real-world position of any point in the image pair that is visible in both images. Vector \mathbf{A} includes $x,y,d(x,y)$, where x,y are the pixel-coordinates and $d(x,y)$ is the disparity. Vector \mathbf{B} has X,Y,Z,W parameters with the real-world coordinate of the object being $X/W,Y/Z,Z/W$. Note that both \mathbf{A} and \mathbf{B} are provided in homogeneous coordinates. In the matrix \mathbf{Q} , x_c and y_c represent the principal points⁵ of the left image in pixel coordinates. f is the focal length, T is the base line and x'_c is the x-coordinate of the principal point in the right image. In our case, x'_c is equal to x_c . From this information, we are able to calculate the 3D real-world position of the object/point. We can obtain the matrix \mathbf{Q} during the calibration process

and x,y and $d(x,y)$ is determined from the stereo-image pair.

Orientation requires three linear independent points on an object as such three points lie in a plane that can be described by two vectors in \mathbf{R}^3 space. When these two vectors are linearly independent, it will span a plane in \mathbf{R}^3 space. When we calculate the normal

vector of the plane, this corresponds to the orientation (see Figure 71).

In Figure 71 3 points of different colour are marked (blue, green and red). The determined 3D position is shown in the form $p: [x,y,z]$ and D is the computed distance (in millimetre). The x and y axes are shown in bright grey. The yellow plane is the triangle plane of BGR points. The orientation of this plane is illustrated by the purple arrow (The displayed number is normalized to 1) in Figure 71 where the 3D orientation vector is projected onto the x-y plane. Note that the orientation has two solutions and we choose the one which points forward to the camera (e.g. with z component being negative).

⁵Pinhole camera model https://docs.opencv.org/2.4/modules/calib3d/doc/camera_calibration_and_3d_reconstruction.html#camera-calibration-and-3d-reconstruction

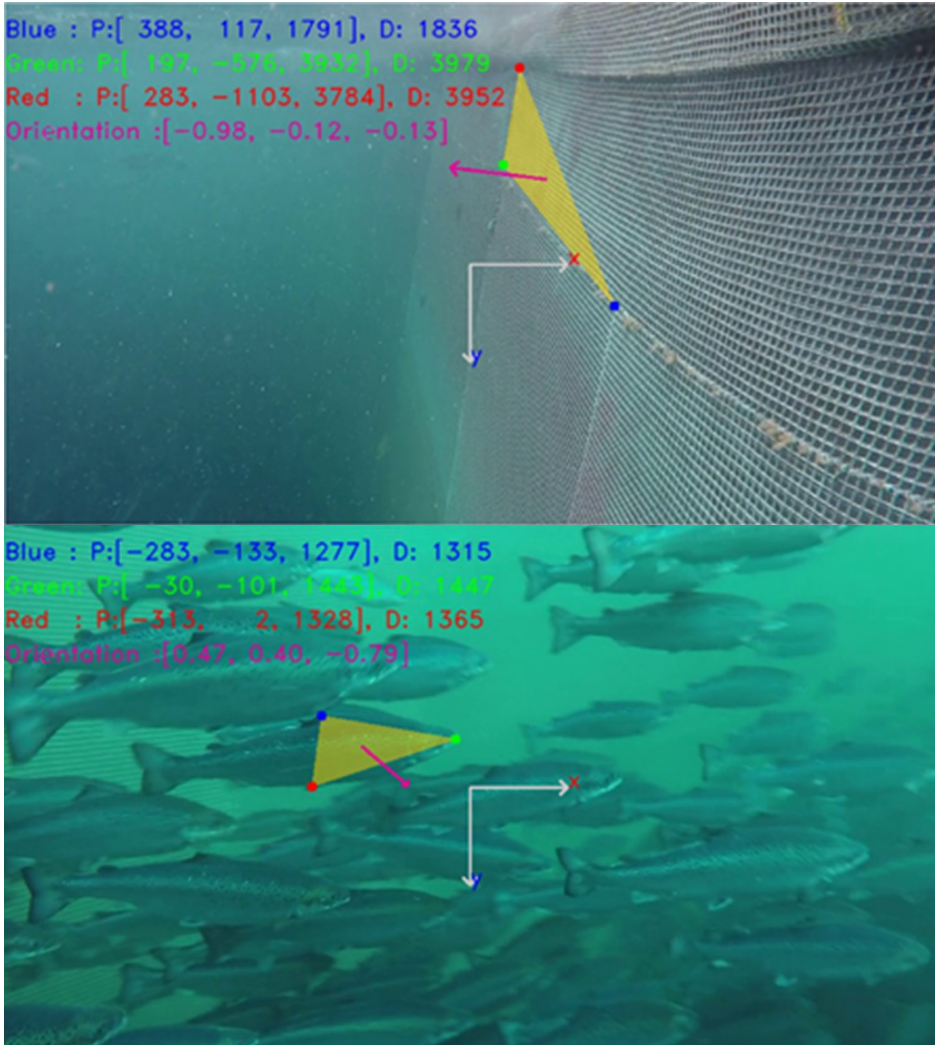


Figure 71: Demonstration of orientation calculation using three points defined on an object

VALIDATION OF THE RESULT

Even though the objects position, distance and orientation seem visually correct, we wish to verify these estimations. Based on the ground truth of the calibration board that identify the side length of a single square (e.g. 31.1 mm), we can select a plane (by defining 3 points with color “BGR”) on the calibration board of known size and get an estimate of the accuracy of the used approach.

In the following, we selected three examples and computed the corresponding errors to validate the obtained results.

In Figure 73, the 3D vector formed by the blue and the green point is: [82,-13,54] , and the vector formed by the blue to the red point is: [1,160,34] The Euclidean norm for these vectors covering 3 and 5 calibration squares are 99 mm and 164 mm, respectively. Based on the square side length of 31.1 mm, one expects a ground truth of 93.3mm and 155.5 mm, respectively. The error in this case is 5.7%.

Two other measurements at longer distances and orientations to the calibration board are shown in Figure 74 and Figure 75 and resulted in increasing errors of 8.5% and 15%, respectively, with the depth estimation becoming more inaccurate with increasing distance. This is also understandable based on fact that the depth d is computed as value proportional to $1/\text{disparity}$ (zero disparity indicates that the point lies at infinity). In particular if we look at the matrix Q , we find that real-world coordinates (x, y, z) are in-

versely proportional to $d(x,y)$. When an object is far away, a small error in disparity shift will increase the depth error as follows:

$$\Delta z = \sqrt{\left(\frac{-fT}{d^2} \Delta d\right)^2} + \dots$$

Here, we can see that with the same Δd , a smaller d will result in a larger error Δz .

Figure 72 illustrates the importance of an accurate stereo calibration. An inaccurate calibration quickly leads to a misalignment, resulting in different y -coordinates for corresponding points expected to lie on the same horizontal epipolar line. However, we note that the observed error is in a range that is still acceptable to guide autonomous underwater operations in a fish cage using robotic vehicles.



Figure 72: Downward epipolar line shift due to the imperfection in the calibration

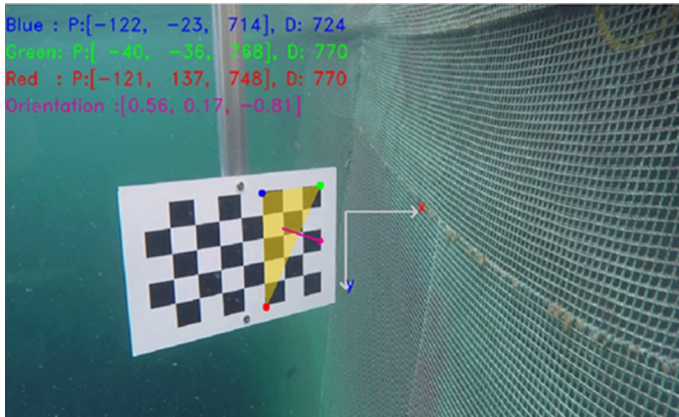


Figure 73: The errors per square length are 1.9 mm, and 1.7 mm (the error is around 6%)

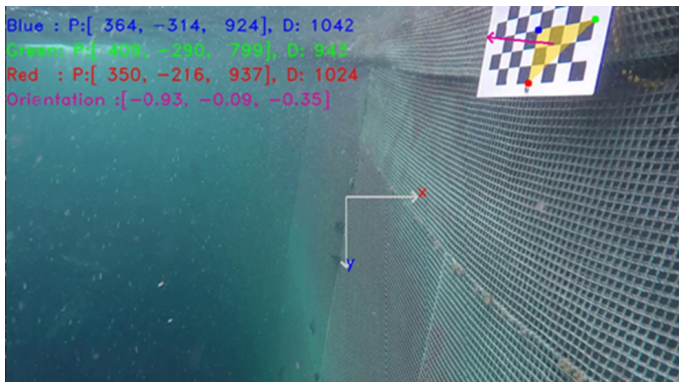


Figure 74: The errors per square length are 2.65 mm, and 1.9 mm (the error is around 8.5%)

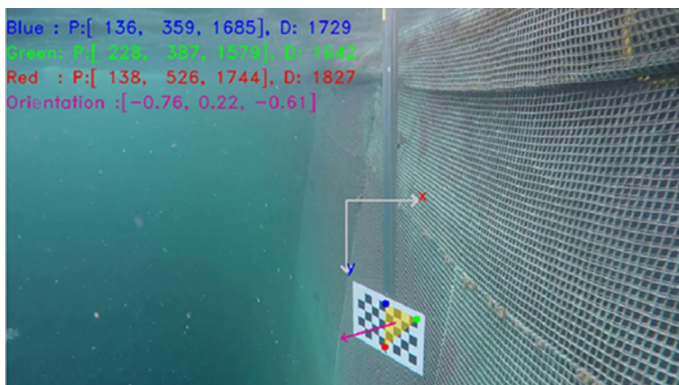


Figure 75: The errors per square length are 4.65 mm, and 4.1 mm (the error is around 15%)

FEATURE TRACKING CONCEPT

If the labelled points have distinct features and do not move very fast (> 10 pixels per frame) between each frame, one can track them for a couple of frames. Sealab AS explored the performance of the feature tracking function. Figure 76 shows some results for a net image sequence where we were able to track the points on the net. The blue dots are automatically detected feature points, and the red dots in the second image are the feature points closest to our selected points in the first image. If the motion of the net relative to the camera is not large ($<$ than the length of one mesh opening), we can follow the net junctions. In this way, we can track the positions of the triangle points, thus determining the distance and orientation of the triangle.

We have recorded different video sequences in order to test the efficacy of the methods by determining the number of frames we can track the selected points. The first video sample was recorded with 20 frames per second and has a total number of 50 frames (see [video](#)). For this video we were able to track a group of points reliable for 36 frames [Note, at frame 37, one of the points jumps to the neighbourhood net junction]. We

observed that the tracking fails when the motion or the motion blur are too large. In this case, motion blur from the used GoPro cameras is the reason for discontinued tracking. We believe that using the SEALAB camera with very low motion blur would enable much longer tracking. In an additional test with a ZED stereo camera we followed the same procedure as for the GoPros (i.e. calibration is included). In this test we moved the net very slowly, and were able to reduce the motion blur significantly (see [video](#)). Thus, we were able to reliably track features on the net for approximately 200 frames. We conclude that the reliable tracking of net-features required for an industrial fish cage inspection needs the development of dedicated software modules.

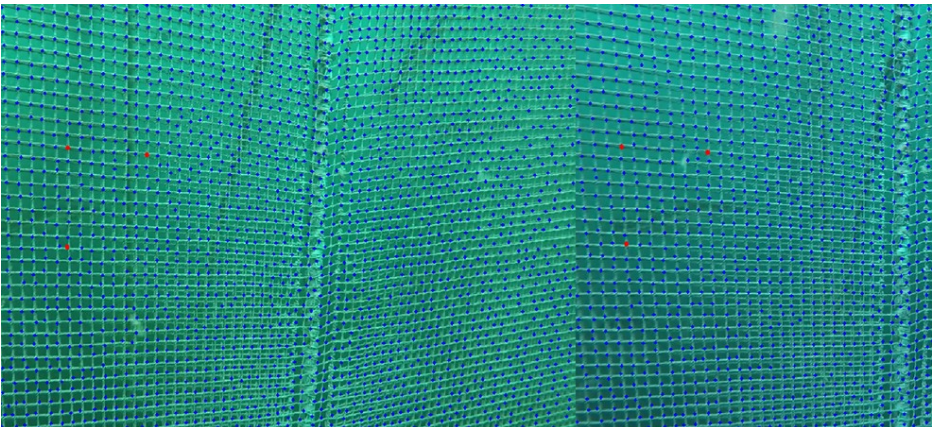


Figure 76: Feature tracking of cage net junctions (GoPro on ROV)

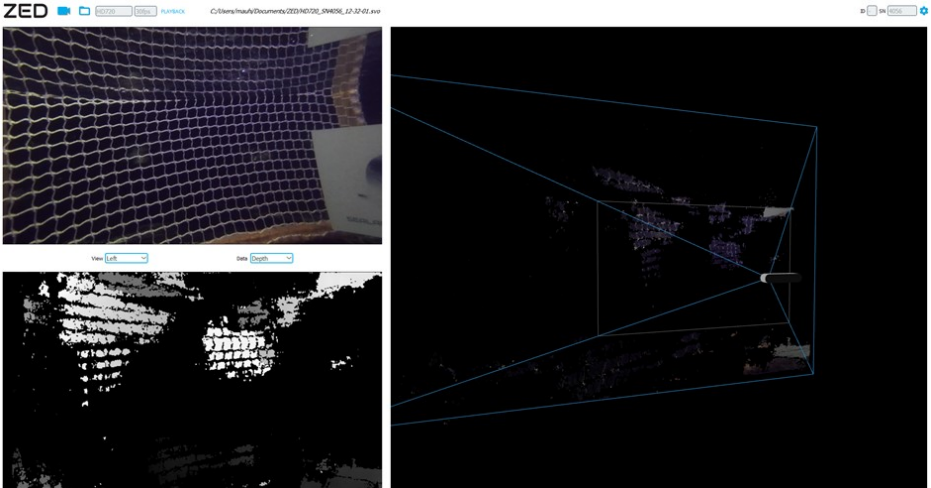


Figure 77: Disparity map and 3D point cloud from dedicated software of ZED

In our experiments we also observed that the orientation vector is 'jiggling' because the features tracking detects the corner of a net junction randomly in the upper left, upper right, lower left and lower right. This happens particularly when the net is too close, and the size of the net junction increases. However, the ZED stereo camera is a consumer stereo-camera that has its own dedicated stereo-matching algorithm and 3D point cloud viewer. Figure 77 shows results obtained with the ZED-camera when it is used for underwater recordings (a cage net placed in a smaller tank). The depth estimation from the ZED is not ideal and subse-

quently most of 3D structure of the net were missing. It appears that the ZED camera may not be ideal for underwater use and that the parameters are optimized for "in-air" recordings, and that a simple recalibration for underwater-conditions is not possible. And even in areas of the image where distortion appears to be small (in the middle), it is still hard for ZED's matching algorithm to find correct correspondences. In the future, the developed side-by-side stereo system discussed in Section 2.1 will be tested thoroughly and compared with results obtained using the GoPro-setup and ZED-camera system.

RESULTS FROM SEALAB STEREO CAMERA

After repairs, some initial calibration tests could be conducted with the Sealab stereo cameras. The tests showed that a low shutter time, strong LEDs, and a 4K resolution were able to resolve any issues related to motion blur. As a consequence, all images of the chessboard show sharp corners, indicating successful calibration is possible.

tation, indicated by the two optical axes being parallel to each other. In Figure 79, the Euclidean norms are 193.5 mm and 95.8 mm, and the ground truths are 186.6 mm and 93.3 mm, respectively. The error per square are 1.15 mm and 0.83 mm. The error is around 3.6%. Recall the fact that $d(x,y)$ are constraint to integers in this case since the distance

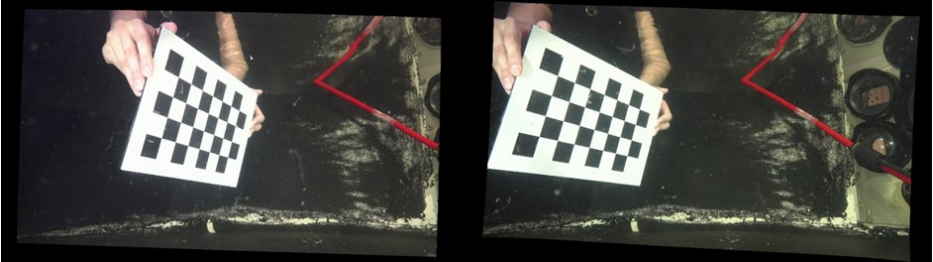


Figure 78: Calibration of the Sealab stereo cameras

In Figure 78, the stereo image after calibration and correction is shown. However, the chessboard lines were almost straight lines already before correction. This indicates that the Sealab stereo cameras has a very low distortion underwater. Both left and right stereo images have an almost parallel orien-

tion between two pixel positions is an integer. With the Sealab stereo camera having a 4K resolution, this will expand $d(x,y)$ domain and consequently expand the range of the z-axis. This will decrease the error (and higher z-resolution) when estimating an object that is far away.

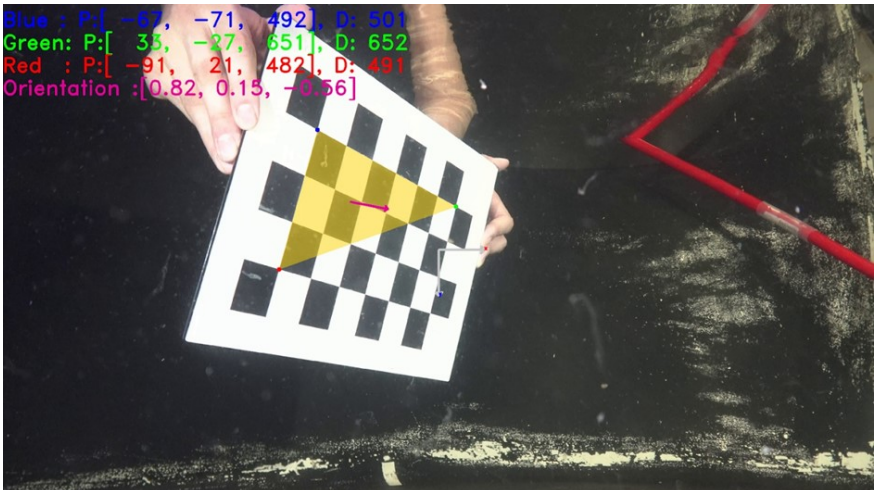


Figure 79: Distance and orientation measured using the Sealab camera

DISCUSSION

In this section, the progress of the developed algorithms for distance and orientation calculation using a stereo setup was reported. Initially, we investigated the use of a stereo block matching algorithm to compute the disparity map that could then be used to generate a 3D point cloud. However, the method proved not to be suitable for the considered underwater environments and will need to be adapted significantly to provide meaningful result. Furthermore, it was difficult to tune all relevant parameters using the stereo block matching algorithm, even for just a single frame. Therefore, we decided to postpone the automatic selection of features on a particular object (e.g., the net) to future work. However, we successfully implemented a module for the distance and orientation computation with an interactive matching as input. This gives accurate result

and it is mathematically rigorous. Therefore, we believe that we can estimate the distance and the orientation of any object given we are able to determine corresponding features in both images of the stereo camera. In frames containing nets, repetitive regular patterns are a problem for an automated net feature matching approach. This challenge may be overcome by selecting unique points such as biofouling organisms growing on the net or repaired net features causing irregularities to use as reference points.

Considering this challenge, the use of a laser could be a beneficial solution as it can produce a unique, recognizable point in the image. This will enable the algorithm to find and track correct correspondences also in areas with a very regular net structure and few unique features.

H2.4 RESULTS FROM FIVE MASTER THESES RELATED TO CAGEREPORTER

Towards Underwater Biomass Estimation using Plenoptic Technology (Malin Kildal, June 2017: Supervisor: Annette Stahl, NTNU, Department of Engineering Cybernetics (ITK))

This thesis investigated the capabilities of 3D plenoptic camera technology to determine whether it can provide decent depth information of objects underwater. As there was no documentation of this technology working in underwater conditions, the underwater calibration procedure and metric measurements were performed. The plenoptic camera technology has been developed as a tool for 3D monitoring in stable and still environments and this thesis explored, by analysing the calibration process and by verifying measured depth points from the determined depth map, if the technology has the potential to be used in an ocean fish farm for measuring the biomass of several hundred thousand Atlantic Salmon.

Results from this thesis show that this technology must be further developed and tested before a complete biomass estimation system can be built, but the results also indicate that this technology indeed has potential for biomass estimation in fish farms. Figure 80 shows the Raytrix camera attached to an aquapod test rig. The best choice for an underwater housing for this system is a flat port. To obtain good results in applied underwater conditions, the fish should be close to the camera as fish farms produce a lot of noise in form of many particles in the water from food and excrement, which degrade the quality of the recorded depth map. A normal field-of-view lens is preferable, even if a narrow field-of-view lens provided a more accurate depth-map.

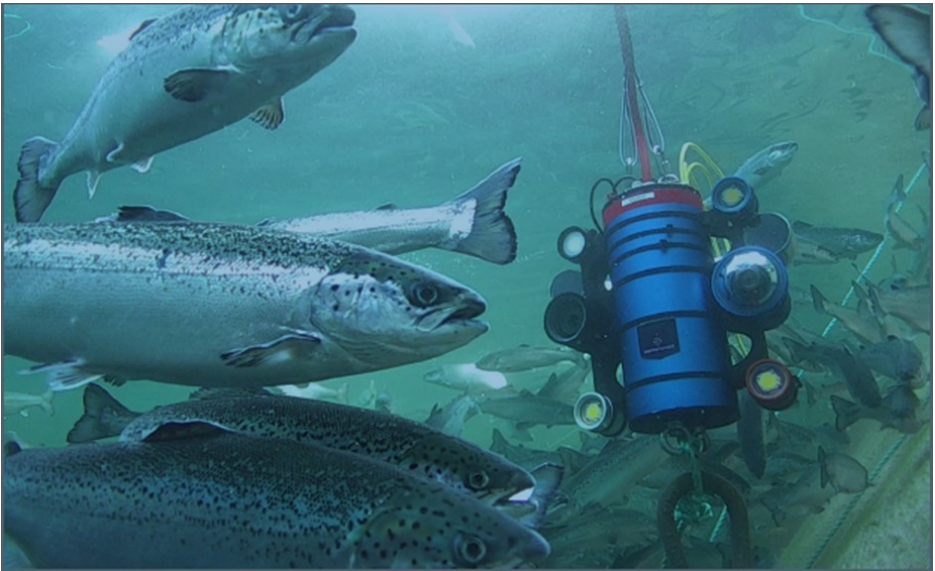


Figure 80: The SEALAB Aquapod with the Raytrix R42 camera attached at the Kåholmen test facility on Hitra. Photo: SEALAB AS

Stabilization of an underwater camera (Thomas Norum Ur, June 2017: Supervisor: Annette Stahl, NTNU, Department of Engineering Cybernetics (ITK), Co-Supervisors: Per Rundtop and Christian Schellewald, SINTEF Ocean)

This thesis describes the development, implementation and testing of a full-scale underwater camera system for surveillance purposes in aquaculture. The mechanical development was carried out using Solidworks, and the software implementation was based on ROS (Robotic Operating System), in which several open source libraries have been incorporated. A mathematical model of the camera system has been derived as well as a simulation tool in Matlab for simulation. Suspended from a single rope, the camera system is equipped with a water jet propul-

sion system that allows the yaw (heading) to be controlled by the use of a PID controller (Figure 81).

A gimbal inspired mechanism enables control of the camera pitch (tilt). Experiments at a full-scale fish farm facility yielded promising results for the yaw-control, whereas the pitch control needs to be further developed. The work presented in this thesis has been carried out during the spring of 2017 in collaboration with Sealab Ocean Group and SINTEF Ocean.

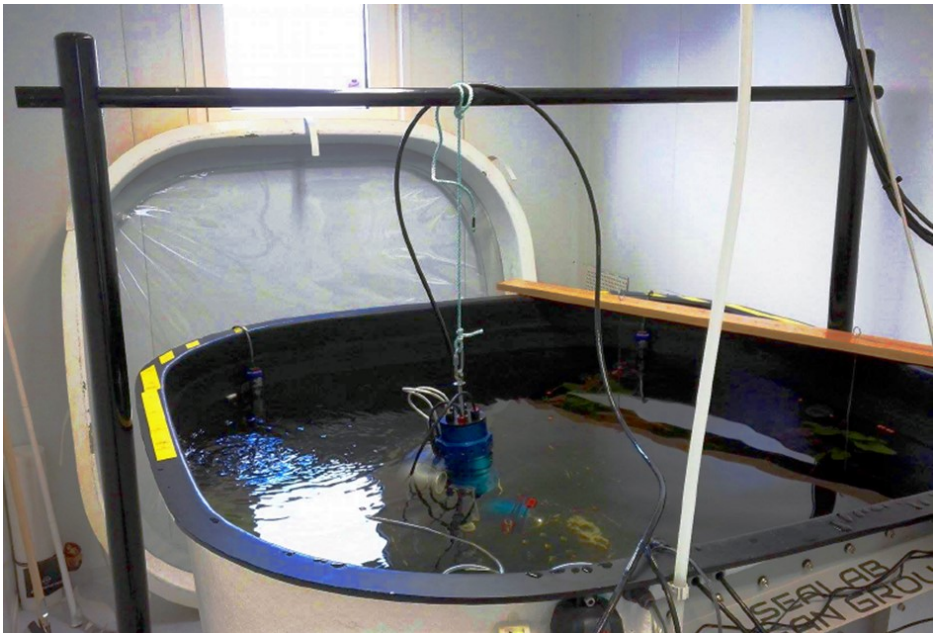


Figure 81: The developed stabilization rig with a camera attached in the SEALAB wet lab. Photo: SEALAB AS

Classification of fish body parts in an underwater environment (Thorbjørn Sømød, July 2017: Supervisor: Annette Stahl, NTNU, Department of Engineering Cybernetics (ITK), Co-Supervisors: Per Rundtop and Christian Schellewald, SINTEF Ocean)

This master thesis investigated a possible approach to recognizing fish parts in a video stream from a camera system situated in an underwater environment. This task can be seen as the first part of a three-step scheme for implementing an automatic system for fish health assessment in the fish farming industry. This thesis describes the work done in setting up an interface to an IP camera that is situated in an underwater environment, collecting and labelling image material from the camera system for training and testing object classifiers, and training the object classifiers for multi-class object recognition based on image descriptors suitable for an underwater environment. Finally, a complete object recognition framework was implemented and performance tests were conducted based on the pre-trained classifiers.

The results are analysed in Figure 82. The results of this thesis show that it is possible to create a system that is able to perform this classification by relying on Support Vector Machine (SVM) classifiers based on

adaptations of the Local Binary Pattern (LBP) image patch descriptor. By using a linear SVM classifier, good results are achieved. Surprisingly, the non-linear SVM classifiers relying on the RBF kernel achieve much lower performance than most of the linear SVM classifiers.

The final goal of a complete system for the recognition of fish parts in a live video stream could not be reached with this classical computer vision and machine learning approach. The classifiers trained on the training images acquired at the test facility at Kåholmen on Hitra, Norway, were not able to classify image patches acquired from video streams taken at a later time. It is suspected that this is because the image patches used for training are not representative of a larger population. We note that state-of-the-art neural network-based approaches show more promising performance in detecting parts of fish. In particular, we refer to results achieved within the IPN project INDISAL.

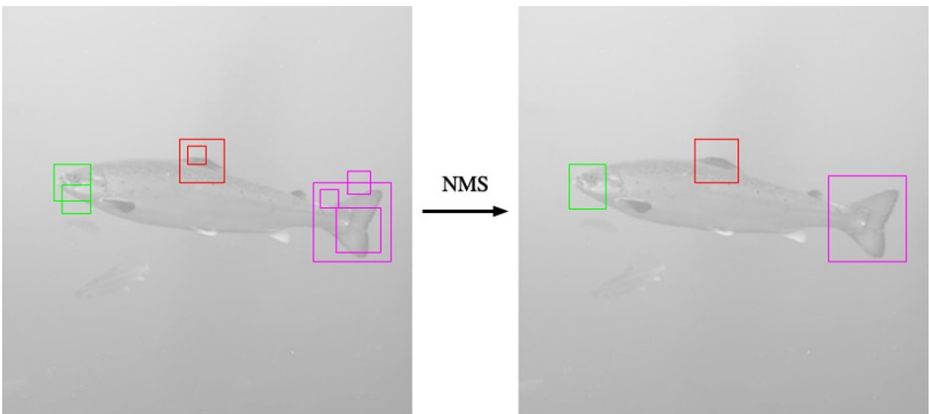


Figure 82: Exemplary results from the developed fish part detection algorithm. After a final non-maxima suppression (NMS) the desired parts of the fish can be detected

Saliency based methods for camera orientation in aquaculture (Magnus Conrad Harr, June 2018: Supervisor: Annette Stahl, NTNU, Department of Engineering Cybernetics (ITK), Co-Supervisors: Christian Schellewald, SINTEF Ocean)

The aim of this thesis was to develop and provide insights into a saliency-based approach for automatic orientation of an underwater camera such that interesting/relevant regions are always captured. Existing algorithms for this purpose are not suitable for separating interesting and non-interesting objects in a sea-cage. Therefore, modifications/additions to these algorithms were implemented and tested. For the performance comparison, several saliency estimation techniques were used, combined with different extensions aiming specifically to work for aquaculture underwater recordings. The results are based on footage from an underwater camera system developed by Sealab (Figure 83). This project lays the foundations for future 24/7 surveillance in sea-cages using computer-vision algorithms. Such algorithms can also provide an image

quality guarantee to operators with remote system access, even when the site is unmanned. The results presented in this thesis indicate that performing general camera orientation based on visual saliency in a sea-cage is difficult. It is expected that for a saliency-based orientation algorithm to function it will have to either be operated only when the camera is sufficiently far from the cage net or be used in tandem with a cage-net detector. As an alternative to a cage-net detector, one could implement a fish detector instead and use that as the basis for an automatic orientation. In conclusion, visual saliency can provide a basis for camera orientation. However, it is likely that other approaches based on machine learning (i.e. learning what is considered interesting or learning which objects should be looked at) would perform better.



Figure 83: Example for a saliency detection algorithm applied to an underwater image containing salmon

In this thesis the possibility of using unsupervised learning based on motion patterns to automatically classify the main groups of objects in a fish farm were investigated. The focus was on separating fish from feed. The approach is based on the hypothesis that fish and feed have distinct motion patterns that can serve as criteria to distinguish the two. The implemented approach is based on optical flow using KLT-tracking to estimate the motion in the image sequences. Similar motion patterns are automatically grouped together using cluster analysis. Mean shift and DBSCAN were chosen as the algorithms to be used in the experiments, based on a preliminary analysis of the motion data. Mean shift is centroid based, while DBSCAN is density based which provided a useful combination of differing properties to compare. Further, the effect of increasing object sizes to the

clustering results was studied.

Results showed that automatically distinguishing fish and feed based on motion patterns is plausible under certain conditions (Figure 84). There are some requirements for the camera position that improve the classification accuracy. For instance, the clustering performance increases when numerous objects are simultaneously visible. Appropriately determining the clustering parameters is also necessary to avoid cluster merging. In cases where several clusters are merged together, valuable information about the objects gets lost. We found that the number of available data samples were too small to draw a conclusion, but for the tested image sequences we were able to distinguish visible motion patterns.

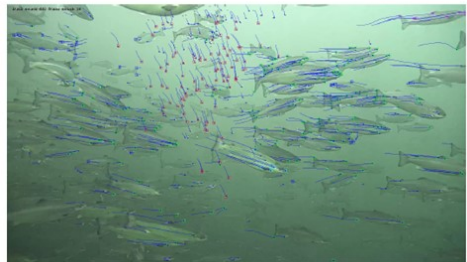
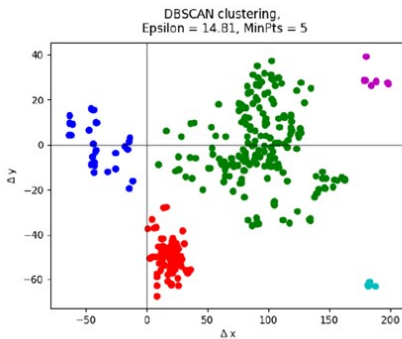


Figure 84: Example for automatic clustering of motion patterns visible in an underwater image-sequence containing salmon and feed pellets

CONCLUSIONS

This report presents the development and validation of a 3D vision system to be used for data capture in fish cages. In particular, a compact and robust sensor with optical components and lighting system was developed to capture high-quality vision data. In addition, methods to evaluate the quality of the captured data were investigated and subsequently validated using vision data obtained from 24/7 video streams from a full-scale fish cage. This report furthermore includes the development of image processing algorithms to estimate the distance and orientation relative to the inspected object of interest, such as the fish or the net. The developed algorithms have been validated based on vision data obtained during laboratory and full-scale tests.

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